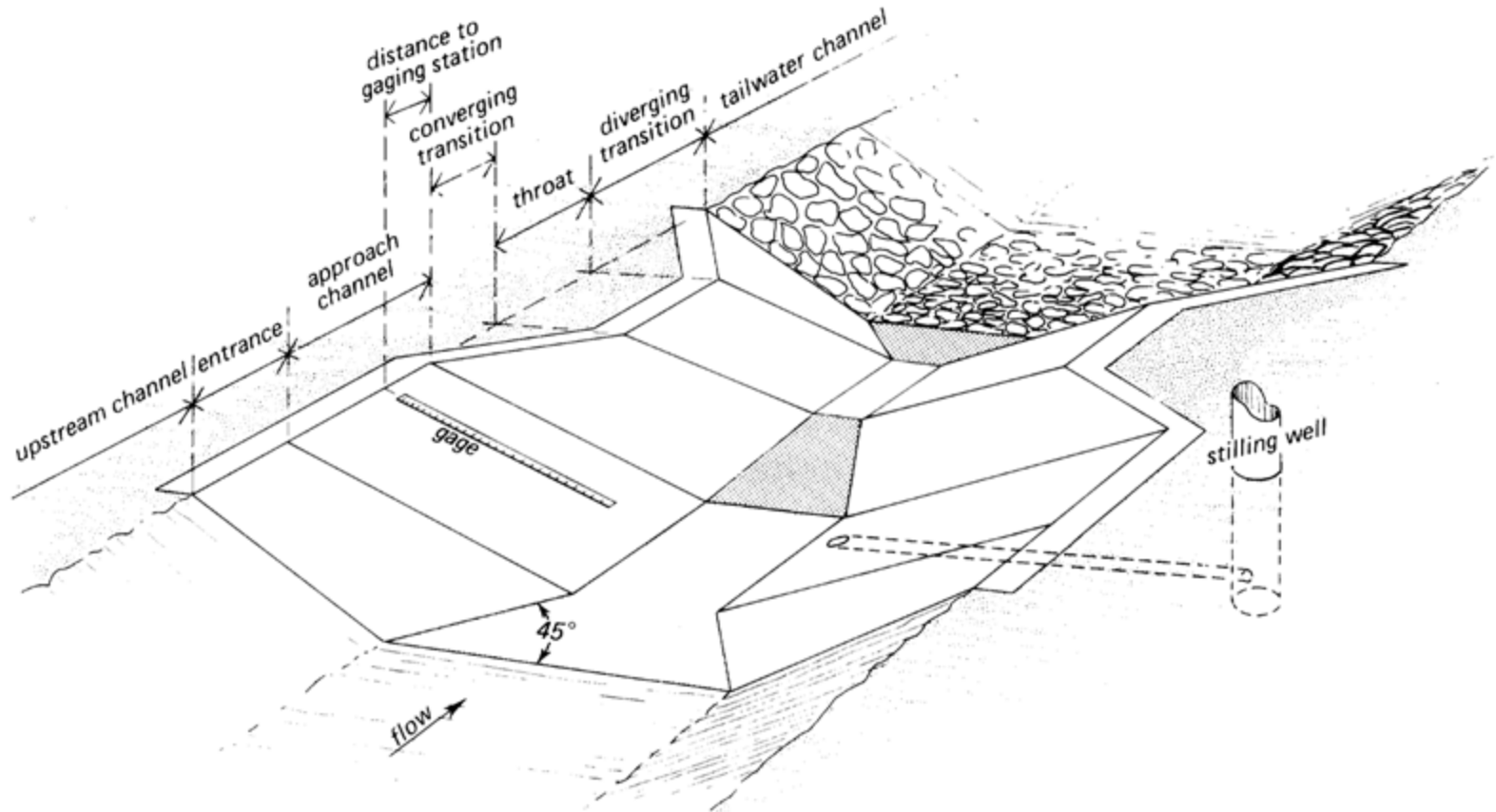
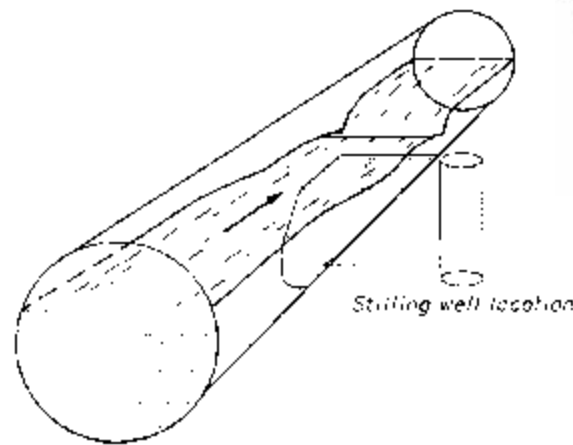
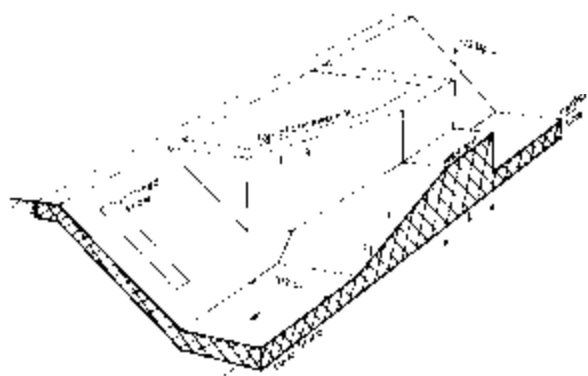
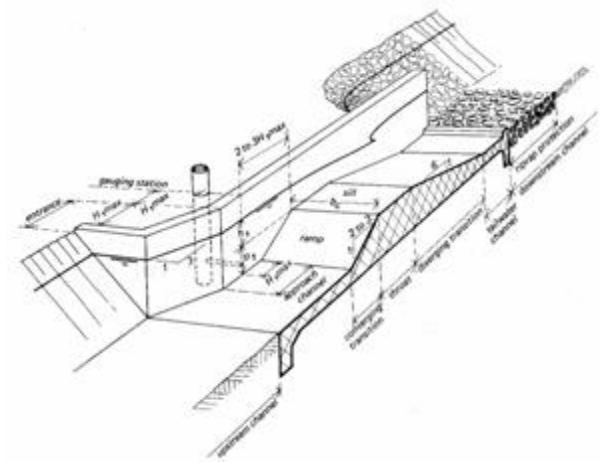
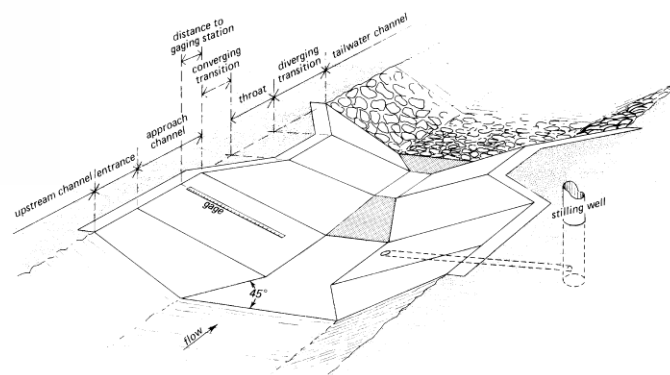
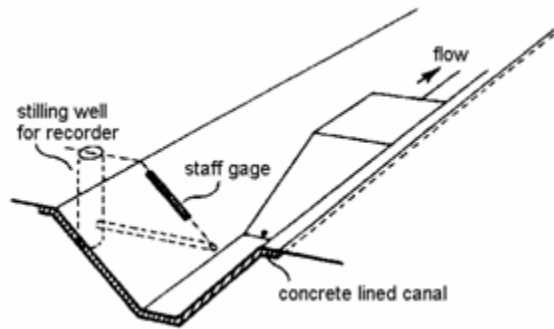
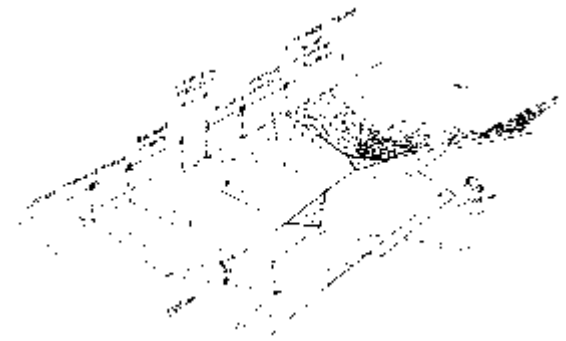
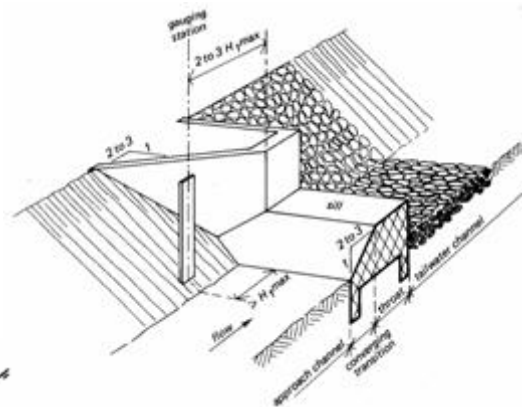


# Introduction to Long-Throated Flumes (Ramp Flumes), Broad-Crested Weirs and WinFlume



The term *long-throated flume* describes a broad class of critical-flow flumes and broad-crested weir devices used to measure flow in open channels.

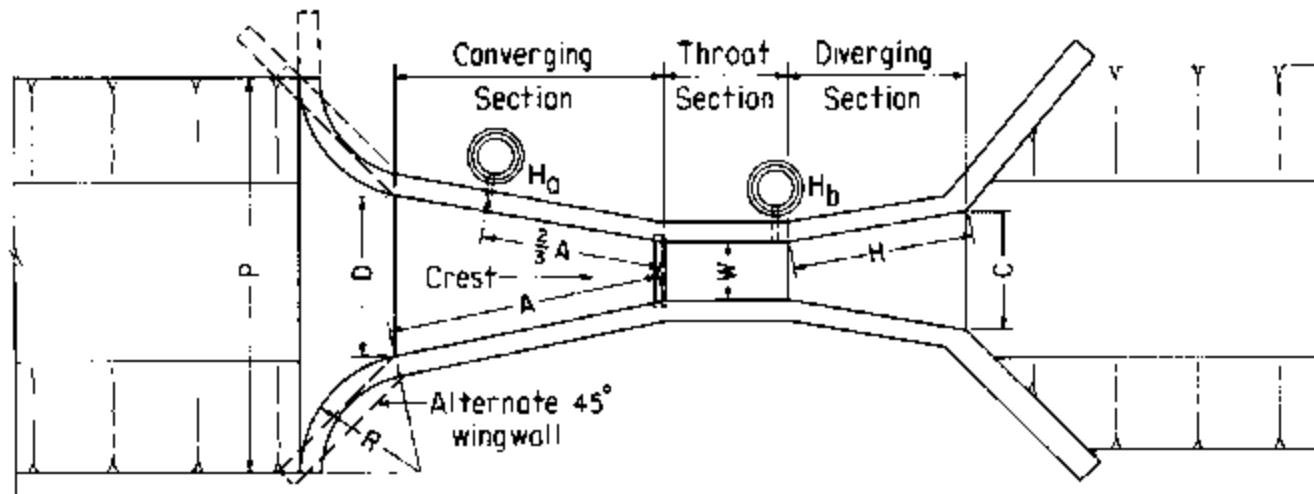


# Traditional Critical-Flow Devices

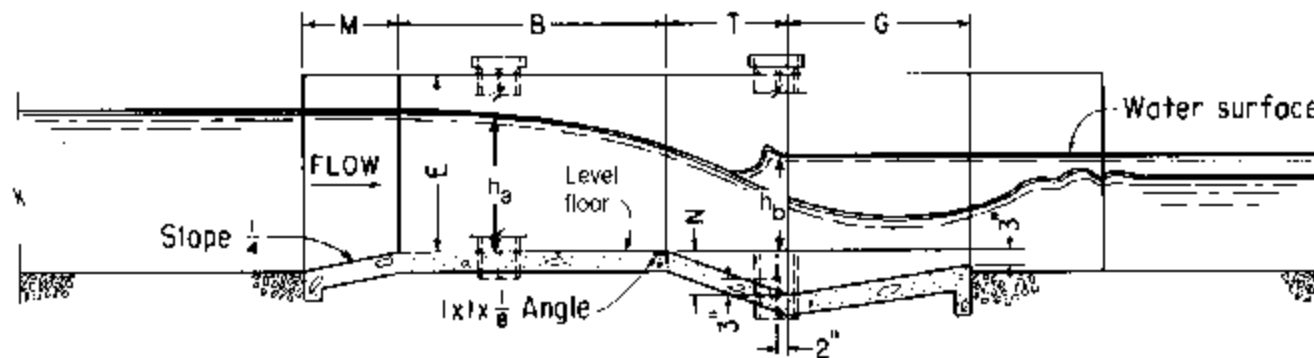
- Traditional critical-flow devices have curved, three-dimensional flow fields in the control section
- All such devices **require laboratory calibration**
- Parshall flumes, cutthroat flumes, H-flumes, etc.
- V-notch weirs, Cipoletti weirs, rectangular weirs



# Parshall Flume



**PLAN**



**PROFILE**

# Long-Throated Flumes and Broad-Crested Weirs

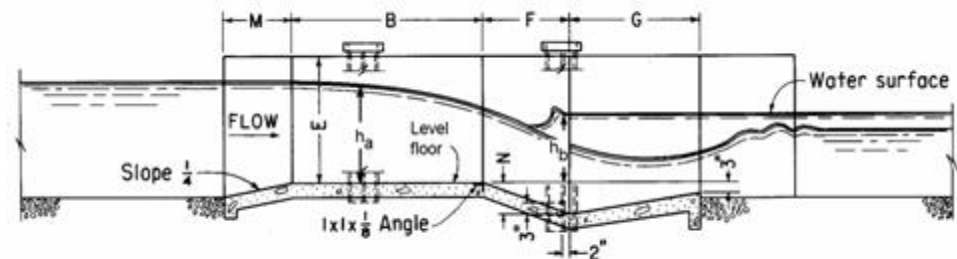
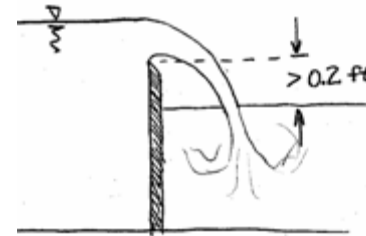
- Long-throated flumes have one-dimensional flow in the control section -- *Long-throated means long enough to eliminate lateral and vertical contraction of the flow at the control section...streamlines are essentially parallel*
  - Can be calibrated using well-established hydraulic theory
    - **No laboratory testing needed**
  - Calculations are iterative and tedious, so computer models that do the calculations have made long-throated flumes practical in recent years

# Advantages of Analytical Calibration

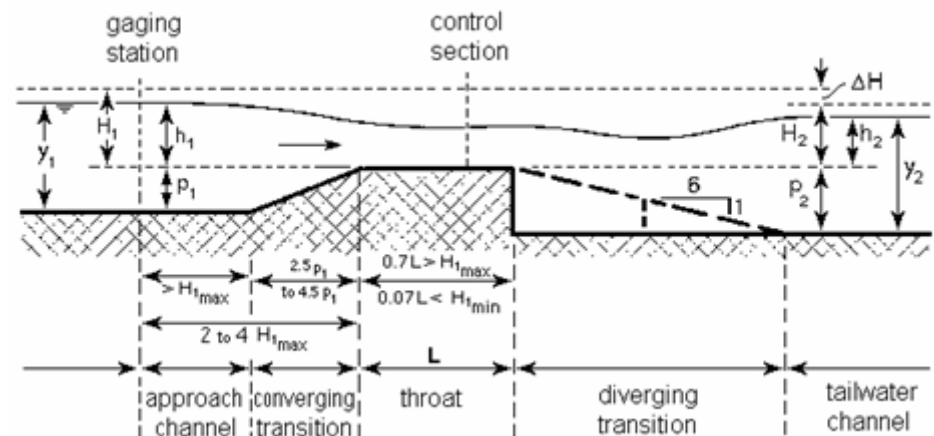
- Allows design of flumes customized to your site and needs
- Easy to calibrate using as-built dimensions
- Better measurement accuracy  
 $\pm 2\%$  uncertainty vs.  $\pm 3-5\%$  uncertainty
- Can accurately predict tolerance for submergence

# Submergence of Flumes and Weirs

- $h_2/h_1$  or  $h_b/h_a$  is the submergence ratio
- Sharp-crested weirs
  - NO SUBMERGENCE ALLOWED
- Parshall flume
  - Some submergence allowed, 50-80%
- Long-throated flume and broad-crested weir
  - Most submergence allowed, 80-95%



PROFILE

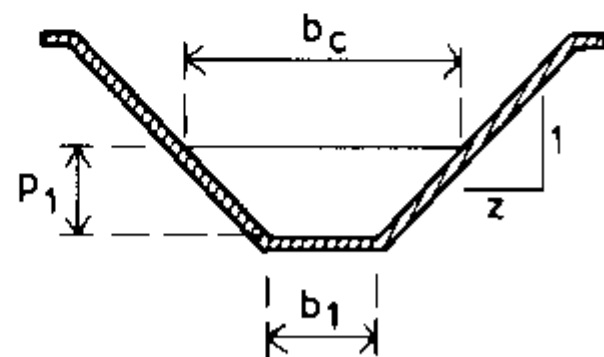
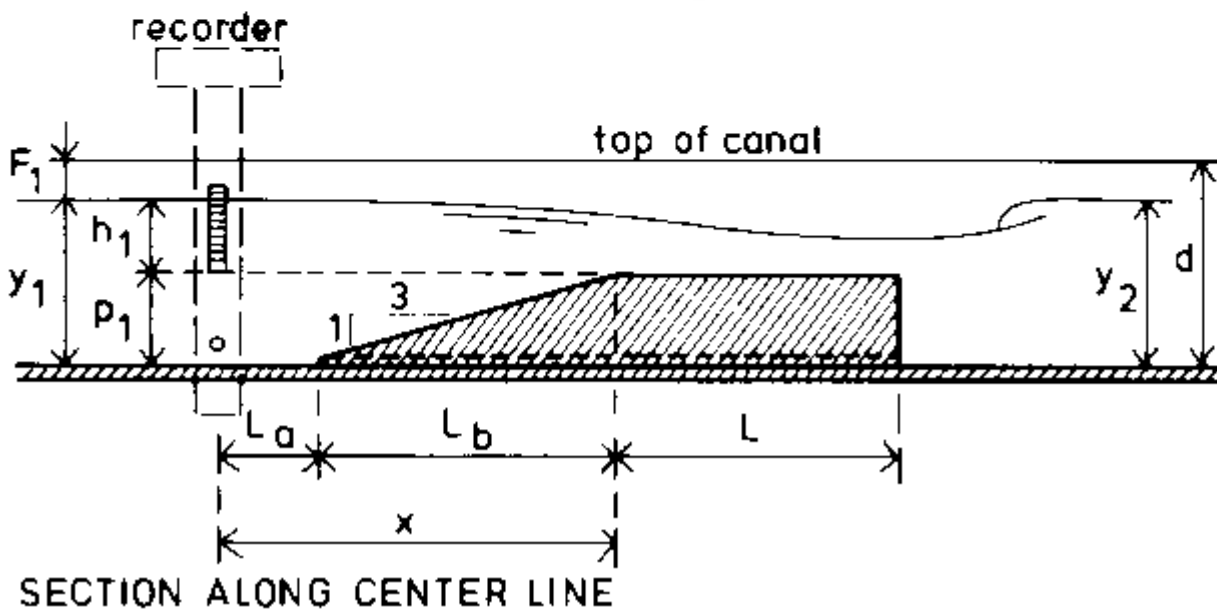
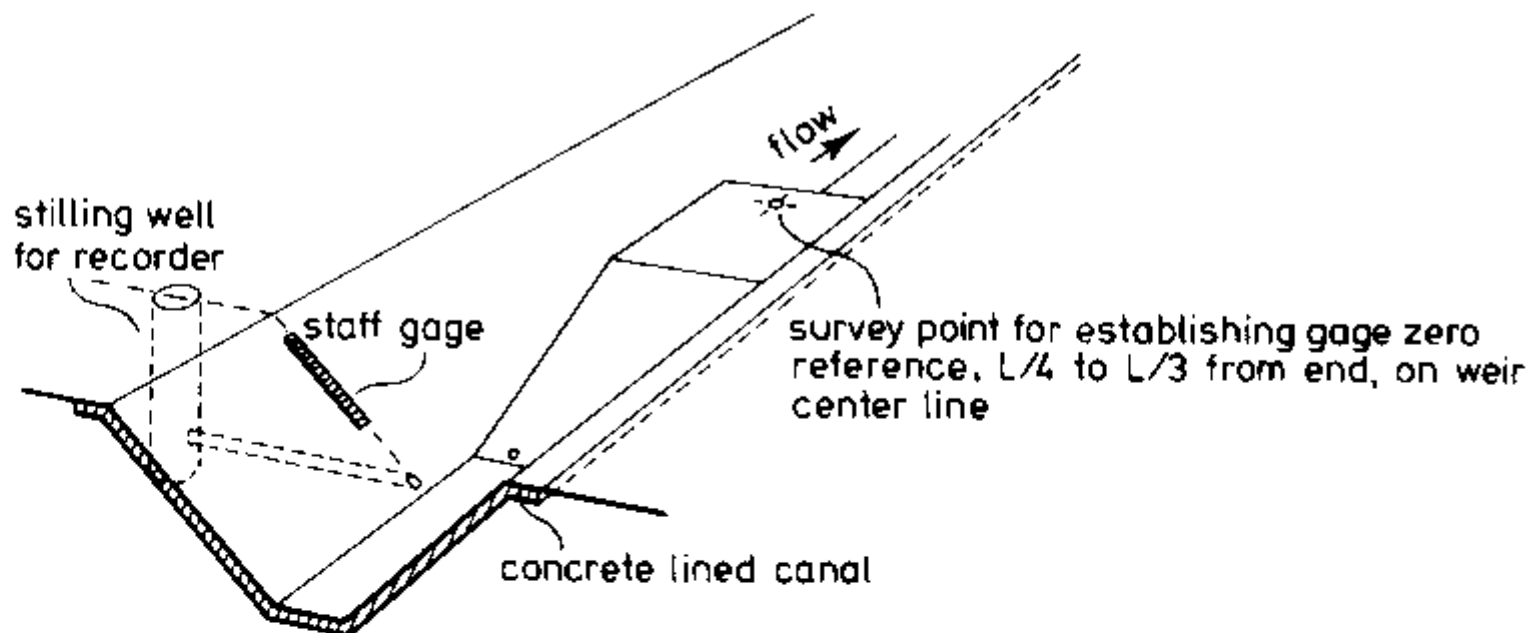


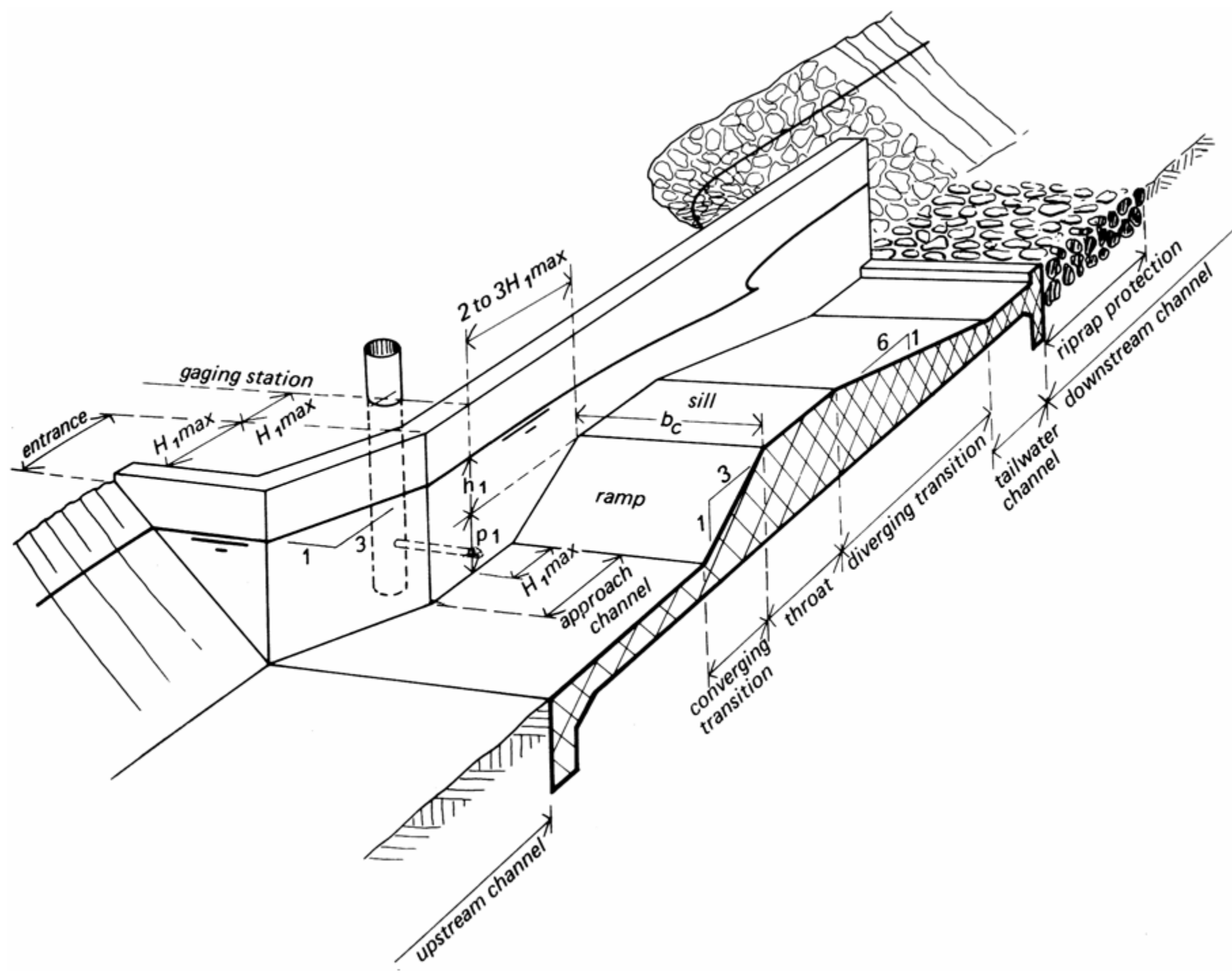
# Throat Section Shape Selection

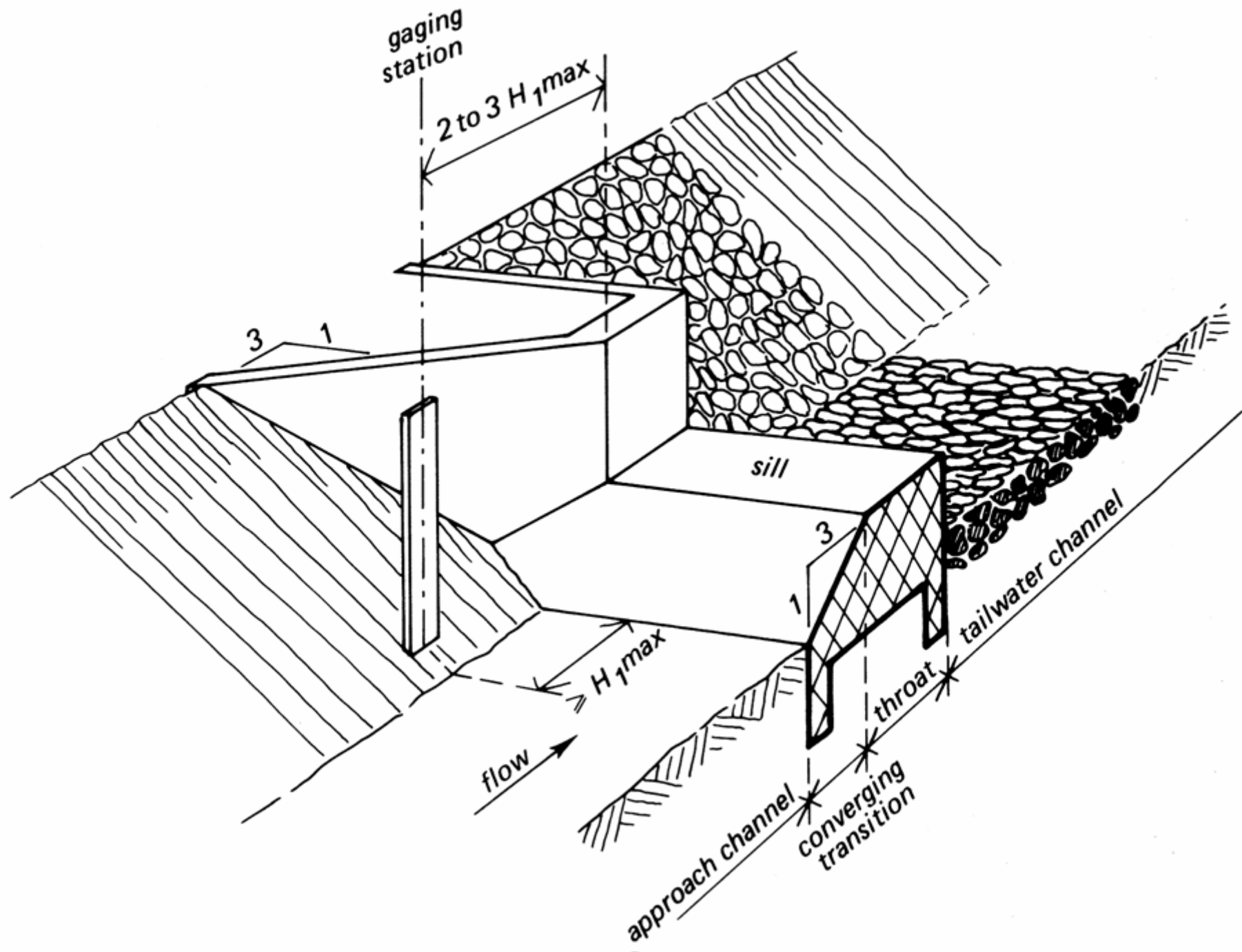
- Constructability
- Range of Flows to be Measured

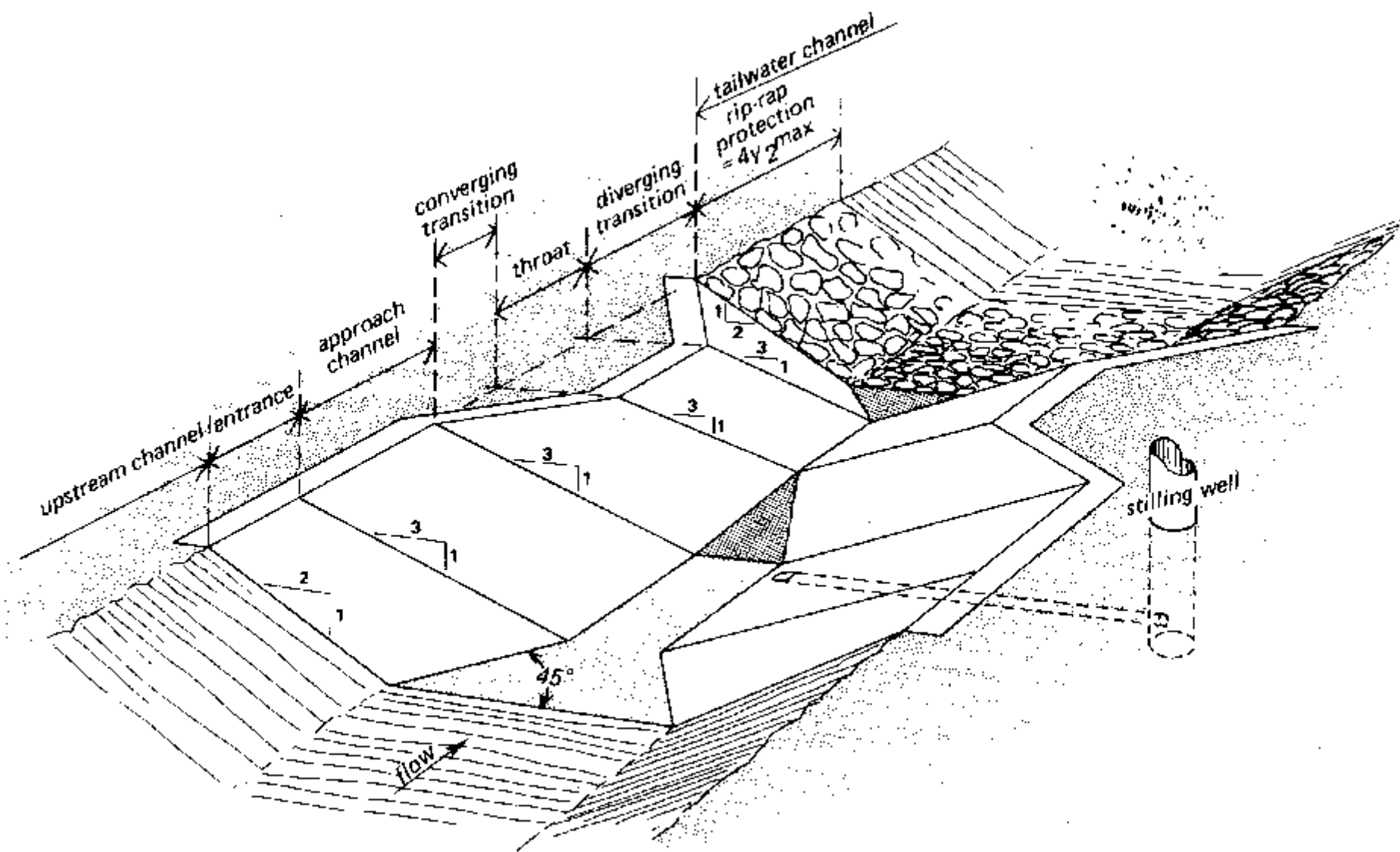
Shape	$Q_{\max}/Q_{\min}$ $\pm 2\%$ uncertainty	$Q_{\max}/Q_{\min}$ $\pm 4\%$ uncertainty
Rectangular	35	100
Triangular	350	1970
Trapezoidal – wide at top	55	180
Trapezoidal – narrow at top	210	1080
Parabolic	105	440
Complex – wide at top	> 100	> 200
Complex – narrow at top	> 250	> 2000











**Figure 4.12.** Triangular-throated flume.

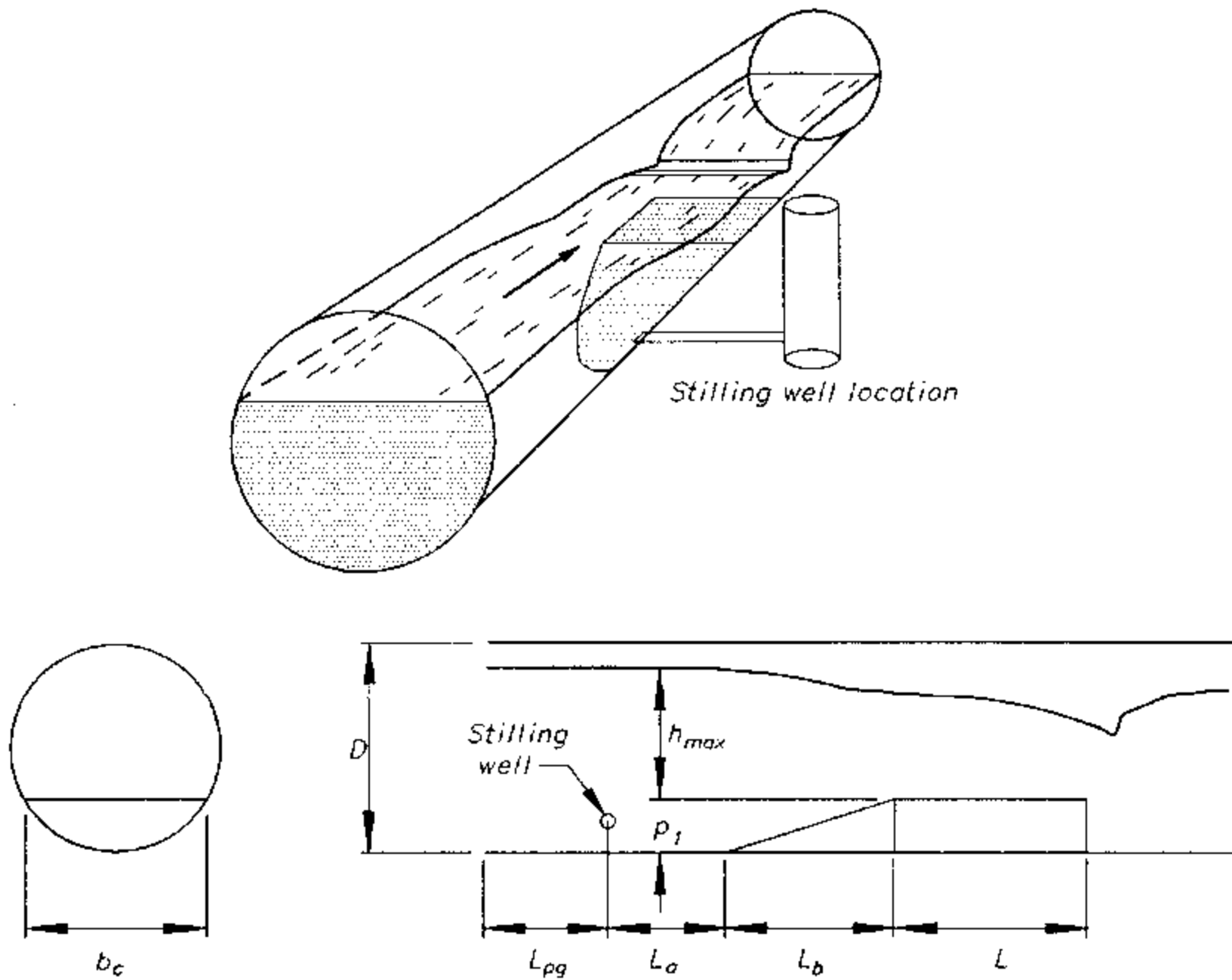


Figure 8-7.—Long-throated flume in a partially filled circular conduit.

# Flume Design & Selection

- Pre-computed flume designs can be chosen using tables in the Water Measurement Manual
- Designs can be developed using the WinFlume computer program
  - Allows for customization
  - Provides best rating table accuracy
  - Simplifies checking of design

# *WinFlume*

## SOFTWARE FOR THE DESIGN AND CALIBRATION OF LONG-THROATED FLUMES AND BROAD-CRESTED WEIRS



Water Resources Research Laboratory  
Denver, Colorado



U.S. Water Conservation Laboratory  
Phoenix, Arizona



International Institute for Land  
Reclamation & Improvement  
Wageningen, The Netherlands

# HOW TO OBTAIN WINFLUME

- The WinFlume program is available on the World Wide Web at:  
**[http://www.usbr.gov/pmts/hydraulics\\_lab/winflume](http://www.usbr.gov/pmts/hydraulics_lab/winflume)**
- There are 16-bit and 32-bit versions available that are appropriate for Windows 3.1x, Windows 95, Windows 98, and Windows NT systems.

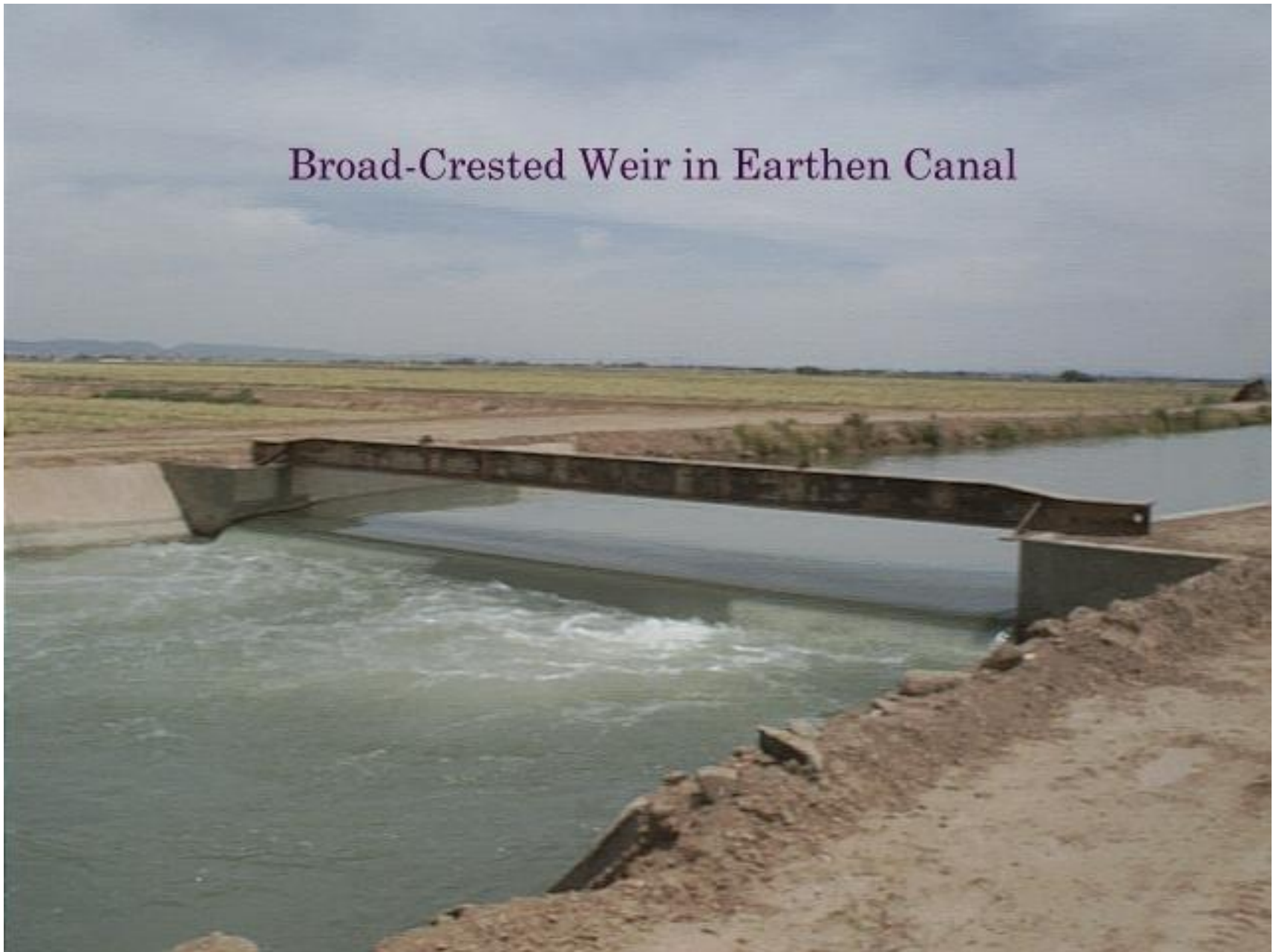
This work has been funded by the U.S. Bureau of Reclamation's  
Water Conservation Field Services Program.



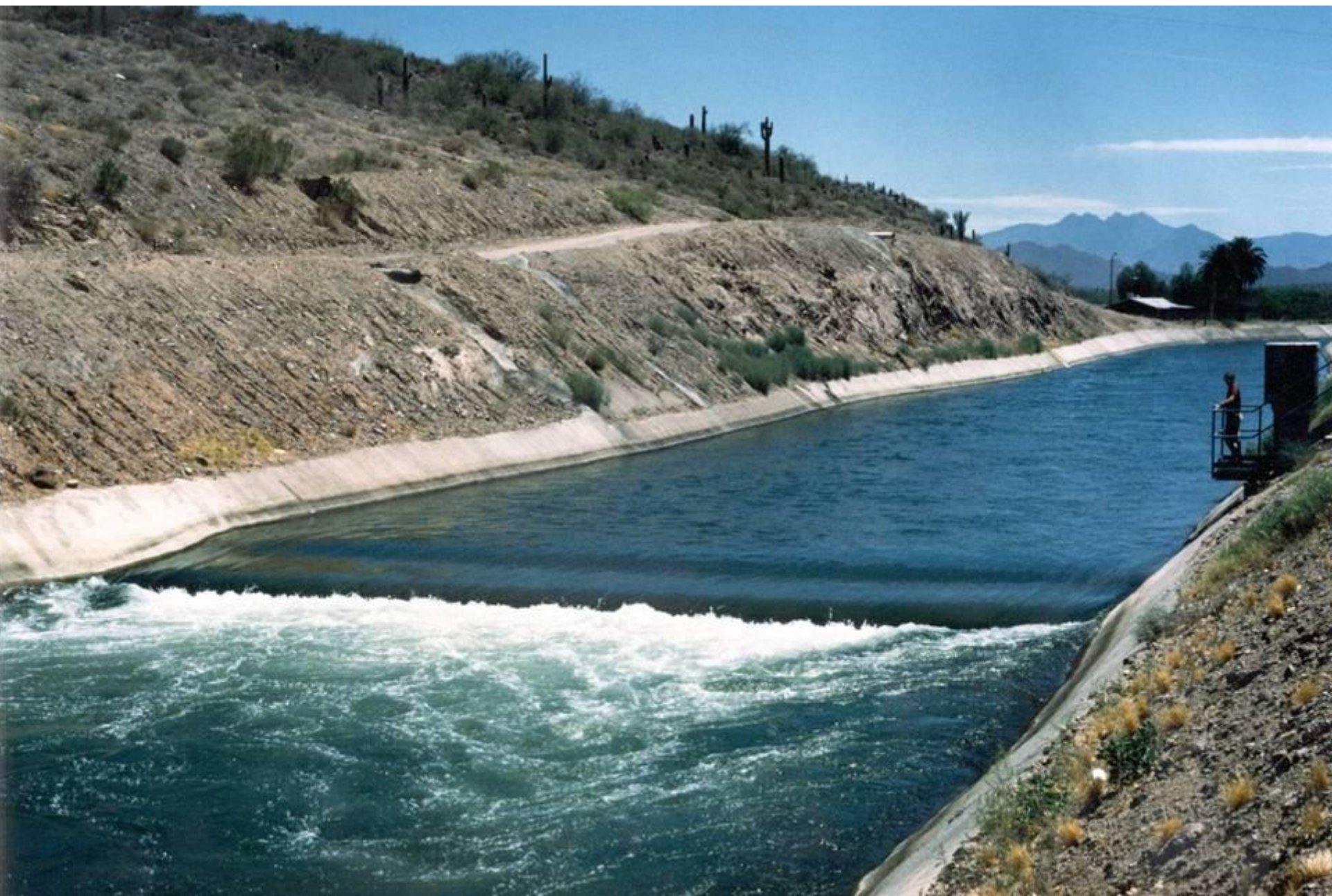
## Broad-Crested Weir in Concrete Lined Canal



## Broad-Crested Weir in Earthen Canal















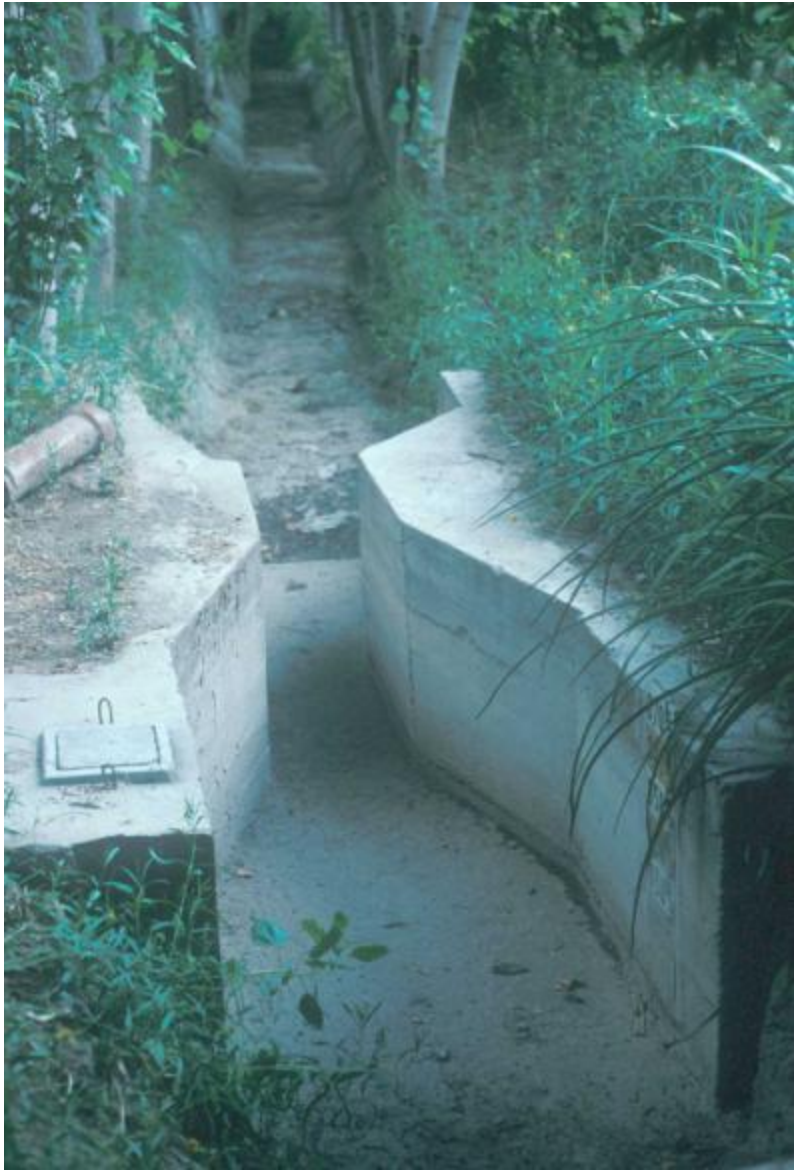














# Portable rectangular-throated flumes of fiberglass and metal







Portable plywood flumes  
for temporary  
measurements in larger  
ditches



12-inch Adjust-A-Flume in USBR lab





Large Adjust-A-Flume...portable if you have enough people



# Temporary plywood flume in concrete-lined ditch





































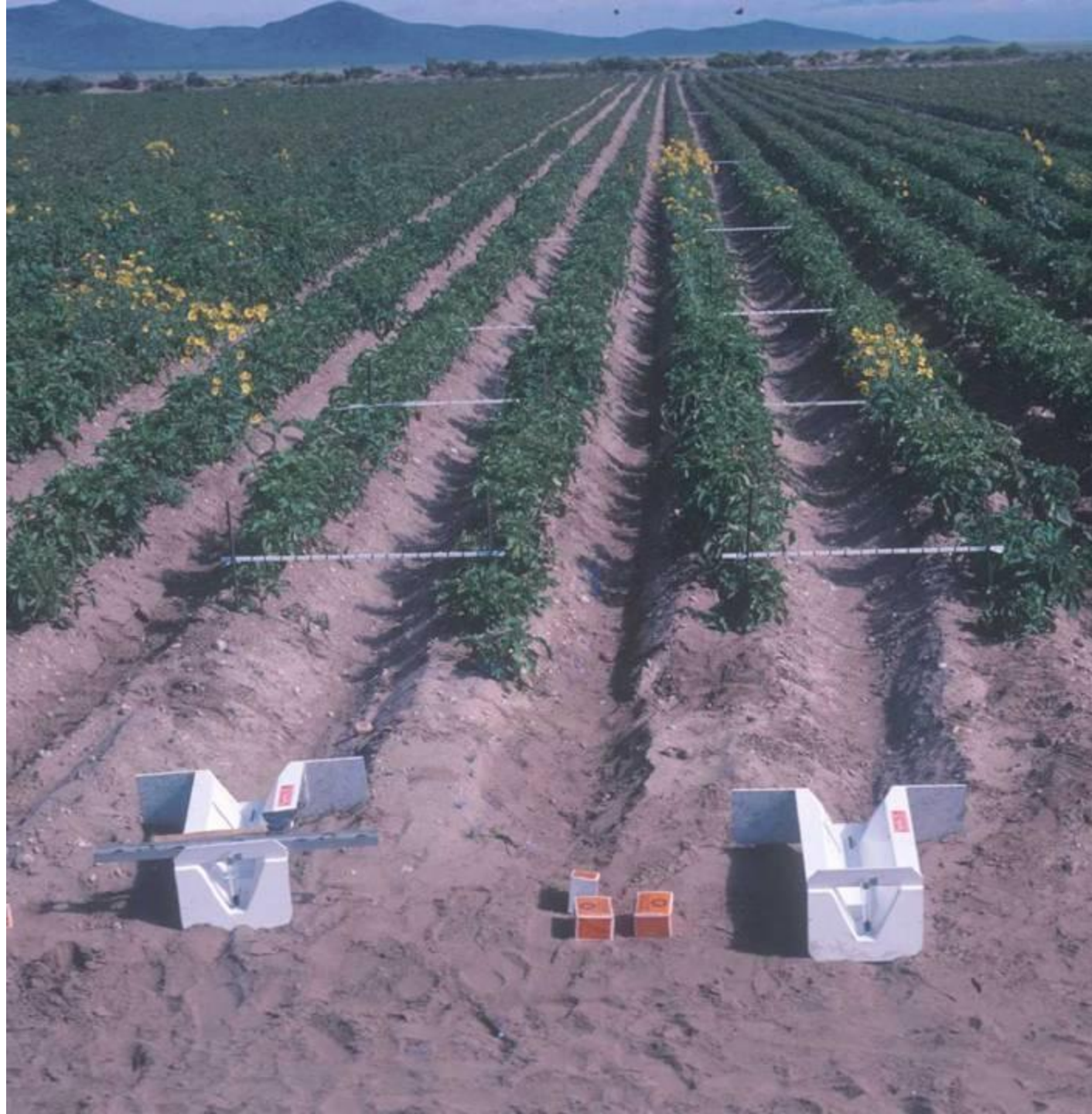
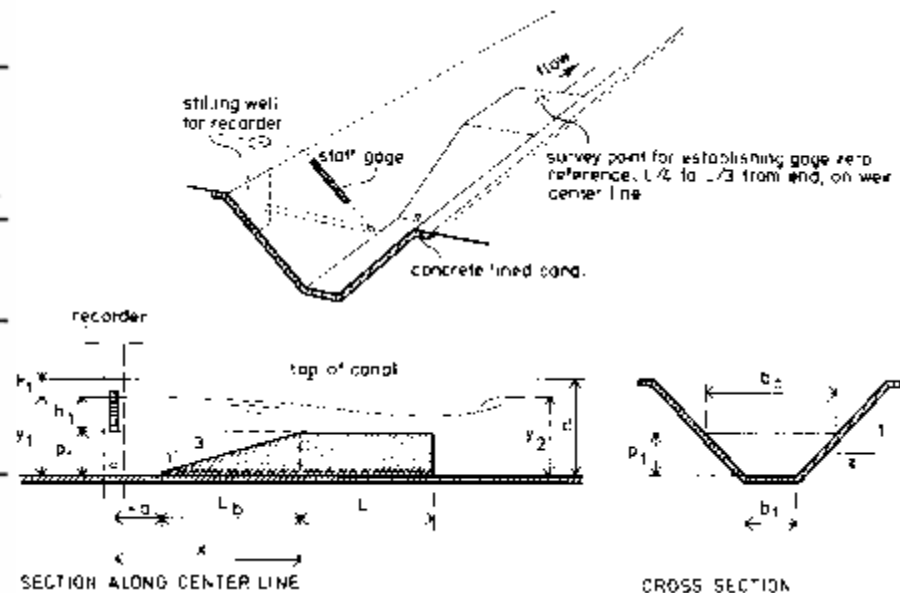


Table 8-2. — Long-throated flume sizes and discharge ranges for lined trapezoidal canals (English units)<sup>a</sup>

Canal Shape		Maximum canal depth <sup>b</sup> , $d$ (ft)	Range of Canal Capacities		Weir selection (table 8-3)	Weir Dimensions		Minimum head loss, $\Delta H^*$ (ft)
Side slope $Z_1$	Bottom width, $b_1$ (ft)		$Q_{\min}^c$ (ft <sup>3</sup> /s)	$Q_{\max}$ (ft <sup>3</sup> /s)		Crest width, $b_c$ (ft)	Sill height, $p_1$ (ft)	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
1.0	1.0	2.5	1.9	8 <sup>d</sup>	A <sub>o</sub>	2.0	0.50	0.06
			4.2	16 <sup>d</sup>	B <sub>o</sub>	2.5	0.75	0.08
			4.8	19	C <sub>o</sub>	3.0	1.00	0.10
			5.6	15	D <sub>o</sub>	3.5	1.25	0.12
			6.2	11	E <sub>o</sub>	4.0	1.50	0.13
1.0	2.0	3.0	5.6	27 <sup>d</sup>	D <sub>o</sub>	3.5	0.75	0.10
			6.2	40	E <sub>o</sub>	4.0	1.00	0.12
			6.8	33	F <sub>o</sub>	4.5	1.25	0.14
			7.4	27	G <sub>o</sub>	5.0	1.50	0.15
			8.2	22	H <sub>o</sub>	5.5	1.75	0.16
1.25	1.0	3.0	5.0	19 <sup>d</sup>	I <sub>o</sub>	3.0	0.8	0.08
			6.4	35	J <sub>o</sub>	4.0	1.2	0.11
			7.6	26	K <sub>o</sub>	5.0	1.6	0.14
1.25	2.0	4.0	6.4	31 <sup>d</sup>	J <sub>o</sub>	4.0	0.8	0.10
			7.6	64 <sup>d</sup>	K <sub>o</sub>	5.0	1.2	0.13
			8.9	78	L <sub>o</sub>	6.0	1.6	0.16
			10.1	62	M <sub>o</sub>	7.0	2.0	0.18
			11.4	46	N <sub>o</sub>	8.0	2.4	0.20
1.5	2.0	4.0	8.	49 <sup>d</sup>	P <sub>o</sub>	5.0	1.00	0.11
			9.	82 <sup>d</sup>	Q <sub>o</sub>	6.0	1.33	0.13
			11.	86	R <sub>o</sub>	7.0	1.67	0.16
			12.	72	S <sub>o</sub>	8.0	2.00	0.18
			13.	60	T <sub>o</sub>	9.0	2.33	0.20
1.5	3.0	5.0	9.	66 <sup>d</sup>	Q <sub>o</sub>	6.0	1.00	0.12
			11.	108 <sup>d</sup>	R <sub>o</sub>	7.0	1.33	0.14
			12.	140 <sup>d</sup>	S <sub>o</sub>	8.0	1.67	0.17
			13.	160	T <sub>o</sub>	9.0	2.00	0.20
			14.	140	U <sub>o</sub>	10.0	2.33	0.22
			17.	98	V <sub>o</sub>	12.0	3.00	0.25



NOTES:

<sup>a</sup>  $L > \Delta H_{1\max}$ ;  $L_b = 2$  to  $3p_1$ ;  $x = L_s + L_b > 2$  to  $3H_{1\max}$

$L > 1.5H_{1\max}$

$d > 1.2h_{1\max} + p_1$

$\Delta H > 0.1H_1$

<sup>b</sup> Maximum recommended canal depth

<sup>c</sup> Limited by sensitivity

<sup>d</sup> Limited by Froude number; otherwise limited by canal depth

\* Calibrations developed with WinFlume and the preceding computer models.



Table 8-3. — Rating equation parameters and ranges of application for flat-crested, long-throated flumes in lined trapezoidal canals<sup>a</sup>

Parameters	Weir A <sub>o</sub>	Weir B <sub>o</sub>	Weir C <sub>o</sub>	Weir D <sub>o</sub>	Weir E <sub>o</sub>	Weir F <sub>o</sub>	Weir G <sub>o</sub>
$K_1$	9.29	10.53	11.99	13.73	14.51	16.18	17.83
$K_2$	0.03	0.04	0.033	0.035	0.053	0.035	0.026
$U$	1.878	1.883	1.822	1.824	1.855	1.784	1.725
$h_1$ , min.	0.12	0.14	0.125	0.13	0.19	0.175	0.16
$h_1$ , max.	0.92	1.22	1.25	1.4	1.69	1.45	1.24
$Q$ , min.	0.26	0.42	0.42	0.51	1.05	1.00	0.98
$Q$ , max.	8.44	16.3	18.9	26.5	40.7	32.8	26.8

Parameters	Weir H <sub>o</sub>	Weir I <sub>o</sub>	Weir J <sub>o</sub>	Weir K <sub>o</sub>	Weir L <sub>o</sub>	Weir M <sub>o</sub>	Weir N <sub>o</sub>
$K_1$	19.44	12.81	15.34	17.13	20.17	23.62	27.17
$K_2$	0.017	0.034	0.055	0.075	0.06	0.044	0.026
$U$	1.674	1.868	1.897	1.907	1.845	1.766	1.692
$h_1$ , min.	0.15	0.125	0.185	0.254	0.228	0.205	0.19
$h_1$ , max.	1.05	1.19	1.485	1.904	2.007	1.675	1.34
$Q$ , min.	0.97	0.41	1.02	2.06	2.03	2.05	2.01
$Q$ , max.	21.7	18.7	34.8	63.60	77.0	61.5	46.0

Parameters	Weir P <sub>o</sub>	Weir Q <sub>o</sub>	Weir R <sub>o</sub>	Weir S <sub>o</sub>	Weir T <sub>o</sub>	Weir U <sub>o</sub>	Weir V <sub>o</sub>
$K_1$	18.95	20.96	23.94	25.61	28.13	31.29	38.44
$K_2$	0.05	0.07	0.056	0.072	0.072	0.062	0.034
$U$	1.874	1.906	1.856	1.866	1.841	1.8	1.709
$h_1$ , min.	0.162	0.225	0.21	0.25	0.275	0.3	0.3
$h_1$ , max.	1.6	2.0	2.2	2.5	2.5	2.25	1.7
$Q$ , min.	1.0	2.0	2.1	3.1	4.0	5.0	5.9
$Q$ , max.	48.4	83.9	108	149	160	141	98.5

<sup>a</sup> Calibrations developed with WinFlume and preceding computer models.

$$Q = K_1(h_1 + K_2)^U$$

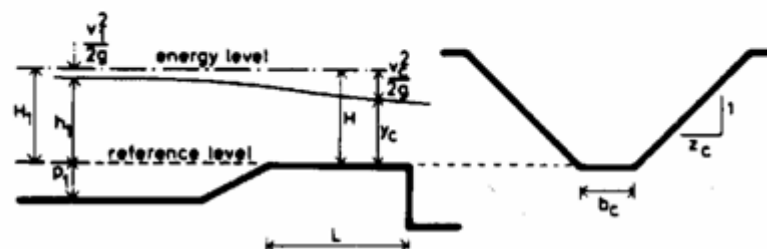
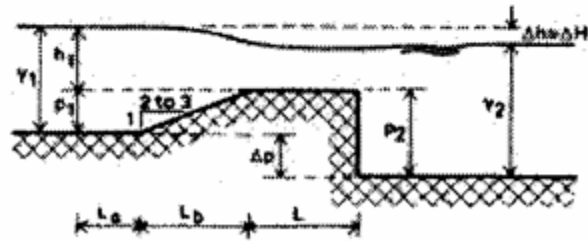
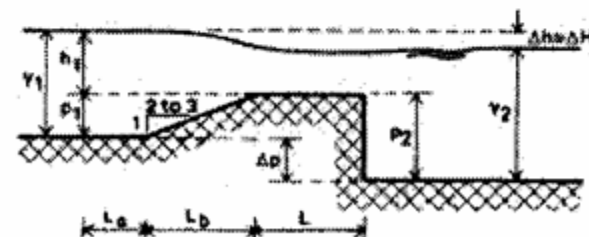


Table 8-4. — Rating equation parameters and ranges of application for flat-crested, long-throated flumes with rectangular throat sections (see Figure 8-6).

$q = K_1(h_1 + K_2)^U$  where  $q$  is the unit discharge in cubic feet per second per foot of width of the throat.

$$Q = qb_c$$

$Q = qh_c$									
Parameters	$0.35 \leq b_c \leq 0.65$ ft, $L = 0.75$ ft			$0.65 \leq b_c \leq 1.0$ ft, $L = 1.0$ ft			$1.0 \leq b_c \leq 1.5$ ft, $L = 1.5$ ft		
	$p_1 = 0.125$ ft	$p_1 = 0.25$ ft	$p_1 = \infty$	$p_1 = 0.25$ ft	$p_1 = 0.5$ ft	$p_1 = \infty$	$p_1 = 0.25$ ft	$p_1 = 0.5$ ft	$p_1 = \infty$
$K_1$	3.996	3.610	3.126	3.696	3.385	3.089	3.686	3.400	3.059
$K_2$	0	0	0	0.004	0	0	0	0	0
$U$	1.612	1.581	1.526	1.617	1.562	1.518	1.598	1.569	1.515
$h_1$ , range	0.06 – 0.46	0.06 – 0.48	0.05 – 0.5	0.08 – 0.7	0.8 – 0.7	0.08 – 0.8	0.1 – 0.9	0.1 – 1.0	0.1 – 1.0
$q$ , range	0.04 – 1.15	0.04 – 1.14	0.03 – 1.08	0.07 – 2.1	0.07 – 1.95	0.07 – 1.8	0.09 – 3.1	0.09 – 3.4	0.09 – 3.1
$\Delta H$	0.04	0.06	0.19	0.06	0.10	0.26	0.07	0.11	0.67
Parameters	$1.5 \leq b_c \leq 3.0$ ft, $L = 2.25$ ft				$3.0 \leq b_c \leq 6.0$ ft, $L = 3.0$ ft				
	$p_1 = 0.25$ ft	$p_1 = 0.5$ ft	$p_1 = 1.0$ ft	$p_1 = \infty$	$p_1 = 0.5$ ft	$p_1 = 1.0$ ft	$p_1 = 1.5$ ft	$p_1 = \infty$	
$K_1$	3.662	3.375	3.19	3.036	3.362	3.169	3.167	3.027	
$K_2$	0.008	0.011	0.009	0	0.013	0.013	0	0	
$U$	1.643	1.625	1.587	1.514	1.636	1.605	1.557	1.519	
$h_1$ , range	0.15 – 1.0	0.15 – 1.5	0.15 – 1.5	0.15 – 1.5	0.21 – 1.84	0.22 – 1.93	0.21 – 1.98	0.2 – 2.04	
$q$ , range	0.18 – 3.2	0.17 – 6.6	0.17 – 6.1	0.17 – 5.6	0.29 – 9.24	0.29 – 9.28	0.29 – 9.26	0.26 – 9.24	
$\Delta H$	0.07	0.13	0.2	0.5	0.13	0.22	0.29	0.63	
Parameters	$b_c \geq 6.0$ ft, $L = 4.0$ ft								
	$p_1 = 1.0$ ft	$p_1 = 1.5$ ft	$p_1 = 2.0$ ft	$p_1 = \infty$					
$K_1$	3.125	3.150	3.105	2.999					
$K_2$	0.017	0.016	0	0					
$U$	1.621	1.575	1.563	1.521					
$h_1$ , range	0.3 – 3.0	0.3 – 2.6	0.3 – 2.64	0.3 – 3.0					
$q$ , range	0.48 – 19	0.48 – 14.2	0.48 – 14.2	0.48 – 16					
$\Delta H$	0.25	0.33	0.40	0.85					



$L_a = h_{1max}$  and  $L_b = 2$  to 3 times  $p_1$  and  $L_a + L_b = 2$  to 3 times  $h_{1max}$

$\Delta H = 0.1H_1$ , or value listed, whichever is greater, for flumes discharging into a rectangular tailwater channel of the same width as the crest,  $b_c$

$\Delta H = 0.4H_1$ , or value listed, whichever is greater, for flumes with an abrupt expansion into a tailwater channel wider than the crest width,  $b_c$

Table 8-5. — Equation and flow range parameters for flat-crested, long-throated flumes in partially full circular conduits ( $K_1$  and  $K_2$  values are valid for units of feet and  $\text{ft}^3/\text{s}$  only).

$p_1/D$	$L_a/D$	$L_p/D$	$L/D$	$K_1$	$K_2$	$U$	range of $h_1/D$	range of $Q/D^{5/2}$	$b_1/D$
0.20	0.50	0.60	0.700	4.176	0.007	1.750	0.080 - 0.43	0.056 - 0.980	0.800
0.25	0.60	0.75	1.125	3.970	0.004	1.689	0.070 - 0.60	0.048 - 1.689	0.866
0.30	0.55	0.90	1.050	3.780	0	1.625	0.070 - 0.55	0.050 - 1.434	0.917
0.35	0.50	1.05	0.975	3.641	0	1.597	0.065 - 0.50	0.046 - 1.202	0.954
0.40	0.45	1.20	0.900	3.507	0	1.573	0.060 - 0.45	0.042 - 0.991	0.980
0.45	0.40	1.35	0.825	3.378	0	1.554	0.055 - 0.40	0.037 - 0.807	0.995
0.50	0.35	1.50	0.750	3.251	0	1.540	0.050 - 0.35	0.032 - 0.640	1.000

Pregage distance,  $L_{pg} \geq h_{max}$

Approach,  $L_a \geq h_{max}$

Converging,  $L_{cv} = 3p_1$

Control,  $L_c \geq 1.5D - p_1$

$\Delta H = 0.1H_1$  for flumes with a 6:1 downstream transition

$\Delta H = 0.2H_1$  for flumes with a vertical drop downstream from the crest

Sill height =  $p_1$

Dimensionless sill height =  $p_1/D$

$h_{min} = 0.07D$

$h_{max} = [0.85D - p_1]$

$$Q = D^{2.5} K_1 \left( \frac{h_1}{D} + K_2 \right)^U$$

Note: The length values shown are minimum lengths in direction of flow, and may be increased 30 percent with only a slight change in calibration.

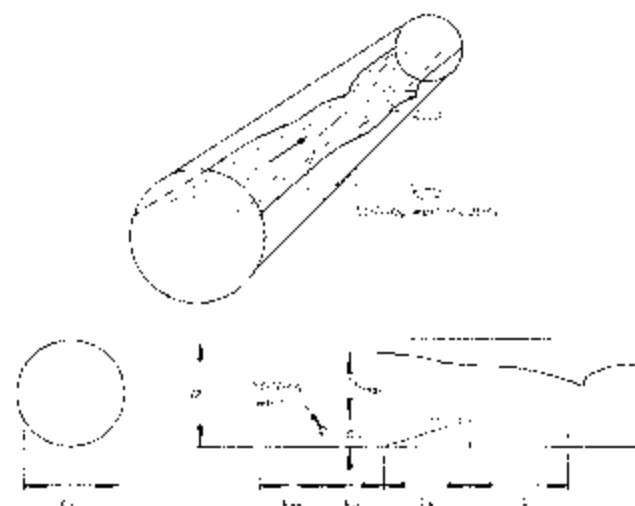


Figure 8-7.—Long-throated flume in a partially full circular conduit.