

Attachment 2.05.4(2)(e)-7

NRCS and WFC Provided

Sideroll Irrigation Designs - Irrigated Cropland

Note: In this attachment the irrigation design for the Morgan fields to be replaced as irrigated cropland (IC) in the post-mine condition. Details of the irrigation layouts can be seen on Map 2.05.4-5. The agreement for irrigation shares to be provided by the Morgans is also part of this attachment.

These irrigation design worksheets are from the Colorado Irrigation Guide and National Engineering Handbook Sec. 15, Chap. 11.



RETURN RECEIPT REQUESTED

Western Fuels-Colorado
P.O. Box 628
Nucla, Colorado 81424

Telephone 970/864-2165
Fax 970/864-2168

April 28, 2010

Mr. and Mrs. Frank Morgan
P.O. Box 4
Nucla, CO 81424

Mike Morgan and JoEllen Turner
P.O. Box 346
Nucla, CO 81424

RE: Reclamation of Morgan Property

Mr. and Mrs. Frank Morgan, Mike Morgan and JoEllen Turner:

Western Fuels-Colorado, LLC (WFC) is returning as you requested the signed original agreement for additional water shares for the post mining reclamation of the Morgan's land.

We noticed that the executed agreement you tendered was not signed by Jo Ellen Turner or by M & M Custom Farming. We are executing this agreement in the good-faith belief that it is binding upon those parties as well, and it is our intent in signing this letter that those parties are also bound by this agreement.

Sincerely,

R. Lance Wade

Mine Manager

Enclosure

XC: Duane Richards w/Enclosure

Christopher Kamper w/Enclosure

Return Signed copy Required

Morgan Lease Agreement

April 19, 2010

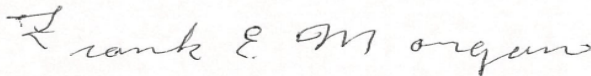
Page 2 of 2

Lessor agrees to lease 50 shares of CCC water and an additional 12 shares, for a total of 62 shares of CCC water to WFC for reclamation on the Morgan property. The ENTIRE 140 acres minus the 25 acres will be returned to irrigated crop production. 62 shares is sufficient to irrigate all the acres on the Morgan Property being mined. Since Michael Morgan and JoEllen Turner will be doing the irrigating, if for any reason this amount of water is not enough, the Morgans will make sure there is more water if needed. This will be determined by 50 years of experience irrigating the place and the Morgans calculations of what is needed. This 62 shares will not be used on property other than Morgans and for no other purpose other than reclamation of this prime farmland.

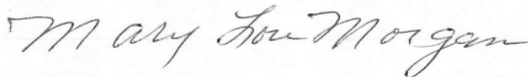
Lance Wade, Mine Manager



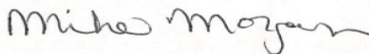
Frank Morgan



Mary Lou Morgan



Mike Morgan



FLOOD IRRIGATION DESIGN WORKSHEET

Project Name: Morgan - Sunshine Corner

Designer: _____ Reviewed by: _____

PRELIMINARY DATA:Design Crop: AlfalfaSoil Name: BerxTown: Nuck

Actual Field dimension
 $1290' \times 770' = 22.8 \text{ ac}$
 $11 \text{ hr} \text{ @ } 2 \text{ sets/day @ } 15 \text{ day}$

 $212 \text{ gpm} = 0.47 \text{ cfs}$
Root Depth: 4 ft. (2)Moisture Extraction: 4 ft (3)AVERAGE WATER HOLDING CAPACITY
(CIG 2-C)Soil Depth
in feet AWC
inches

1 st	_____
2 nd	_____
3 rd	_____
4 th	_____

TOTAL AVAILABLE WATER (TAW)*
 Recommendation from NRCS 4.0" (grass) & 7.6" on Morgan Prime Farmland soils (4)

total only to moisture extraction depth.

Management Allowance

Deficiency (Table CO 684.2) _____ 50 % (5)

IRRIGATION NET APPLICATION:

= % OF Total TAW

(4) x (5) (Decimal) = (7.6) x (50%)Net. App. = () in. (6) 3.8 in.

DAILY PEAK CONSUMPTIVE USE RATE: .21 for grass & .25 for alfalfa in/day
(CO683.52)

IRRIGATION FREQUENCY:

$$= \frac{(\text{Net Application}) \quad (6)}{\text{Daily Peak Consumptive Use} \quad (7)} = \frac{(3.8)}{(.25)}$$

$$= \text{days return period} \quad (7) \quad \underline{15.2} \text{ days (round down)} = \underline{15} \quad (7)$$

IRRIGATION GROSS APPLICATION

DESIGN FIELD EFFICIENCY (50-60% FOR CORRUGATE FLOOD IRRIGATION)
(CO685.69) 55 % (8)

GROSS APPLICATION.

$$= \frac{\text{NET App.} \quad (6)}{\text{Field Eff. \%} \quad (8)} \times 100 = \frac{(3.8) \times 100}{(55) \%}$$

$$= \underline{6.9} \text{ in.} \quad (9)$$

MAX HOURLY WATER APPLICATION RATE:

MAX APP Rate w/cover
(CIG Table 6-D-1, CIG Sec 2-C) 1.0 in/hr (10)

SET TIME: 11 HR (11)

Normally 11 or 23 hrs/set.... (11hr) for flood irrigation is recommended by NRCS)

CHECK POSSIBLE HOURLY APPLICATION RATES

$$= \frac{\text{Gr. App. In.} \quad (9)}{\text{Set time} \quad (11)} = \frac{(6.9)}{(11)}$$

$$= \text{Hourly App. Rate} = \underline{0.63} \text{ in/hr*} \quad (12)$$

USE 6.9 in. Gross App. On 11 hr. Sets

NUMBER OF SETS PER DAY:

$$= 24 / (11)$$

$$= 24 / 11$$

$$= 2.2 \text{ (rounded down)} = 2 \text{ (13)}$$

Dimension of field to be Furrow Irrigated:

Actual Length: 770 ft

L = row length, feet (NRCS recommends 400-600ft)... use: 770 ft (14)

Width: 1290 ft (15)

Length of set per day (ft)

$$\begin{aligned} \text{LNS} &= \frac{\text{Width}}{(\text{Frequency} \times \text{sets per day})} = \frac{(15)}{(7) \times (13)} = \frac{\frac{1290}{(15)}}{(15) \times (2)} = \\ &= 43 \text{ ft use : } 43 \text{ ft (17)} \end{aligned}$$

R = width between wetting furrows, feet (30 inch or 2.5ft) (19)

Number of furrows or pipe gates

$$N = \text{Number of Gates} = \frac{(\text{LNS})}{R} = \frac{(17)}{(19)} = \frac{(43)}{(25)} = \frac{17.2}{\text{USE } 17} \text{ (18)}$$

A = area in acres of each wetting furrow

$$A = \frac{(\# \text{ gates}) \times R \times L}{43560} = \frac{(18) \times (19) \times (14)}{43560} = \frac{(17) \times (2.5) \times (170)}{43560} = 0.75 \text{ ac } (16)$$

Q= Volume of irrigation water to fulfill design (gallon per minute)

$$Q = \frac{\text{Gross Irrigation Application} \times 450 \times A}{T}$$

$$= \frac{(9) \times 450 \times (16)}{(11)} = \frac{(6.9) \times 450 \times (0.75)}{(11)} \text{ gpm} = 212 \text{ gpm}$$

450 is a conversion constant:

$$450 \text{ gpm} = 1 \text{ acre-inch/hr}$$

SYSTEM EFFICIENCY (maintenance, cleaning head gate, checking water, farmer needed time off) ... = 100% (23)

(NRCS states numerous farmers in the Norwood area do not take a day off, so 100% as seen on NRCS design for side roll sprinkler design that DRMS approved)

AREA WORKSHEET
MARCH 1993

SIDEROLL SPRINKLER DESIGN WORKSHEET

Based on (Old and New) Colorado Irrigation Guide and
National Engineering Handbook Sec. 15, Chap. 11

Project Name: Morgan's N 1/2 Sec 1 T46N R16W
Designer: Jim Boyd Date: 2-12-10
Field #: 1 Checked by: _____ Date: _____

PRELIMINARY DATA:

DESIGN CROP: Alfalfa Use crop with greatest water needs.
SOIL NAME: Borx Fine Sandy Loam
TOWN: Nuclea

SPRINKLER LATERAL SLOPE [S]: 0 % "+" for downhill slope, "-" for uphill slope

MINIMUM PRESSURE 40 psi available for sideroll [P]

FIELD DIMENSIONS LENGTH 840 (720) ft. [L] (mainfold or mainline direction)

WIDTH 1320 (1320) ft. [W] (sideroll direction)

SOILS INFORMATION:

DESIGN GROUP 12
(CIG Section 2B)

MAX SPRINKLER APP. RATE 0.5 inch/hr. [1]
(CIG Section 2-C, CIG Table 6-D-1, Table CO685.70)

ROOT DEPTH 4 ft. [2]
(Attached table 11-2 or Table CO684.2)

MOISTURE EXTRACTION DEPTH (Table CO684.2) 4 ft. (max 5 ft.) [3]

* Assume reclaimed soil depth = 4 ft.

AVERAGE WATER
HOLDING CAPACITY
(CIG 2-C)

Soil Depth*
in feet
1st
2nd
3rd
4th
5th

AWC
inch

2.0
2.0
1.8
1.8
1.8

} 7.6 inches

TOTAL AVAILABLE WATER (TAW)*
*Total only to moisture extraction depth.

7.6 in. [4] round off.

Alfalfa
OPTION 1

OPTION 2

MANAGEMENT ALLOWED
DEFICIENCY (Table CO684.2) 50 % [4] _____ % [5]

IRRIGATION
NET APPLICATION:

= % of TOTAL TAW

[4] X [5] (Decimal) = (7.6) x (.5) () x ()

NET. APP. = () in. [6] 3.8 in. _____ in.

DAILY PEAK
CONSUMPTIVE
USE RATE
(CO683.52)

0.25 in/day _____ in/day [Up]

IRRIGATION FREQUENCY:

= (Net Application) [6]
(Daily Peak Consump-
tive Use) [Up]

(3.8)
(0.25)

()
()

= days return period [7] 15 days _____ days

IRRIGATION
GROSS APPLICATION:

DESIGN FIELD EFFICIENCY
(CO685.69) 70 % [8]

GROSS APP.

OPTION 1

OPTION 2

$$= \frac{\text{Net App.}}{\text{Field Eff. \%}} \times 100 \quad [6] \quad \frac{(3.8)}{(.7)} \times 100 \quad [8] \quad \frac{(\quad)}{(\quad)} \times 100$$

$$= \underline{5.4} \text{ in. [9]} \quad \underline{\quad} \text{ in. [9]}$$

MAX HOURLY WATER
APPLICATION RATE:

MAX APP. RATE W/COVER
(CIG Table 6-D-1, CIG Sec 2-C) 1.0 in/hr. [10]

SET TIME

Trail 1

Trail 2

Trial 3

Trial 4

Normally 11
or 23 hrs./set

11 hrs [11] 23 hrs hrs hrs

CHECK POSSIBLE HOURLY
APPLICATION RATES*

$$= \frac{\text{Gr. app. in. [9]}}{\text{Set time [11]}} \quad (= \frac{5.4}{12}) \quad (\frac{5.4}{23}) \quad \frac{(\quad)}{(\quad)} \quad \frac{(\quad)}{(\quad)}$$

$$= \text{Hourly App. Rate} = \underline{0.45} \text{ in/hr* [12]} \quad \underline{0.24} \text{ in/hr*} \quad \underline{\quad} \text{ in/hr*} \quad \underline{\quad} \text{ in/hr*}$$

USE 5.4 in. Gross App. on 12 hr. Sets

*Must not exceed MAX APP. RATE W/COVER [10]

SIDEROLL SPACING:

S_m shall not exceed 65% of Sprinkler Wetted diameter (D)
 S_l shall not exceed 50% of Sprinkler Wetted diameter (D)

Considering up to 5 mph wind use $S_m=60\%$ of (D), $S_l=50\%$ of (D)

SPRINKLER SET SPACING

(Assume 60ft design spacing with 100 ft wetted diameter) 60 ft [S_m]

SPACING OF NOZZLE ALONG LATERAL

(Assume 40ft design spacing with 100 ft wetted diameter) 40 ft [S_l]

NUMBER DAYS TO IRRIGATE
WITH 1 SIDEROLL

* 12 hour sets but only one per day per sideroll ≤ 15 day return time

$$= \frac{(\text{Field Length } [L]) (\text{Set Time } [11] + 1 \text{ hr})}{[S_m] \times (24)} = \frac{(720) (6.5)}{(60) \times (24)} = \frac{(840)}{(60) \times (24)} = \frac{(7.6)}{(15)} \text{ days } [13]$$

NUMBER SIDEROLLS NEEDED = $\frac{\# \text{ days one sideroll } [13]}{\text{irrigation frequency } [7]}$

$$= \frac{(7.6)}{(15)} = 0.5, \text{ round to } \underline{1} \text{ siderolls } [14]$$

REQUIRED SPRINKLER HEAD CAPACITY:

Flow at Nozzle = $\frac{\text{Hourly App. Rate } [12] \times (S_m) \times (S_l)}{96.3 \text{ (conversion factor)}}$

$$= \frac{(0.45) \times (60) \times (40)}{96.3} \approx \underline{11.2} \text{ gpm } [15]$$

SPRINKLER NOZZLE COVERAGE:

Select Nozzle from Catalogs with
given pressure
required head capacity

$$\underline{35} \text{ psi } [P]$$
$$\underline{11.2} \text{ gpm } [15]$$

Start with nozzle selection with a 100ft \pm 5ft Wetted Diameter.

SELECTION:

MAKE
SIZE
FLOW
PSI@NOZZLE
DIA

Rain Bird
 $7/32" \times 1/8"$
11.1
35
75

in.
gpm [16]
psi [DP]
ft.

MODEL

30 PSH - 3/4"
(1/8" spreader)

Design Pressure

SIDEROLL LENGTH* [SRL] = Field Width [W] - 1 Spacing along lateral [S_1]

$$\begin{aligned} &= (1320) - 1 (40) \\ \text{SRL} &= \underline{1280} \text{ ft.} \end{aligned}$$

*Use multiples of 40 ft.

NUMBER HEAD REQ'D = $\frac{\text{SRL}}{S_1} + 1$

$$= \frac{(1280)}{(40)} + 1$$

$$= \underline{33} \text{ heads per sideroll [17]}$$

DETERMINE SIDEROLL HEADLOSS:

Spec. allows a variation of up to $\pm 10\%$ of the design pressure without special design.

MULTIPLE OUTLET FACTOR = 0.36 [F]
(Table CO685.72)

use # outlets per sideroll

LATERAL SIZE = Use 5 in. dia. *Aluminum Pipe*

FLOW per SIDEROLL = (# heads [17]) x (nozzle flow [16])

$$= (33) \times (11.1)$$

$$= \underline{366.3} \text{ gpm.}$$

$$\approx 0.82 \text{ cfs}$$

SIDEROLL HEADLOSS per 100LF =
(Table CO685.73)

for 40 ft. pipe lengths

$$\text{SIDEROLL LENGTH SRL} = \underline{2.7} \text{ ft./ 100 ft. [18]}$$

≈ 29.3 shares
CC-Ditch Water

SELECTION:

MAKE
SIZE
FLOW
PSI@NOZZLE
DIA

Rain Bird
 $7/32" \times 1/8"$
 11.1
 35
 75

in.
gpm [16]
psi [DP]
ft.

MODEL

$30 PSH - 3/4"$
 $(1/8" \text{ spreader})$

Design Pressure

SIDEROLL LENGTH* [SRL] = Field Width [W] - 1 Spacing along lateral [S_1]

$$= (1320) - 1 (40)$$
$$SRL = \underline{1280} \text{ ft.}$$

*Use multiples of 40 ft.

NUMBER HEAD REQ'D

$$= \frac{SRL}{S_1} + 1$$

$$= \frac{(1280)}{(40)} + 1$$

$$= \underline{33} \text{ heads per sideroll [17]}$$

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FLOW per SIDEROLL

$$= (\# \text{ heads [17]}) \times (\text{nozzle flow [16]})$$

$$= (33) \times (11.1)$$

$$= \underline{366.3} \text{ gpm.} \approx 0.82 \text{ cfs}$$

SIDEROLL HEADLOSS per 100LF =
(Table CO685.73)

for 40 ft. pipe lengths

SIDEROLL LENGTH SRL = 2.7 ft./ 100 ft. [18]

$\approx 29.3 \text{ shares}$
CC-Ditch Water

TOTAL SIDEROLL
HEADLOSS
 with 5" Lateral

$$= \frac{(\text{Sideroll Length [SRL]}) \times (\text{Headloss [18]}) \times [F]}{(2.31) \times (100)}$$

$$\frac{(1280) \times (2.7) \times (0.36)}{2.31 \times 100} = 5.4 \text{ psi [19]}$$

PRESSURE GAIN (or LOSS) DUE
TO FIELD SLOPE

$$= \frac{[S]\% \times [SRL]}{2.31 \times 100} = \frac{(0) \times (1280)}{2.31 \times 100}$$

NOTE: Look at most
 restrictive conditions
 in an entire field.

$$= (-0-) \pm \text{psi [20] pressure due to elevation change}$$

PRESSURE VARIATION:

$$= \frac{\text{Sideroll Headloss [19]} + \text{Elev. pressure Gain or Loss [20]}}{[DP]}$$

$$= \frac{(5.4)}{(35)} + \text{or } - \frac{(-0-)}{(35)} \times 100 = (15.4)\%*$$

*PRESSURE VARIATION MUST NOT EXCEED $\pm 10\%$ of DP. If flow control nozzles are used, then $\pm 10\%$ pressure limit can be dealt with easily.

REQUIRED PRESSURE AT MAINLINE AT BEGINNING OF SIDEROLL [MPS]

For Level Laterals $= [DP] + 0.75 [19] + 1$
 $= 35 + 0.75 (5.4) + 1 = 40.4$

For Lateral Laid Downhill $= [DP] + 0.75 [19] - 0.5 [20] + 1$
 $= \underline{\hspace{1cm}} + 0.75 (\underline{\hspace{1cm}}) - 0.5 (\underline{\hspace{1cm}}) + 1 = \underline{\hspace{1cm}}$

For Laterals Laid Uphill
 (not recommended) $= [DP] + 0.75 [19] + 0.5 [20] + 1$
 $= \underline{\hspace{1cm}} + 0.75 (\underline{\hspace{1cm}}) + 0.5 (\underline{\hspace{1cm}}) + 1 = \underline{\hspace{1cm}}$

MANIFOLD LENGTH [ML] *

$$= \text{Field Length [L]} - (1) (S_m) \\ = (840) - (60) = 780 \text{ ft. [ML]}$$

NUMBER SETS

$$= \frac{ML}{S_m} + 1 = \frac{(780)}{(60)} + 1 = 14 \text{ sets per field}$$

*Use multiples of 60 ft. Note this length may be shorter if 60 ft. swing lines are used.

MAINLINE CAPACITY
(Manifold)

$$\text{MAINLINE CAP.} = \frac{(\# \text{head req'd [17]}) \times (\text{nozzle flow (gpm) [16]}) \times (\# \text{siderolls [14]})}{449}$$

$$= (33) \times (11.1) \times (1) \\ = 366.3 \text{ gpm} = \frac{366.3}{449} \text{ gpm} = 0.82 \text{ cfs}$$

or 29.3 shares cc-Ditch Water

TOTAL SIDEROLL PRESSURE REQUIRED:

$$\text{TOTAL PRESSURE REQUIRED} = \text{MPS} + \text{swing line loss} + \text{riser, hydrant and stub valve loss.} \\ = (40.4) + () + (2.0) + () + () \\ \text{TOTAL} = (42.4) \text{ psi req. at beginning of sideroll riser}$$

TOTAL SYSTEM PRESSURE REQUIREMENT:

$$= \text{Required sideroll pressure} + \text{Mainline pressure losses.}$$

Mainline pressure losses are found by using the pipeline computer program. Mainline losses should be checked at the beginning set and last set and any restrictive sets inbetween.

$$\text{TOTAL} = (42.4) + (2.0) \\ = 44.4 \text{ psi at beginning of system.}$$

FLOOD IRRIGATION DESIGN WORKSHEET

Project Name: Morgan - 12.9 ac TRIANGLE

Designer: _____ Reviewed by: _____

PRELIMINARY DATA:Design Crop: AlfalfaSoil Name: BerryTown: NucleRoot Depth: 4 ft. (2)Moisture Extraction: 4 ft (3)AVERAGE WATER HOLDING CAPACITY
(CIG 2-C)Soil Depth
in feet AWC
inches1st2nd3rd4thTOTAL AVAILABLE WATER (TAW)*Recommendation from NRCS 4.0" (grass) & 7.6" on Morgan Prime Farmland soils (4)

total only to moisture extraction depth.

Management Allowance
Deficiency (Table CO 684.2)50 % (5)IRRIGATION NET APPLICATION:

= % OF Total TAW

(4) x (5) (Decimal) = (7.6) x (50%)Net. App. = () in. (6) 3.8 in.

DAILY PEAK CONSUMPTIVE USE RATE: .21 for grass & .25 for alfalfa in/day
(CO683.52)

IRRIGATION FREQUENCY:

$$= \frac{(\text{Net Application}) \quad (6)}{\text{Daily Peak Consumptive Use}} \quad (3.8) \quad (.25)$$

$$= \text{days return period} \quad (7) \quad \underline{15.2} \text{ days (round down)} = \underline{15} \quad (7)$$

IRRIGATION GROSS APPLICATION

DESIGN FIELD EFFICIENCY (50-60% FOR CORRUGATE FLOOD IRRIGATION)
(CO685.69) 55 % (8)

GROSS APPLICATION.

$$= \frac{\text{NET App.} \quad (6)}{\text{Field Eff. \%} \quad (8)} \times 100 = \frac{(3.8) \times 100}{(55) \%}$$

$$= \underline{6.9} \text{ in.} \quad (9)$$

MAX HOURLY WATER APPLICATION RATE:

MAX APP Rate w/cover
(CIG Table 6-D-1, CIG Sec 2-C) 1.0 in/hr (10)

SET TIME: 11 HR (11)

Normally 11 or 23 hrs/set..... (11hr for flood irrigation is recommended by NRCS)

CHECK POSSIBLE HOURLY APPLICATION RATES

$$= \frac{\text{Gr. App. In.} \quad (9)}{\text{Set time} \quad (11)} = \frac{(6.9)}{(11)}$$

$$= \text{Hourly App. Rate} = \underline{0.63} \text{ in/hr*} \quad (12)$$

USE 6.9 in. Gross App. On 11 hr. Sets

NUMBER OF SETS PER DAY:

$$= 24 / (11)$$

$$= 24 / 11$$

$$= 2.2 \text{ (rounded down)} = 2 \text{ (13)}$$

$$\frac{1 - 11 \text{ hr set}}{\text{day}}$$

Dimension of field to be Furrow Irrigated:

Actual Length: 406 ft

L = row length, feet (NRCS recommends 400-600ft)... use: 406 ft (14)

Width: 1380 ft (15)

Length of set per day (ft)

$$\text{LNS} = \frac{\text{Width}}{(\text{Frequency} \times \text{sets per day})} = \frac{(15)}{(7) \times (13)} = \frac{(1380)}{(15) \times (2)} =$$

$$= 46 \text{ ft use : } 46 \text{ ft (17)}$$

R = width between wetting furrows, feet (30 inch or 2.5ft) (19)

Number of furrows or pipe gates

$$N = \text{Number of Gates} = \frac{(\text{LNS})}{R} = \frac{(46)}{(19)} = \frac{(46)}{(2.5)} = 18.4 \text{ GATES (18)}$$

USE 18

A = area in acres of each wetting furrow

$$A = \frac{(\# \text{ gates}) \times R \times L}{43560} = \frac{(18) \times (19) \times (14)}{43560} = \frac{(18) \times (2.5) \times (406)}{43560} = 0.42 \text{ ac (16)}$$

Q = Volume of irrigation water to fulfill design (gallon per minute)

$$Q = \frac{\text{Gross Irrigation Application} \times 450 \times A}{T}$$

$$= \frac{(9) \times 450 \times (16)}{(11)} = \frac{(6.9) \times 450 \times (4.2)}{(10)} \text{ gpm} = 112 \text{ gpm}$$

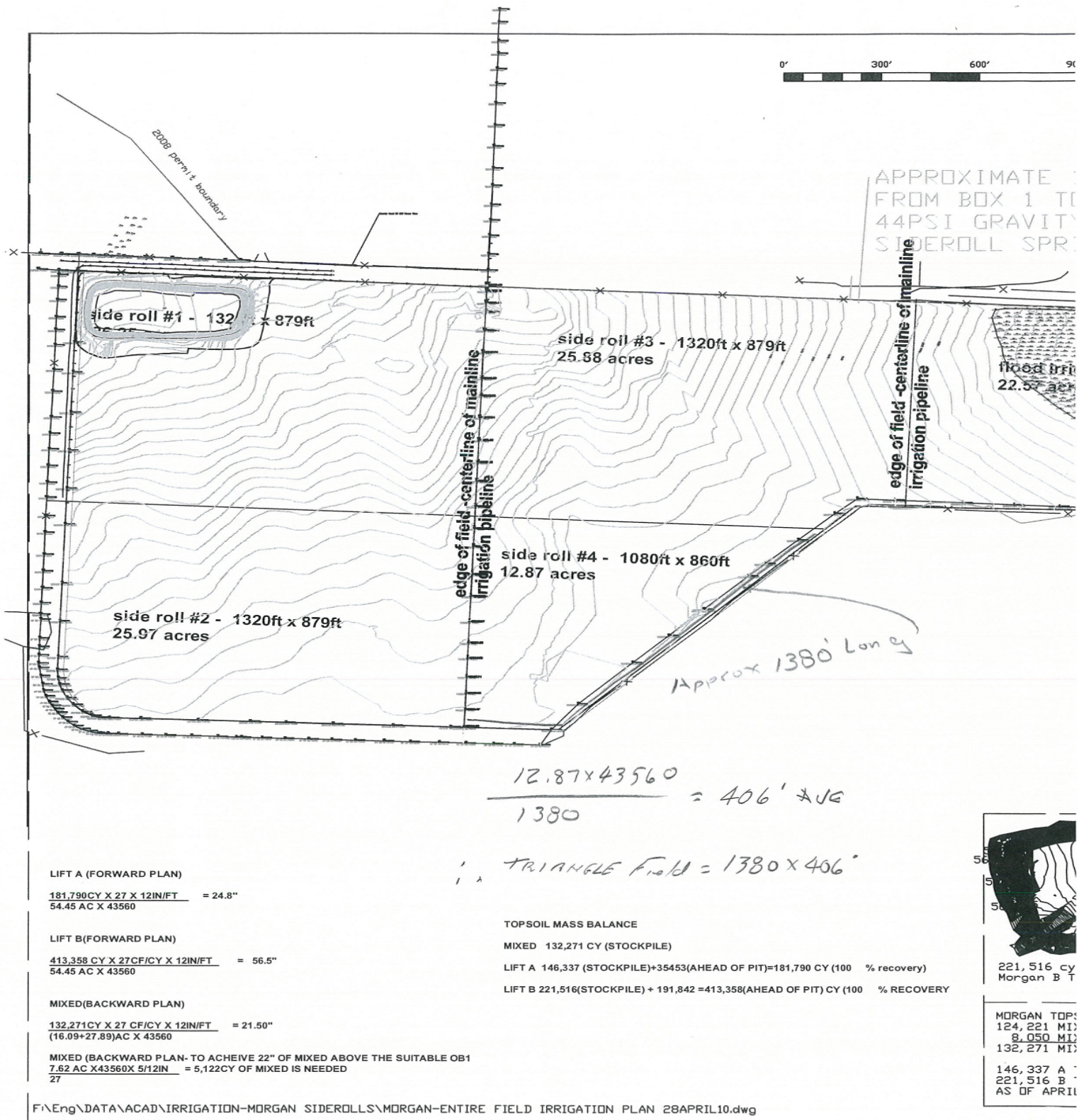
$$\approx 0.26 \text{ CFS}$$

450 is a conversion constant:

$$450 \text{ gpm} = 1 \text{ acre-inch/hr}$$

SYSTEM EFFICIENCY (maintenance, cleaning head gate, checking water, farmer needed time off) ... = 100% (23)

(NRCS states numerous farmers in the Norwood area do not take a day off, so 100% as seen on NRCS design for side roll sprinkler design that DRMS approved)





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Sincerely,

R. Lance Wade

Mine Manager

Enclosure

XC: Duane Richards w/Enclosure
Christopher Kamper w/Enclosure

Return Signed copy Required

Morgan Lease Agreement

April 19, 2010

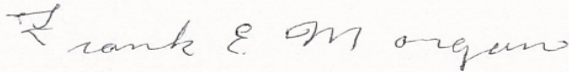
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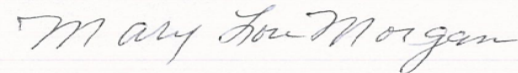
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Mike Morgan

