

**Attachment 2.05.3(3)-12**  
**Sediment Pond 012 Engineering Design**

Pond 012 was initially designed for the 2000 Permit Amendment. The pond was constructed in 2007. The as built report is included in attachment 2.05.3(3)-13. Due to changes in the planned post mine topography, Pond 012's post mine and pre mine drainage have to be compared.

### **Pond 012 - Design Confirmation**

Pond 012 is currently in place at New Horizon Mine. However, changes to the reclamation plan have altered the post mine drainage. The pre mine drainage area is 55.1 acres, while the post mine drainage area is 38.1 acres. Therefore the pre mine drainage will continue to be the worst case, and the design will remain unchanged.

#### Runoff Curve Number and Runoff

Project: POND 012 By: R . L. GUBKA

Location: NEW HORIZON MINE

Present

|             | CN | C | AREA         |
|-------------|----|---|--------------|
| UNDISTURBED | 80 | C | 12.152 Acres |
| DISTURBED   | 85 | C | 42.933 Acres |

CN (weighted): 84

CF (weighted): 0.500

#### 2. Runoff

Frequency ..... : 10 yr

Rainfall, P (24-hour) .. : 2.00 in

Runoff, Q ..... : 0.74 in

Runoff Volume ..... : 3.39 Acre-Ft

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Time of Concentration (SCS Method)

Curve Number: 84

Length of Flow (ft): 1354.62

Average Land Slope (°): 6.40

Time of Concentration (hrs): 0.23

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Pond Report

Top of dam elevation: 5610.0000

Bottom of pond elevation: 5603.0000

Top of dam width: 10.0000

Cut slope percent grade: 100.00, slope ratio: 1.00

Fill slope percent grade: 25.00, slope ratio: 4.00

Interior slope percent grade: 40.00, slope ratio: 2.50

Lower left grid corner : 1114657.98,601617.47

Upper right grid corner: 1117967.98,603397.47

X grid resolution: 331, Y grid resolution: 178

X grid cell size: 10.00, Y grid cell size: 10.00

Pond EarthWork Volumes

Total fill: 4,186.42 C.F., 155.05 C.Y.

Total cut : 500,392.33 C.F., 18,533.05 C.Y.

Pond Storage Volumes

| Water Elev | Storage(AcreFt) | (C.Y.) | (C.F.)   | Area(Acre) |
|------------|-----------------|--------|----------|------------|
| 5603.00    | 0.00000         | 0.0    | 0.0      | 0.515      |
| 5604.00    | 0.54061         | 872.2  | 23549.1  | 0.584      |
| 5605.00    | 1.14204         | 1842.5 | 49747.1  | 0.638      |
| 5606.00    | 1.78390         | 2878.0 | 77706.9  | 0.700      |
| 5607.00    | 2.48382         | 4007.2 | 108195.3 | 0.720      |
| 5608.00    | 3.22681         | 5205.9 | 140559.8 | 0.781      |
| 5609.00    | 4.02186         | 6488.6 | 175192.2 | 0.830      |
| 5610.00    | 4.86649         | 7851.3 | 211984.4 | 0.852      |

# **POND 012** **25YR-24HR EVENT**

***TOTALLY ENCISED TOP OF DAM AT 5610 AND BOTTOM OF  
5603,***

Ross L. Gubka, P.E.

## ***General Information***

### ***Storm Information:***

|                 |               |
|-----------------|---------------|
| Storm Type:     | NRCS Type II  |
| Design Storm:   | 25 yr - 24 hr |
| Rainfall Depth: | 2.400 inches  |

### ***Particle Size Distribution:***

| Size (mm) | NEW HORIZON<br>MINE 1<br>PARTIAL SIZE<br>DISTRIBUTION |
|-----------|---|
| 2.0000    | 100.000%  |
| 1.0000    | 70.000%   |
| 0.5000    | 67.000%   |
| 0.2500    | 58.000%   |
| 0.1250    | 52.000%   |
| 0.0630    | 38.000%   |
| 0.0160    | 21.000%   |
| 0.0040    | 11.000%   |

***Structure Networking:***

| Type | Stru<br># | (flows<br>into) | Stru<br># | Musk. K<br>(hrs) | Musk. X | Description |
|------|-----------|-----------------|-----------|------------------|---------|-------------|
| Pond | #1        | ==>             | End       | 0.000            | 0.000   |             |

#1  
Pond

***Structure Summary:***

|    |     | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|-----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | In  | 55.080                                    | 55.080                                | 33.02                      | 4.55                                 | 750.1              | 233,893                             | 141.94                                | 80.87          |
|    | Out |   |                                       | 2.33                       | 1.66                                 | 38.0               | 29,941                              | 0.00                                  | 0.00           |

***Particle Size Distribution(s) at Each Structure***

***Structure #1:***

| Size (mm) | In       | Out      |
|-----------|----------|----------|
| 2.0000    | 100.000% | 100.000% |
| 1.0000    | 91.478%  | 100.000% |
| 0.5000    | 87.557%  | 100.000% |
| 0.2500    | 75.796%  | 100.000% |
| 0.1250    | 67.955%  | 100.000% |
| 0.0630    | 49.659%  | 100.000% |
| 0.0160    | 27.443%  | 100.000% |
| 0.0040    | 14.375%  | 100.000% |



## Structure Detail:

### Structure #1 (Pond)

#### Pond Inputs:

|                      |            |
|----------------------|------------|
| Permanent Pool Elev: | 5,604.50   |
| Permanent Pool:      | 0.85 ac-ft |
| *Sediment Storage:   | 0.00 ac-ft |
| Dead Space:          | 20.00 %    |

*\*No sediment capacity defined*

#### Perforated Riser

| Riser Diameter (in) | Riser Height (ft) | Barrel Diameter (in) | Barrel Length (ft) | Barrel Slope (%) | Manning's n | Spillway Elev | Number of Holes per Elev |
|---------------------|-------------------|----------------------|--------------------|------------------|-------------|---------------|--------------------------|
| 18.00               | 5.00              | 18.00                | 100.00             | 0.01             | 0.0150      | 5,608.00      | 1                        |

#### Pond Results:

|                         |           |
|-------------------------|-----------|
| Peak Elevation:         | 5,608.23  |
| H'graph Detention Time: | 4.38 hrs  |
| Dewater Time:           | 0.58 days |
| Trap Efficiency:        | 94.93 %   |

*Dewatering time is calculated from peak stage to lowest spillway*

#### Elevation-Capacity-Discharge Table

| Elevation | Area (ac) | Capacity (ac-ft) | Discharge (cfs) | Dewater Time (hrs)  |
|-----------|-----------|------------------|-----------------|---------------------|
| 5,603.00  | 0.515     | 0.000            | 0.000           | Top of Sed. Storage |
| 5,603.50  | 0.549     | 0.266            | 0.000           |                     |
| 5,604.00  | 0.584     | 0.549            | 0.000           |                     |
| 5,604.50  | 0.611     | 0.848            | 0.000           | Low hole SPW #1     |
| 5,605.00  | 0.638     | 1.160            | 0.000           |                     |
| 5,605.50  | 0.669     | 1.487            | 0.000           |                     |
| 5,606.00  | 0.700     | 1.829            | 0.000           |                     |
| 5,606.50  | 0.710     | 2.181            | 0.000           |                     |
| 5,607.00  | 0.720     | 2.539            | 0.000           |                     |
| 5,607.50  | 0.750     | 2.906            | 0.000           |                     |
| 5,608.00  | 0.781     | 3.289            | 0.000           | Spillway #1         |
| 5,608.23  | 0.790     | 3.468            | 2.333           | 13.90 Peak Stage    |
| 5,608.50  | 0.805     | 3.686            | 5.165           |                     |
| 5,609.00  | 0.830     | 4.094            | 8.509           |                     |

| Elevation | Area<br>(ac) | Capacity<br>(ac-ft) | Discharge<br>(cfs) | Dewater<br>Time<br>(hrs) |
|-----------|--------------|---------------------|--------------------|--------------------------|
| 5,609.50  | 0.841        | 4.512               | 10.421             |                          |
| 5,610.00  | 0.852        | 4.935               | 12.033             |                          |

Detailed Discharge Table

| Elevation | Perf. Riser (cfs) | Combined<br>Total<br>Discharge<br>(cfs) |
|-----------|-------------------|---|
| 5,603.00  | 0.000             | 0.000                                   |
| 5,603.50  | 0.000             | 0.000                                   |
| 5,604.00  | 0.000             | 0.000                                   |
| 5,604.50  | 0.10>0.000        | 0.000                                   |
| 5,605.00  | 0.000             | 0.000                                   |
| 5,605.50  | 0.000             | 0.000                                   |
| 5,606.00  | 0.000             | 0.000                                   |
| 5,606.50  | 0.000             | 0.000                                   |
| 5,607.00  | 0.000             | 0.000                                   |
| 5,607.50  | 0.000             | 0.000                                   |
| 5,608.00  | 0.000             | 0.000                                   |
| 5,608.50  | 5.165             | 5.165                                   |
| 5,609.00  | 8.509             | 8.509                                   |
| 5,609.50  | 10.421            | 10.421                                  |
| 5,610.00  | 12.033            | 12.033                                  |

**Subwatershed Hydrology Detail:**

| Stru #   | SWS # | SWS Area (ac) | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|----------|-------|---------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1       | 1     | 42.930        | 0.148              | 0.148        | 0.299  | 84.000       | M   | 32.18                | 3.717                 |
|          | 2     | 12.150        | 0.044              | 0.044        | 0.302  | 80.000       | M   | 11.23                | 0.831                 |
| <b>Σ</b> |       | <b>55.080</b> |                    |              |        |              |     | <b>33.02</b>         | <b>4.547</b>          |

**Subwatershed Sedimentology Detail:**

| Stru #   | SWS # | Soil K | L (ft)   | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l)  |
|----------|-------|--------|----------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|--------------|
| #1       | 1     | 0.320  | 1,351.51 | 6.40  | 0.5000 | 1.0000 | 1    | 636.2           | 261,451                    | 160.43                      | 87.83        |
|          | 2     | 0.320  | 420.77   | 6.77  | 1.0000 | 1.0000 | 1    | 179.5           | 284,327                    | 184.92                      | 95.06        |
| <b>Σ</b> |       |        |          |       |        |        |      | <b>750.1</b>    | <b>233,893</b>             | <b>141.94</b>               | <b>80.87</b> |

**Subwatershed Time of Concentration Details:**

| Stru # | SWS # | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|--------|-------|---|-----------|------------------|-------------------|----------------|--------------|
| #1     | 1     | 5. Nearly bare and untilled, and alluvial valley fans | 6.40      | 86.45            | 1,351.51          | 2.520          | 0.148        |
| #1     | 1     | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.148</b> |
| #1     | 2     | 5. Nearly bare and untilled, and alluvial valley fans | 6.77      | 28.47            | 420.77            | 2.600          | 0.044        |
| #1     | 2     | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.044</b> |

**Subwatershed Muskingum Routing Details:**

| Stru # | SWS # | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|--------|-------|---|-----------|------------------|-------------------|----------------|--------------|
| #1     | 1     | 5. Nearly bare and untilled, and alluvial valley fans | 6.40      | 86.45            | 1,351.51          | 2.520          | 0.148        |
| #1     | 1     | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.148</b> |
| #1     | 2     | 5. Nearly bare and untilled, and alluvial valley fans | 6.77      | 28.47            | 420.77            | 2.600          | 0.044        |
| #1     | 2     | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.044</b> |

**POND 012**  
**10 YR-24HR EVENT**

***TOTALLY ENCISED TOP OF DAM AT 5610 AND BOTTOM OF  
5603,***

Ross L. Gubka, P.E.

## ***General Information***

### ***Storm Information:***

|                 |               |
|-----------------|---------------|
| Storm Type:     | NRCS Type II  |
| Design Storm:   | 10 yr - 24 hr |
| Rainfall Depth: | 2.000 inches  |

### ***Particle Size Distribution:***

| Size (mm) | NEW HORIZON<br>MINE 1<br>PARTIAL SIZE<br>DISTRIBUTION |
|-----------|---|
| 2.0000    | 100.000%  |
| 1.0000    | 70.000%   |
| 0.5000    | 67.000%   |
| 0.2500    | 58.000%   |
| 0.1250    | 52.000%   |
| 0.0630    | 38.000%   |
| 0.0160    | 21.000%   |
| 0.0040    | 11.000%   |

***Structure Networking:***

| Type | Stru<br># | (flows<br>into) | Stru<br># | Musk. K<br>(hrs) | Musk. X | Description |
|------|-----------|-----------------|-----------|------------------|---------|-------------|
| Pond | #1        | ==>             | End       | 0.000            | 0.000   |             |

|            |
|------------|
| #1<br>Pond |
|------------|

***Structure Summary:***

|    |     | Immediate<br>Contributing<br>Area<br>(ac) | Total<br>Contributing<br>Area<br>(ac) | Peak<br>Discharge<br>(cfs) | Total<br>Runoff<br>Volume<br>(ac-ft) | Sediment<br>(tons) | Peak<br>Sediment<br>Conc.<br>(mg/l) | Peak<br>Settleable<br>Conc.<br>(ml/l) | 24VW<br>(ml/l) |
|----|-----|---|---------------------------------------|----------------------------|--------------------------------------|--------------------|-------------------------------------|---------------------------------------|----------------|
| #1 | In  | 55.080                                    | 55.080                                | 24.99                      | 3.41                                 | 487.4              | 225,506                             | 135.51                                | 70.10          |
|    | Out |   |                                       | 0.84                       | 0.52                                 | 7.5                | 21,321                              | 0.00                                  | 0.00           |

***Particle Size Distribution(s) at Each Structure***

***Structure #1:***

| Size (mm) | In       | Out      |
|-----------|----------|----------|
| 2.0000    | 100.000% | 100.000% |
| 1.0000    | 94.455%  | 100.000% |
| 0.5000    | 90.406%  | 100.000% |
| 0.2500    | 78.262%  | 100.000% |
| 0.1250    | 70.166%  | 100.000% |
| 0.0630    | 51.275%  | 100.000% |
| 0.0160    | 28.336%  | 100.000% |
| 0.0040    | 14.843%  | 100.000% |



## ***Structure Detail:***

### Structure #1 (Pond)

**Pond Inputs:**

|                      |            |
|----------------------|------------|
| Permanent Pool Elev: | 5,604.50   |
| Permanent Pool:      | 0.85 ac-ft |
| *Sediment Storage:   | 0.00 ac-ft |
| Dead Space:          | 20.00 %    |

*\*No sediment capacity defined*

### Perforated Riser

| Riser Diameter (in) | Riser Height (ft) | Barrel Diameter (in) | Barrel Length (ft) | Barrel Slope (%) | Manning's n | Spillway Elev | Number of Holes per Elev |
|---------------------|-------------------|----------------------|--------------------|------------------|-------------|---------------|--------------------------|
| 18.00               | 5.00              | 18.00                | 100.00             | 0.01             | 0.0150      | 5,608.00      | 1                        |

**Pond Results:**

|                         |           |
|-------------------------|-----------|
| Peak Elevation:         | 5,608.08  |
| H'graph Detention Time: | 7.62 hrs  |
| Dewater Time:           | 0.36 days |
| Trap Efficiency:        | 98.46 %   |

*Dewatering time is calculated from peak stage to lowest spillway*

### Elevation-Capacity-Discharge Table

| Elevation | Area (ac) | Capacity (ac-ft) | Discharge (cfs) | Dewater Time (hrs)  |
|-----------|-----------|------------------|-----------------|---------------------|
| 5,603.00  | 0.515     | 0.000            | 0.000           | Top of Sed. Storage |
| 5,603.50  | 0.549     | 0.266            | 0.000           |                     |
| 5,604.00  | 0.584     | 0.549            | 0.000           |                     |
| 5,604.50  | 0.611     | 0.848            | 0.000           | Low hole SPW #1     |
| 5,605.00  | 0.638     | 1.160            | 0.000           |                     |
| 5,605.50  | 0.669     | 1.487            | 0.000           |                     |
| 5,606.00  | 0.700     | 1.829            | 0.000           |                     |
| 5,606.50  | 0.710     | 2.181            | 0.000           |                     |
| 5,607.00  | 0.720     | 2.539            | 0.000           |                     |
| 5,607.50  | 0.750     | 2.906            | 0.000           |                     |
| 5,608.00  | 0.781     | 3.289            | 0.000           | Spillway #1         |
| 5,608.08  | 0.782     | 3.354            | 0.844           | 8.70 Peak Stage     |
| 5,608.50  | 0.805     | 3.686            | 5.165           |                     |
| 5,609.00  | 0.830     | 4.094            | 8.509           |                     |

| Elevation | Area<br>(ac) | Capacity<br>(ac-ft) | Discharge<br>(cfs) | Dewater<br>Time<br>(hrs) |
|-----------|--------------|---------------------|--------------------|--------------------------|
| 5,609.50  | 0.841        | 4.512               | 10.421             |                          |
| 5,610.00  | 0.852        | 4.935               | 12.033             |                          |

Detailed Discharge Table

| Elevation | Perf. Riser (cfs) | Combined<br>Total<br>Discharge<br>(cfs) |
|-----------|-------------------|---|
| 5,603.00  | 0.000             | 0.000                                   |
| 5,603.50  | 0.000             | 0.000                                   |
| 5,604.00  | 0.000             | 0.000                                   |
| 5,604.50  | 0.10>0.000        | 0.000                                   |
| 5,605.00  | 0.000             | 0.000                                   |
| 5,605.50  | 0.000             | 0.000                                   |
| 5,606.00  | 0.000             | 0.000                                   |
| 5,606.50  | 0.000             | 0.000                                   |
| 5,607.00  | 0.000             | 0.000                                   |
| 5,607.50  | 0.000             | 0.000                                   |
| 5,608.00  | 0.000             | 0.000                                   |
| 5,608.50  | 5.165             | 5.165                                   |
| 5,609.00  | 8.509             | 8.509                                   |
| 5,609.50  | 10.421            | 10.421                                  |
| 5,610.00  | 12.033            | 12.033                                  |

### Subwatershed Hydrology Detail:

| Stru #   | SWS # | SWS Area (ac) | Time of Conc (hrs) | Musk K (hrs) | Musk X | Curve Number | UHS | Peak Discharge (cfs) | Runoff Volume (ac-ft) |
|----------|-------|---------------|--------------------|--------------|--------|--------------|-----|----------------------|-----------------------|
| #1       | 1     | 42.930        | 0.149              | 0.149        | 0.299  | 85.000       | M   | 24.64                | 2.845                 |
|          | 2     | 12.150        | 0.044              | 0.044        | 0.302  | 80.000       | M   | 7.85                 | 0.570                 |
| <b>Σ</b> |       | <b>55.080</b> |                    |              |        |              |     | <b>24.99</b>         | <b>3.414</b>          |

### Subwatershed Sedimentology Detail:

| Stru #   | SWS # | Soil K | L (ft)   | S (%) | C      | P      | PS # | Sediment (tons) | Peak Sediment Conc. (mg/l) | Peak Settleable Conc (ml/l) | 24VW (ml/l)  |
|----------|-------|--------|----------|-------|--------|--------|------|-----------------|----------------------------|-----------------------------|--------------|
| #1       | 1     | 0.320  | 1,351.51 | 6.40  | 0.5000 | 1.0000 | 1    | 471.7           | 255,227                    | 156.27                      | 85.12        |
|          | 2     | 0.320  | 420.77   | 6.77  | 0.5000 | 1.0000 | 1    | 59.5            | 151,759                    | 98.70                       | 47.93        |
| <b>Σ</b> |       |        |          |       |        |        |      | <b>487.4</b>    | <b>225,506</b>             | <b>135.51</b>               | <b>70.10</b> |

### Subwatershed Time of Concentration Details:

| Stru # | SWS # | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|--------|-------|---|-----------|------------------|-------------------|----------------|--------------|
| #1     | 1     | 5. Nearly bare and untilled, and alluvial valley fans | 6.38      | 86.45            | 1,354.63          | 2.520          | 0.149        |
| #1     | 1     | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.149</b> |
| #1     | 2     | 5. Nearly bare and untilled, and alluvial valley fans | 6.77      | 28.47            | 420.77            | 2.600          | 0.044        |
| #1     | 2     | <b>Time of Concentration:</b>                         |           |                  |                   |                | <b>0.044</b> |

### Subwatershed Muskingum Routing Details:

| Stru # | SWS # | Land Flow Condition                                   | Slope (%) | Vert. Dist. (ft) | Horiz. Dist. (ft) | Velocity (fps) | Time (hrs)   |
|--------|-------|---|-----------|------------------|-------------------|----------------|--------------|
| #1     | 1     | 5. Nearly bare and untilled, and alluvial valley fans | 6.38      | 86.45            | 1,354.62          | 2.520          | 0.149        |
| #1     | 1     | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.149</b> |
| #1     | 2     | 5. Nearly bare and untilled, and alluvial valley fans | 6.77      | 28.47            | 420.77            | 2.600          | 0.044        |
| #1     | 2     | <b>Muskingum K:</b>                                   |           |                  |                   |                | <b>0.044</b> |

## **POND 012 BANK SAFETY CALCULATIONS**

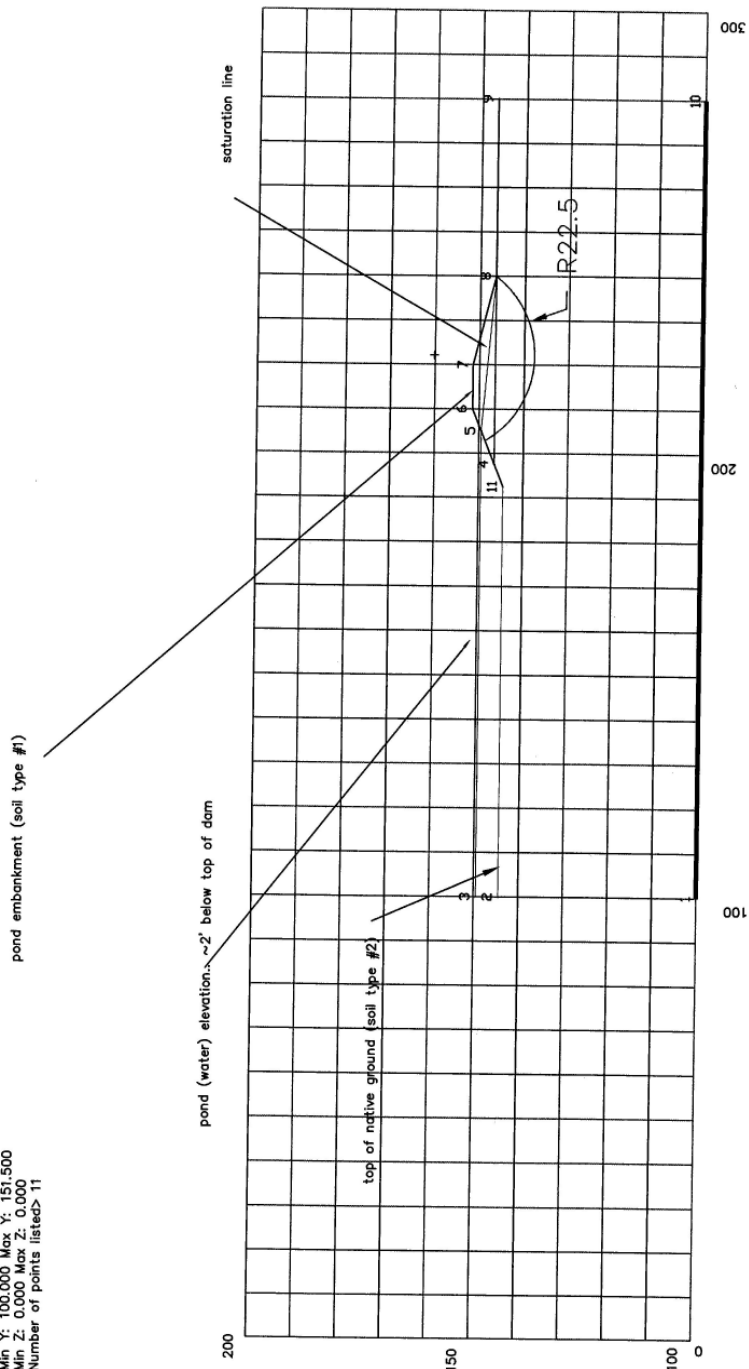
[illegible]

results from SB-Slope program, with failure passing thru pt #8  
center of failure plane = 222.1x,160.2y,  
r=22.5,  
FACTOR OF SAFETY=1.62

Note: Embankment data (#1) for SB-Slope = tri-axial results (Advanced Terra Testing) from pond 009  
density = 107 pcf  
cohesion = 84 pcf  
PHI = 29.1

Native data (#2) for SB-Slope = tri-axial results (Western Colorado Testing) for pond 012 embankment  
density = 118 pcf  
cohesion = 79 pcf  
PHI = 28.7

| Point#                      | Numbering | Earthing | Elev          | Description |
|-----------------------------|-----------|----------|---------------|-------------|
| 1                           | 100.000   |          | 100.000 0.000 |             |
| 2                           | 144.500   |          | 100.000 0.000 |             |
| 3                           | 149.500   |          | 100.000 0.000 |             |
| 4                           | 146.500   |          | 197.500 0.000 |             |
| 5                           | 149.500   |          | 205.000 0.000 |             |
| 6                           | 151.500   |          | 210.000 0.000 |             |
| 7                           | 151.500   |          | 220.000 0.000 |             |
| 8                           | 146.500   |          | 240.000 0.000 |             |
| 9                           | 146.500   |          | 280.000 0.000 |             |
| 10                          | 146.500   |          | 280.000 0.000 |             |
| 11                          | 144.500   |          | 192.500 0.000 |             |
| Min X:                      | 100.000   | Max X:   | 280.000       |             |
| Min Y:                      | 100.000   | Max Y:   | 151.500       |             |
| Min Z:                      | 0.000     | Max Z:   | 0.000         |             |
| Number of points listed> 11 |           |          |               |             |



GEOSYSTEM SLOPE STABILITY PROGRAM  
SB-SLOPE

PROJECT DATA:

Project: 012 POND

Location: NEW HORIZON MINE

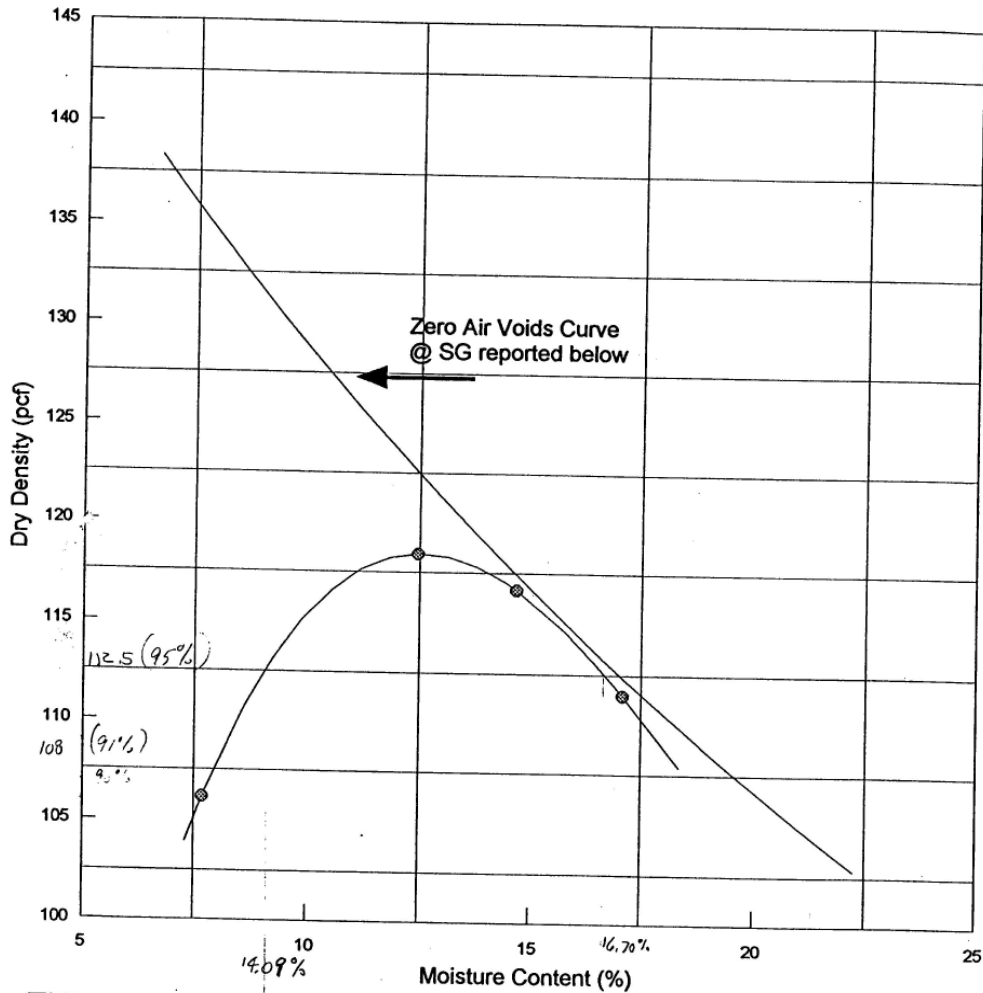
Filename: 012POND Description: 012 POND 2.5h:1V

ANALYSIS DATA:

| Point<br>No. | Coordinates<br>X Y | Line<br>No. | Left<br>Point | Right<br>Point | Soil<br>No. | Phreatic<br>Line | Soil<br>No. | Density<br>pcf | Cohesion<br>psf | Phi<br>Deg |
|--------------|--------------------|-------------|---------------|----------------|-------------|------------------|-------------|----------------|-----------------|------------|
| 1            | 100.0 100.0        | 1           | 1             | 10             | 2           | N                | 1           | 107.0          | 84              | 29.0       |
| 2            | 100.0 144.5        | 2           | 2             | 11             | 2           | N                | 2           | 118.0          | 79              | 29.0       |
| 3            | 100.0 149.5        | 3           | 11            | 4              | 2           | N                |             |                |                 |            |
| 4            | 197.5 146.5        | 4           | 4             | 8              | 2           | N                |             |                |                 |            |
| 5            | 205.0 149.5        | 5           | 8             | 9              | 2           | N                |             |                |                 |            |
| 6            | 210.0 151.5        | 6           | 4             | 5              | 1           | N                |             |                |                 |            |
| 7            | 220.0 151.5        | 7           | 5             | 6              | 1           | N                |             |                |                 |            |
| 8            | 240.0 146.5        | 8           | 6             | 7              | 1           | N                |             |                |                 |            |
| 9            | 280.0 146.5        | 9           | 7             | 8              | 1           | N                |             |                |                 |            |
| 10           | 280.0 100.0        | 10          | 5             | 8              | 1           | Y                |             |                |                 |            |
| 11           | 192.5 144.5        |             |               |                |             |                  |             |                |                 |            |

# Proctor Compaction Test

Sample 1



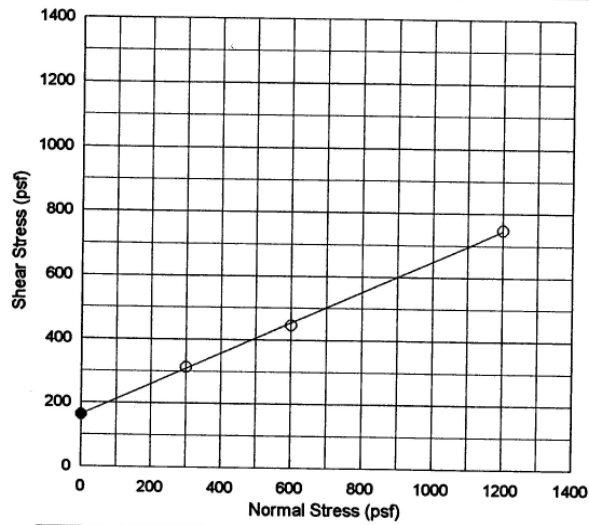
OPTIMUM MOISTURE CONTENT = 12.5 MAXIMUM DRY DENSITY = 118.4  
ASTM D 698 A, Rock correction applied? N

ADVANCED TERRA TESTING, INC.

$\frac{118.4}{\times 90\%}$   
10.7 pcf For Pond 012 Embankment

### Normal Stress vs. Peak Shear Stress

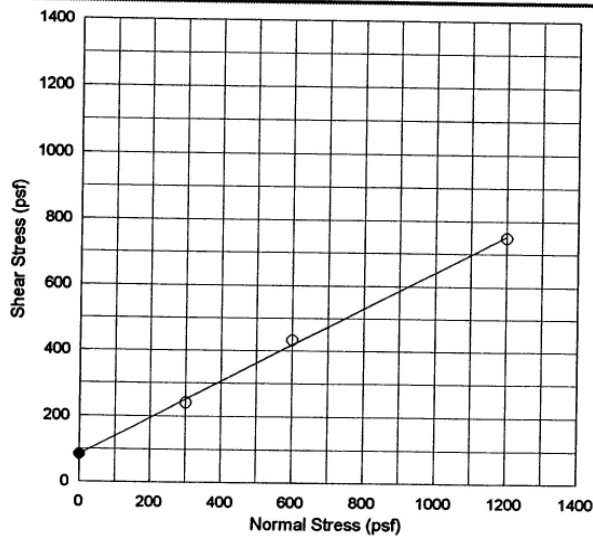
Sample 1,,



○ Shear Data — Best Fit Line ●  $c = 163.0$  psf  $\Phi = 25.9$  degrees

### Normal Stress vs. Ultimate Shear Stress

Sample 1,,



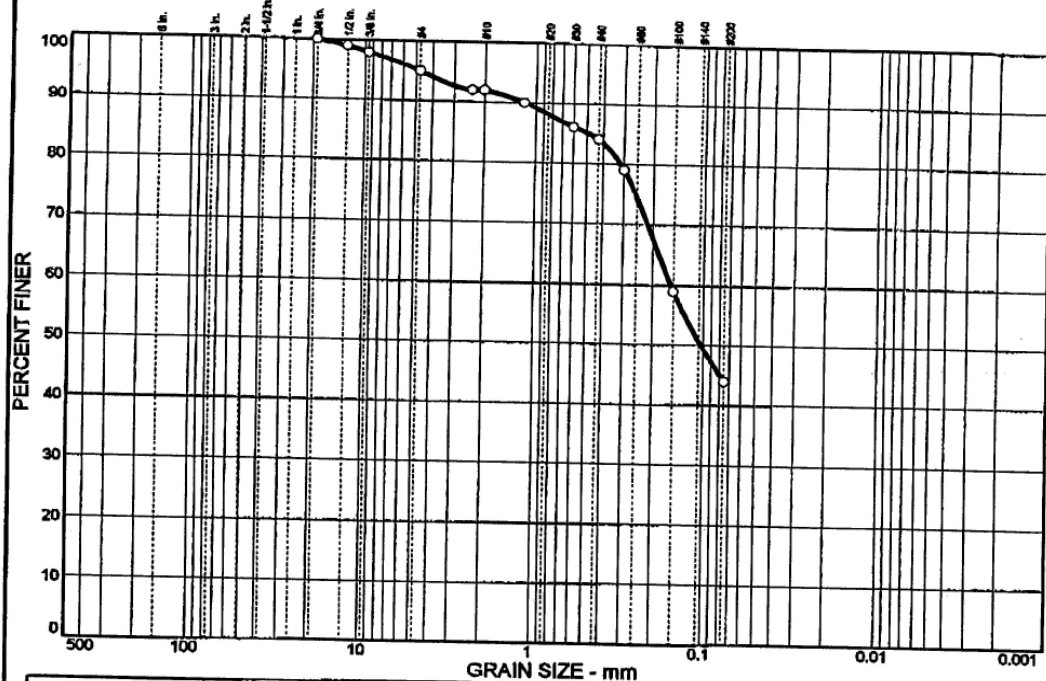
○ Shear Data — Best Fit Line ●  $c = 84.0$  psf  $\Phi = 29.1$  degrees

USE FOR Pond 012  
Embankment

ADVANCED TERRA TESTING, INC.



# PARTICLE SIZE DISTRIBUTION TEST REPORT



| % + 3" | % GRAVEL | % SAND | % SILT | % CLAY |
|--------|----------|--------|--------|--------|
| 0.0    | 5.0      | 51.0   | 44.0   |        |

| SIEVE SIZE | PERCENT FINER | SPEC.* PERCENT | PASS? (X=NO) |
|------------|---------------|----------------|--------------|
| 3/4 in.    | 100.0         |                |              |
| 1/2 in.    | 99.0          |                |              |
| 3/8 in.    | 98.0          |                |              |
| #4         | 95.0          |                |              |
| #8         | 92.0          |                |              |
| #10        | 92.0          |                |              |
| #16        | 90.0          |                |              |
| #30        | 86.0          |                |              |
| #40        | 84.0          |                |              |
| #50        | 79.0          |                |              |
| #100       | 59.0          |                |              |
| #200       | 44.0          |                |              |

\* (no specification provided)

**Soil Description**  
Sand, silty, clayey (SC-SM)

**Atterberg Limits**  
PL= 16 LL= 22 PI= 6

**Coefficients**  
D<sub>85</sub>= 0.491 D<sub>60</sub>= 0.155 D<sub>50</sub>= 0.103  
D<sub>30</sub>= D<sub>15</sub>=  
C<sub>u</sub>= C<sub>c</sub>=

**Classification**  
USCS= SC-SM AASHTO= A-4(0)

**Remarks**  
Sampled by JB, 12-7-04  
Tested by JB, 12-9-04  
Reviewed by JCH

Sample No.: 04-402 Source of Sample:  
Location: Pond 102 Fill Material

Date: 12-17-04  
Elev./Depth: N/A

WESTERN COLORADO TESTING, INC.

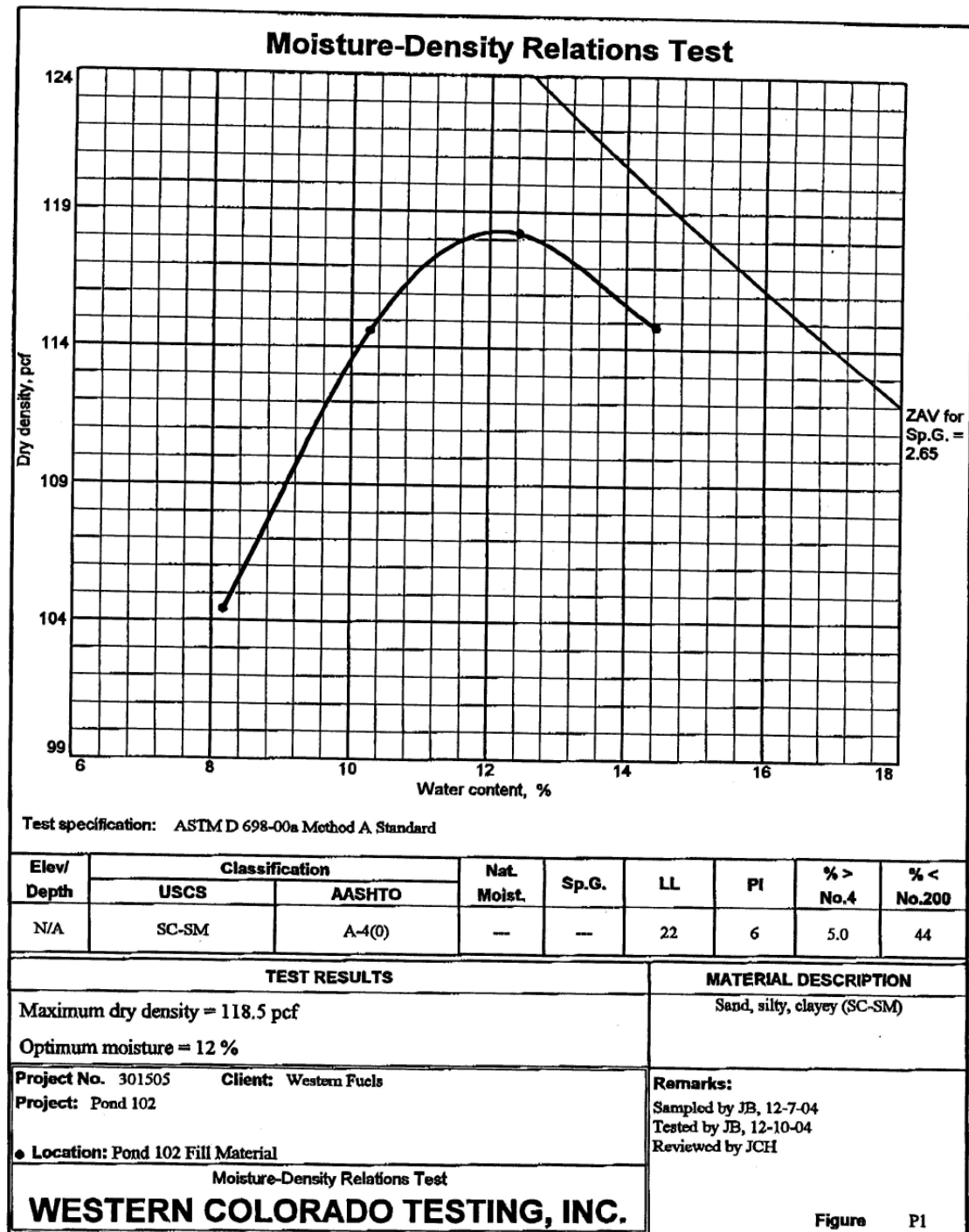
Client: Western Fuels  
Project: Pond 102

Project No: 301505

Figure 2

Pond 012 POND- Native





POND 012 - Native



WESTERN  
COLORADO  
TESTING,  
INC.

# Consolidated Triaxial Compression, ASTM D 4767-95

Job Name: Triaxial Testing Job No.: 301,505 Technician: BJR/JCH Date: 1/10/2005  
 Sample Location: Undisturbed In-situ Depth: 0 Lab Number: 04-405  
 Description: Sand, silty, clayey (SC-SM)  
 MDD (pcf): n/a OMC (%): n/a Compaction Method: n/a

| Confining Pressure: 6 psi          |         |       |  |
|------------------------------------|---------|-------|--|
|                                    | Initial | Final |  |
| Dry Density (pcf)                  | 103.2   | 84.1  |  |
| Moisture Content (%)               | 7.8%    | 20.9% |  |
| Saturation (%)                     | —       | —     |  |
| Height (in.)                       | 3.50    | 3.39  |  |
| Diameter (in.)                     | 1.93    |       |  |
| Cross-Sec. Area (in <sup>2</sup> ) | 2.93    | 3.31  |  |
| Void Ratio                         | 0.38    | 0.43  |  |
| Specific Gravity*                  | 2.65    |       |  |

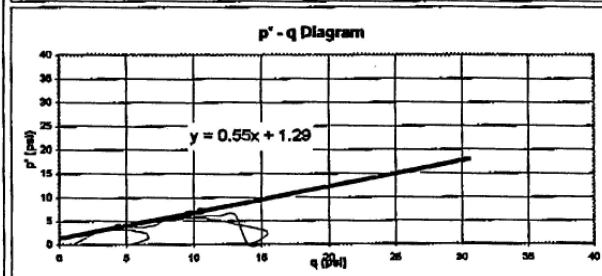
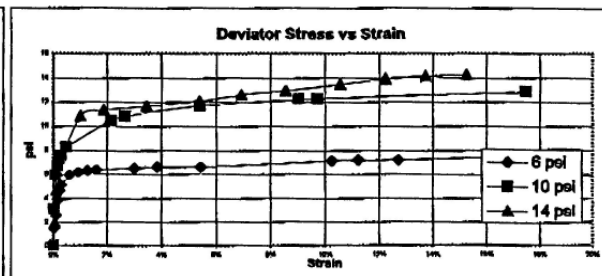
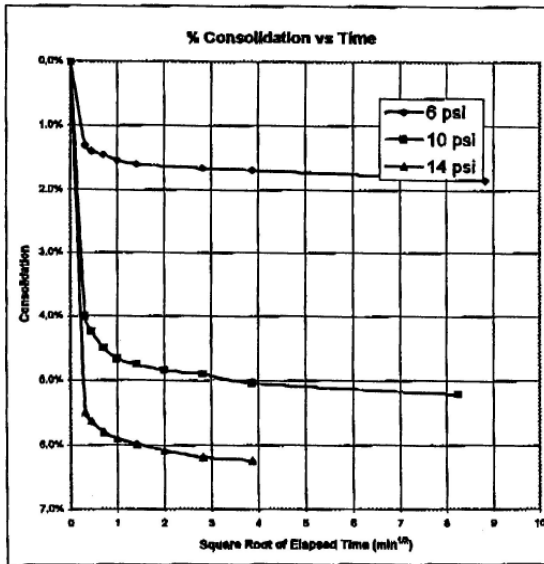
\*Assumed

| Confining Pressure: 10 psi         |         |       |  |
|------------------------------------|---------|-------|--|
|                                    | Initial | Final |  |
| Dry Density (pcf)                  | 98.2    | 85.9  |  |
| Moisture Content (%)               | 6.4%    | 22.5% |  |
| Saturation (%)                     | —       | —     |  |
| Height (in.)                       | 3.59    | 2.86  |  |
| Diameter (in.)                     | 1.94    |       |  |
| Cross-Sec. Area (in <sup>2</sup> ) | 2.97    | 3.68  |  |
| Void Ratio                         | 0.41    | 0.42  |  |
| Specific Gravity*                  | 2.65    |       |  |

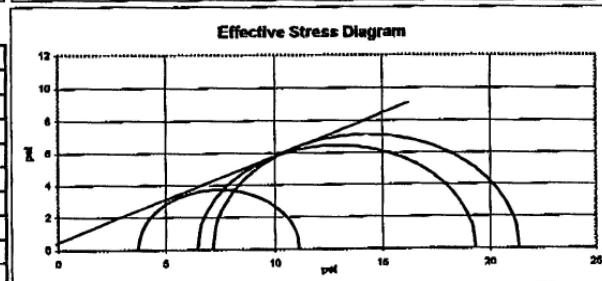
\*Assumed

| Confining Pressure: 14 psi         |         |       |  |
|------------------------------------|---------|-------|--|
|                                    | Initial | Final |  |
| Dry Density (pcf)                  | 106.7   | 85.6  |  |
| Moisture Content (%)               | 5.3%    | 15.9% |  |
| Saturation (%)                     | —       | —     |  |
| Height (in.)                       | 3.94    | 3.34  |  |
| Diameter (in.)                     | 1.94    |       |  |
| Cross-Sec. Area (in <sup>2</sup> ) | 2.95    | 3.53  |  |
| Void Ratio                         | 0.36    | 0.42  |  |
| Specific Gravity*                  | 2.65    |       |  |

\*Assumed



|                         | 6 psi  | 10 psi | 14 psi |
|-------------------------|--------|--------|--------|
| B Coefficient           | 99     | 97     | 95     |
| t <sub>50</sub> (min)   | 1.1    | 1.1    | 1.1    |
| Back Pressure (psi)     | 69.4   | 71.4   | 70.9   |
| Effective Stress (psi)  | 5.4    | 8.3    | 14.1   |
| Minor Eff. Stress (psi) | 0.7    | 2.9    | 2.9    |
| Major Eff. Stress (psi) | 5.4    | 8.3    | 14.1   |
| Deviator Stress (psi)   | 7.4    | 12.9   | 14.2   |
| Strain @ Failure (%)    | 18.3%  | 17.5%  | 15.3%  |
| Shear Rate (in/min)     | 0.0022 | 0.0023 | 0.0022 |

Failure Criteria: Maximum Load

NATIVE EARTH  
Angle of Internal Friction: 28.7 degrees  
 $\sigma_{1e} \pm 2$

q<sub>u</sub>: 0.55 psi

Fig. S2

$$= 1.44 \times 0.55$$

$$= 79.2 \frac{\text{lb}}{\text{ft}^2}$$

POND OR Native