



SMITH WILLIAMS CONSULTANTS, INC.

SCANNED

Appendix C.2

Geomembrane Tensile Strength and Anchor Trench Calculations

Liner Calc's

Calc. FOS for Tensile Failure and Anchor Pull-out due to self-weight.
Based on methods presented in "Designing With Geosynthetics" 4 th edition
Robert M. Koerner, 1998 Prentice-Hall



Project: CC&V Phase 5 2.5 Slope w/ 300 slope length

Date: August 2007

By: J. F. Lupo

checked: WITTNER 8/6/07

Input Parameters

Height of Slope (ft):	300 ft
Slope (Z:1):	2.5
FML Thickness (mil):	80 mil
FML Yield Stress (psi):	2200 psi
FML Specific Gravity:	0.935
Soil Friction Angle	30 degrees
Liner-Soil Interface Friction Angle (degrees):	15 degrees
Anchor Trench Depth (ft):	3 ft
Anchor Trench Width (ft):	3 ft
Anchor Set-Back (ft)	3 ft
Soil Depth over Setback	2 ft
Soil Unit Weight (pcf):	110 pcf

TENSILE FAILURE OF LINER FROM SELF-WT CALC'S

FML Density =	pcf
Slope Length =	ft
Slope Angle =	degrees
Liner Total WL/ Unit ft. =	lbs/ft
Max. Tensile Force From Self-Wt. =	lbs/ft
Frictional Resistance =	lbs/ft
Tensile Stress (neg. frictional resistance)	psi
Tensile Stress (w/ frictional resistance)	psi
FOS Tensile failure (MIN)	0.13
FOS Tensile failure (MAX)	1.80 PASS
	FOS must be greater than 10 to pass
	PASS
	FOS must be greater than 10 to pass
Max. Heat/Cool Force:	lbs/ft
Max. Tensile Stress Developed +	psi
FOS Tensile Failure =	PASS
	FOS must be greater than 5 to pass

LINER ANCHOR CALC'S

At Rest Coeff.	0.50
Active Pressure Coeff.	0.83
Passive Pressure Coeff.	0.67
Allowable Liner Force	lbs/ft
Shear Force Above Membrane Due to Soil Cover	lbs/ft
Shear Force Below Liner Due to Soil Cover	lbs/ft
Shear Force Below Liner Due to Liner Pull-Down	lbs/ft
Active Pressure Anchor Backfill Side	lbs/ft
Passive Pressure Anchor InSitu Side	lbs/ft
Sum of Forces	1.50
FOS Pull-out	1.80 PASS

Liner Calc's

Calc. FOS for Tensile Failure and Anchor Pull-out due to self-weight.
Based on methods presented in "Designing With Geosynthetics" 4 th edition
Robert M. Koerner, 1998 Prentice-Hall



SMITH WILLIAMS CONSULTANTS, INC.

Project: CC&V Phase 5 2.0 Slope w/ 300 slope length

Date: August 2007

By: J. F. Lupo

CHECKED: WITTWER 8/6/07

Input Parameters

Height of Slope (ft):	300 ft
Slope (Z:1):	2
FML Thickness (mil):	80 mil
FML Yield Stress (psi):	2200 psi
FML Specific Gravity:	0.935
Soil Friction Angle	30 degrees
Liner-Soil Interface Friction Angle (degrees):	15 degrees
Anchor Trench Depth (ft):	3 ft
Anchor Trench Width (ft):	3 ft
Anchor Set-Back (ft)	3 ft
Soil Depth over Setback	2 ft
Soil Unit Weight (pcf):	110 pcf

TENSILE FAILURE OF LINER FROM SELF-WT CALC'S

FML Density =	110 pcf
Slope Length =	300 ft
Slope Angle =	15 degrees
Liner Total Wt./Unit ft. =	220.92 lbs/ft
Max. Tensile Force From Self-Wt. =	16.69 lbs/ft
Frictional Resistance =	182.53 lbs/ft
Tensile Stress (neg. frictional resistance)	21.55 psi
Tensile Stress (w/ frictional resistance)	56.44 psi
FOS Tensile failure (MIN)	PASS
FOS Tensile failure (MAX)	PASS

FOS must be greater than 10 to pass

FOS must be greater than 10 to pass

Max. Heat/Cool Force:	lbs/ft
Max. Tensile Stress Developed +	psi
FOS Tensile Failure =	PASS

FOS must be greater than 5 to pass

LINER ANCHOR CALC'S

At Rest Coeff.	
Active Pressure Coeff.	
Passive Pressure Coeff.	
Allowable Liner Force	
Shear Force Above Membrane Due to Soil Cover	lbs/ft
Shear Force Below Liner Due to Soil Cover	lbs/ft
Shear Force Below Liner Due to Liner Pull-Down	lbs/ft
Active Pressure Anchor Backfill Side	lbs/ft
Passive Pressure Anchor InSitu Side	lbs/ft
Sum of Forces	lbs/ft
FOS Pull-out	PASS



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Appendix C.3.1

Phases I Through 5 Primary Solution Collection Pipe Burial Calculations



SMITH WILLIAMS CONSULTANTS, INC.

Project: CC&V Phase 5 VLF	Job No. 1125
Calculation Title: Ore Loading Effects on solution collection piping	
Prepared By: JFL	Date: March 14, 2008
Checked By: DTW	Date: March 19, 2008

OBJECTIVE:

Assess the effect of ore loading on solution collection piping deformation for the Phase 5 VLF extension, and existing pipes within the VLF (including underdrains).

METHOD:

The method for PE pipe deformation under high loads is based on the work presented in Lupo (2001).

Traditional methods for pipe design are based on stress theory, whereby the stress conditions within the pipe wall are evaluated based on assumed loading conditions. This design approach was initially developed for concrete and steel pipe and has been extended for PE pipe design. The stress theory method was developed assuming the pipe materials are very stiff compared to the pipe envelope material (the material surrounding the pipe). Under these conditions, the loads are carried entirely by the pipe, not by the pipe envelope.

Pipe design employing stress theory requires the pipe to be designed to account for the following performance criteria:

- Wall Crushing : Wall crushing occurs when the wall stress exceeds the long-term compressive strength of pipe material;
- Wall Buckling: Wall buckling occurs when the total soil pressure exceeds the pipe critical buckling pressure; and
- Ring Deflection: Ring deflection is defined as the ratio between the vertical change in diameter to the original pipe diameter. Typically, pipe deflection is calculated using the Modified Iowa method (USDA, 1990). The design limit for ring deflection is typically assumed to be approximately 5 percent. Krizek (1990) reports that this value was derived from the inspections of numerous pipe installations, where the average deflection before failure was determined to about 20 percent of the pipe diameter. Assuming a safety factor of 4, results in design ring deflection of 5 percent.

For design, the applied stress on the pipe is based on an assumed prism of ore above the pipe, so the vertical stress can be calculated as:

$$\sigma_v = \gamma_o * h$$

where:



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γ_0 = unit of ore, and
 h = height of ore over the pipe.

This applied stress, plus any additional stresses, are applied as an external pressure to the pipe to assess wall crushing and pipe buckling. The pipe-ore interaction is not accounted for in these calculations.

The pipe ring deflection is typically evaluated using the Modified Iowa method. This method relates pipe deflection to the stiffness of the pipe and ore. In the modified Iowa method, the pipe and ore stiffness are addressed separately; the pipe-ore interaction is not accounted for in this method.

While the traditional approach can be used for PE pipe design, field and laboratory studies have shown that the traditional approach for pipe design may result in overly conservative designs. For leach facility design this can lead to limits on ore height over the pipe, or special pipe bedding/trenching design.

The reason the traditional design approach may be overly conservative is that PE pipes are significantly more flexible than steel or concrete pipes. Field and laboratory studies conducted by Watkins and Reeve (1979), Watkins (1987), Watkins (1990), Sargand et al (1993) and Reeve et al (1981) have shown that flexible pipe performance is strongly influenced by the pipe-envelope interaction. A schematic illustrating the pipe-envelope interaction with respect to pipe performance limits is shown in Figure 1.

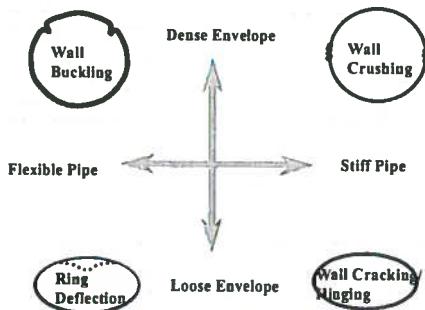


Figure 1. Schematic of Pipe Performance Limits (after Watkins and Reeve, 1979).

Field and laboratory performance tests have shown that the primary performance limit for PE pipes is ring deflection (Watkins and Reeve, 1979). Excessive ring deflection in PE pipes may lead to:

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- Restricted flow within the pipe, and
- Excessive dimpling leading to pipe buckling.

Compared to stiff pipe (i.e. steel and concrete), flexible pipe, such as PE, interacts differently with the surrounding ore. PE pipe readily deforms under load, interacting closely with the ore. Furthermore, PE material is a viscoelastic material, which has the beneficial property of creeping or stress relaxation under load. This means that after the pipe is loaded, the stress in the wall of the pipe will decrease (relax) over time as the pipe deforms.

The flexibility of PE pipe can lead to the development of a stress arch within the ore. A stress arch transfers a portion of the vertical stress around the flexible pipe and into the adjacent ore. PE pipe deformation and stress arch development are illustrated in Figures 2 and 3, respectively.

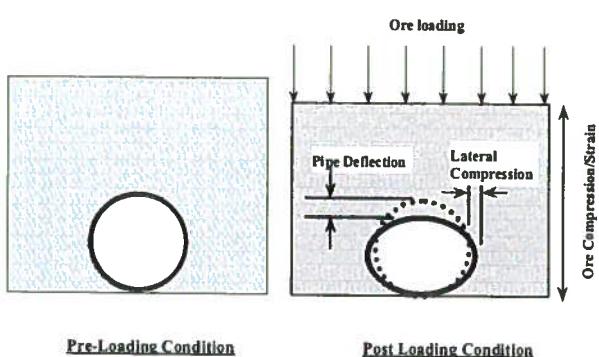


Figure 2. Flexible Pipe Deformation

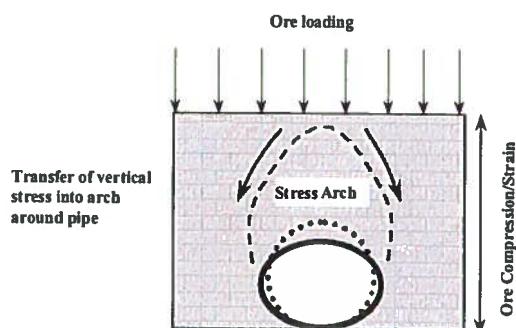


Figure 3. Stress Arch Development

Several laboratory and field test programs have been conducted to assess the actual performance of



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PE pipes. The results of these test programs have been instrumental in the understanding of PE pipe performance. A summary of pipe test results is presented in Figure 4.

PIPE PERFORMANCE

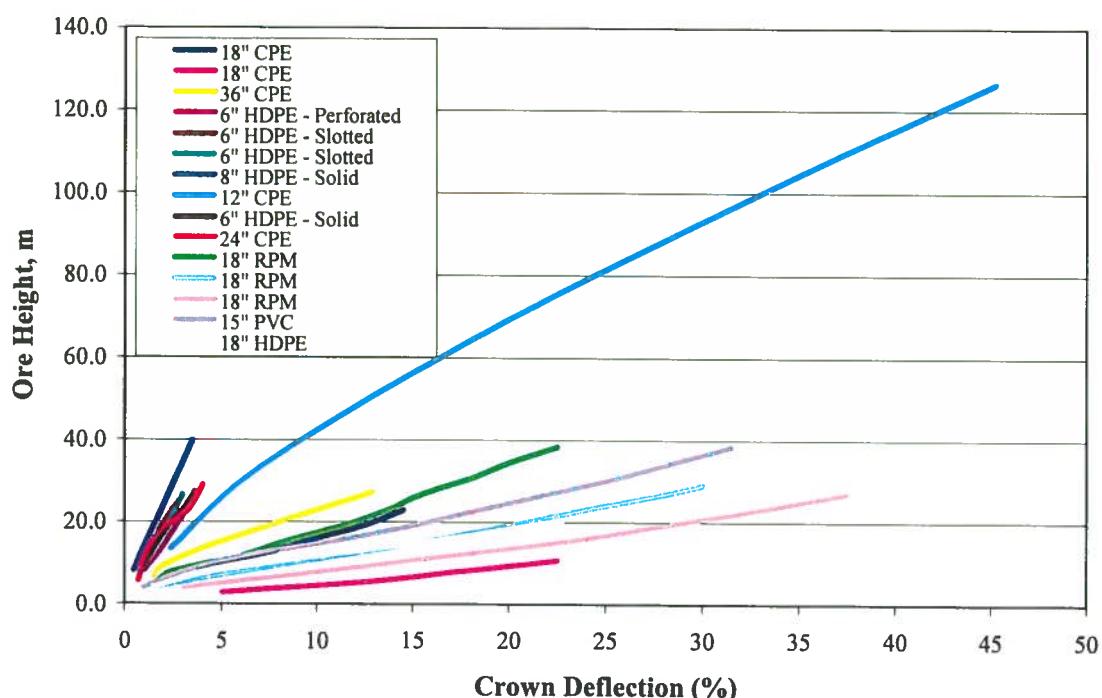


Figure 4. Pipe Test Data

When reviewing the test data presented in Figure 4, it is important to note that none of the PE pipes failed in these tests. All of the tests were terminated before failure of the pipes could be reached because of limitations to the test apparatus or fill height.

The results from these tests clearly show that PE pipes can remain stable and functional with ring deflections in excess of 20 percent. These results also agree well with observations from actual leach pads, as illustrated in Figure 5 which shows a functional solution collection pipe from a leach pad, with approximately 20 percent ring deflection.



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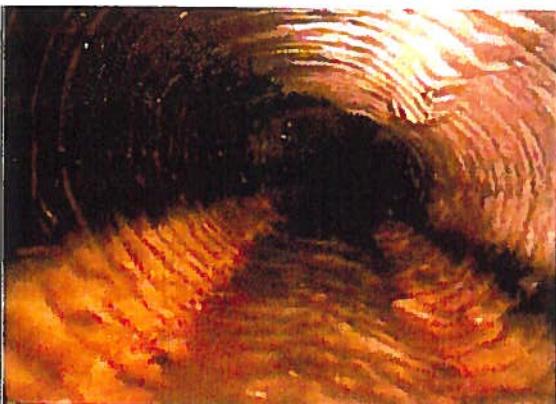


Figure 5 Functioning Solution Collection Pipe w/ 20% Ring Deflection (Binocular Shape)

Watkins (1990) has shown that the pipe deflection is closely associated with the compression of the material surrounding the pipe (termed the pipe envelope). Therefore, the pipe design approach should account for the compression characteristics of the pipe envelope.

The recommended approach for flexible pipe design is based on the work of Burns & Richard (1964) and Höeg (1968), which present closed form plane-strain solutions for thin, circular, elastic conduits buried in an elastic soil. These equations include the interaction of the pipe with the surrounding material. To provide a more suitable solution for flexible pipe design, these equations have been modified to account for the following:

- Non-linear compression of ore during loading,
- Viscoelastic nature of the PE pipe material, and
- A more thorough accounting for the stress arch effect due rotation of principle stresses.

ASSUMPTIONS:

- The corrugated PE pipe characteristics are defined by those presented by Advanced Drainage Systems (ADS).
- Solid PE pipe characteristics are defined by Drisco-Pipe.
- The pipe envelope behavior is based on compression tests conducted on actual Cresson Project Drain Cover Fill (DCF). The compression curve is defined as that presented in



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Figure 6. The parameters of the ore/DCF were based on test data, and have the following properties:

Property	Value
Unit Wt.	118 pcf
Elastic Modulus	Varies according to Fig. 6
Friction Angle	40 degrees

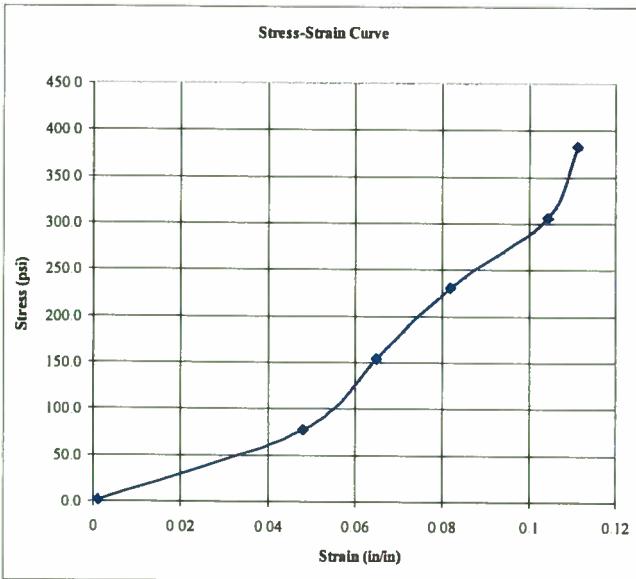


Figure 6. DCF Compression Curve

CALCULATIONS:

Pipe deformation calculations were conducted for the following scenarios, which cover the Primary, Secondary, LVSC, Leak Detection, and the Arequa Gulch Spring pipes under the maximum applicable ore depths.



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Pipe Deformation Analyses

VLF Phase	Pipe	Ore Depth (ft)
5	Primary Pipe – 26" OD, DR 11 Solid HDPE Pipe	590
5	Secondary Pipe – 16" OD PCPE	590
5	Secondary Pipe – 12" OD PCPE	590
IV	Primary Pipe – 26" OD, DR 11 Solid HDPE Pipe	800
IV	Secondary Pipe – 18" OD PCPE	800
I,II	Primary Pipe – 15" OD PCPE	800
I,II,III	LVSC, Leak Detection Pipe – 4" OD PCPE	800
Arequa Gulch Spring Pipe		800

The results of the pipe deformation analyses are presented in Attachment A.

CONCLUSIONS:

The pipe deformation analyses indicate that the pipes, under the maximum ore load, will deform between 10 to 22 percent, as summarized below. It is noted that pipes undergoing deformations in the range of 20% should be sized for twice the flow capacity, as the pipe will likely take on a binocular shape (see Figure 5). In the case of VLF (all Phases I-IV and 5), all pipes were sized assuming a binocular shape, therefore the pipes will function as designed, even under 22% crown deflection.



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VLF Phase	Pipe	Crown Deflection	Acceptable (y/n)
5	Primary Pipe – 26" OD, DR 11 Solid HDPE Pipe	10-12%	Yes
5	Secondary Pipe – 16" OD PCPE	18%	Yes. Size pipe for twice the flow to accommodate deformation
5	Secondary Pipe – 12" OD PCPE	18%	Yes. Size pipe for twice the flow to accommodate deformation
IV	Primary Pipe – 26" OD, DR 11 Solid HDPE Pipe	12-15%	Yes
IV	Secondary Pipe – 18" OD PCPE	22%	Yes. In original design, these pipes were sized for twice the flow assuming a binocular pipe section.
I,II	Primary Pipe – 15" OD PCPE	22%	Yes. In original design, these pipes were sized for twice the flow assuming a binocular pipe section.
I,II,III	LVSC, Leak Detection Pipe – 4" OD PCPE	22%	Yes. In original design, these pipes were sized for twice the flow assuming a binocular pipe section.
Arequa Gulch Spring Pipe	4" OD SDR 17 Solid HDPE	16%	Yes

References

Burns, J.Q. and Richard, R.M., 1964. "Attenuation of Stresses for Buried Conduits"; *Proc. Symp. Soil-Structure Interaction*, University of Arizona.

Höeg, K., 1968. "Stresses Against Underground Structural Cylinders"; *J. Soil Mech. And Foundation Div. ASCE*, Vol. 94, No. SM4.



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Krizek, R.J., 1990. "Buried Conduits", presented in Structural Engineering Handbook, E. Gaylord and C. Gaylord, eds., McGraw-Hill Publishing.

Lupo, J.F. 2001, *Performance of PE Pipes Under High Heap Loads*, 2001 Society for Mining, Metallurgy, and Exploration Annual Meeting, Denver, Colorado, USA.

Reeve, R.C., Slicker, R.E., and Lang, T.J., 1981, Corrugated Plastic Tubing, Proc. Int'l. Conf. Underground Plastic Pipe, ASCE, New Orleans, Louisiana

Sargand, S.M., Hazen, G.A., Fernando, M.E.R., and Hurd, J.O., 1993. "Field Performance of a Corrugated HDPE Pipe", Transportation Research Board, 72nd Annual Meeting, Washington, D.C.

USDA, 1990. Design and Installation of Flexible Conduits – Plastic Pipe, Soil Conservation Service, Technical Release No. 77.

Watkins, R.K., Dwiggins, J.M. and Altermatt, W.E., 1987. "Structural Design of Buried Corrugated Polyethylene Pipes", In *Transportation Research Record 1129*, TRB, National Research Council, Washington, D.C.

Watkins, R.K., 1990. "Plastic Pipes Under High Landfills", Buried Plastic Pipe Technology, ASTM STP 1093, George S. Buczala and Michael J. Cassady, eds. ASTM, Philadelphia.

Watkins, R.K. and Reeve, R.C., 1979. "Structural Performance of Buried Corrugated Polyethylene Tubing", Thirtieth Annual Highway Geology Symposium, FHA, Portland Oregon.

Watkins, R.K., 1987. "Structural Performance of Perforated and Slotted High-Density Polyethylene Pipes Under High Soil Cover", unpublished report.



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Attachment A
Pipe Deformation Analyses

BURIED PLASTIC PIPE LOADING WORKSHEET V2.0

Polyethylene Pipe &土管
PVC-U Pipe & 土管

SAC



Project: C.A. Pipe & Plastics Pipe 24" O.D. SDR 35 HDPE
In: Layer
Soil: Sand
Note: Impact of ground surface slopes is included

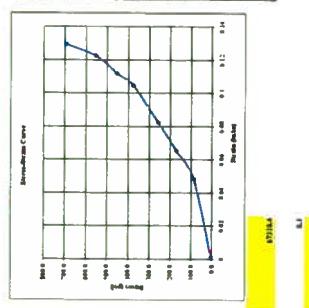
ROH and PITE Load Data

Horizontal	C-Value	Vertical Axle	C-Component Method	Vertical Stress Ratio	A	C
0%	85%	85%	85%	1.00		
10% Earthfill	8%	60%	60%	0.50		
10% Compacted	34%	34%	34%	0.50	0.44	0.44
10% Gravel	31%	31%	31%	0.30	0.30	0.30
10% Sand	38%	38%	38%	0.30	0.30	0.30
10% Soil	43%	43%	43%	0.30	0.30	0.30
10% Slope	26%	26%	26%	0.30	0.30	0.30
10% Compacted Slope	34%	34%	34%	0.30	0.30	0.30
10% Gravel Slope	31%	31%	31%	0.30	0.30	0.30
10% Sand Slope	38%	38%	38%	0.30	0.30	0.30
10% Soil Slope	43%	43%	43%	0.30	0.30	0.30

Soil Adhesion Parameters		
θ_{ad}	ϕ_{ad}	Cohesion of Contact Soil (Cohesionless soil)
45°	33°	27.13

Angle of Internal Friction Soil (Cohesionless soil)

Free Vertical Compression Ratio					
A-Value (Vertical Load / Total Vertical Force)	1.0	0.01	1.000		
B-Value	0.93	0.004	1.171		
C-Value	0.79	0.045	26.9		
D-Value	0.75	0.009	375.0		
E-Value	0.72	0.002	2372		
F-Value	0.69	0.004	46.0	0.026	
G-Value	0.66	0.116	0.000	0.026	
H-Value	0.63	0.211	0.000	0.046	
I-Value	0.60	0.317	0.000	0.076	



Free Vertical Compression Ratio
Depth 1000 mm
Depth 1500 mm
Depth 2000 mm

PDI INTERFAZ FAISACE			PDI INTERFAZ FAISACE			PDI INTERFAZ FAISACE		
		Base Densidad (kg/m³)			Base Densidad (kg/m³)			Base Densidad (kg/m³)
Año:	Base:	Uso:	Año:	Base:	Uso:	Año:	Base:	Uso:
0	001.3	0.001.00	0	-1.300	0.001.00	0	000.304	0.001.00
10	079.5	000.300	10	-1.311	000.300	10	000.304	000.300
20	079.5	000.300	20	-1.311	000.300	20	000.304	000.300
30	079.5	000.300	30	-1.311	000.300	30	000.304	000.300
40	079.5	000.300	40	-1.311	000.300	40	000.304	000.300
50	079.5	000.300	50	-1.311	000.300	50	000.304	000.300
60	079.5	000.300	60	-1.311	000.300	60	000.304	000.300
70	079.5	000.300	70	-1.311	000.300	70	000.304	000.300
80	079.5	000.300	80	-1.311	000.300	80	000.304	000.300
90	079.5	000.300	90	-1.311	000.300	90	000.304	000.300
100	079.5	000.300	100	-1.311	000.300	100	000.304	000.300
Variancia Diferencia (%)								
Estimaciones Diferencia (%)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00
Total Dif. Promedio de Chorro (%)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00
Correlacionado Desviación (%)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00
Ara. Largo de la tuba (m)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00
PDI INTERFAZ FAISACE								
		Base Densidad (kg/m³)			Base Densidad (kg/m³)			Base Densidad (kg/m³)
Año:	Base:	Uso:	Año:	Base:	Uso:	Año:	Base:	Uso:
0	000.000	0.000.000	0	-1.000	0.000.000	0	000.000	0.000.000
10	000.000	0.000.000	10	-1.000	0.000.000	10	000.000	0.000.000
20	000.000	0.000.000	20	-1.000	0.000.000	20	000.000	0.000.000
30	000.000	0.000.000	30	-1.000	0.000.000	30	000.000	0.000.000
40	000.000	0.000.000	40	-1.000	0.000.000	40	000.000	0.000.000
50	000.000	0.000.000	50	-1.000	0.000.000	50	000.000	0.000.000
60	000.000	0.000.000	60	-1.000	0.000.000	60	000.000	0.000.000
70	000.000	0.000.000	70	-1.000	0.000.000	70	000.000	0.000.000
80	000.000	0.000.000	80	-1.000	0.000.000	80	000.000	0.000.000
90	000.000	0.000.000	90	-1.000	0.000.000	90	000.000	0.000.000
100	000.000	0.000.000	100	-1.000	0.000.000	100	000.000	0.000.000
Variancia Diferencia (%)								
Estimaciones Diferencia (%)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00
Total Dif. Promedio de Chorro (%)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00
Correlacionado Desviación (%)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00
Ara. Largo de la tuba (m)								
0.00	-0.00	0.00	0.00	-0.00	0.00	0.00	-0.00	0.00

Building (Ref)	CROWN			SPRINGCLINE		
	Standard Deviation, per cent (days)					
11.75	417.5	207.9	62.3	184.3	184.8	42.7
12.25	373.1	209.7	60.9	181.3	64.8	41.4
12.75	373.1	279.9	51.3	179.2	175.2	41.1
13.25	362.7	214.5	60.1	177.3	16.6	41.9
13.75	371.6	239.0	70.8	176.1	16.2	42.6
14.25	370.6	188.3	56.6	175.1	36.3	42.1
14.75	367.8	209.8	51.6	176.5	36.2	42.9
15.25	361.7	240.3	50.8	171.2	36.5	42.1
15.75	360.9	245.5	80.9	171.9	36.3	42.9
16.25	349.8	374.5	71.6	172.0	35.9	41.5
16.75	369.9	182.4	26.1	173.7	35.8	42.6
17.25	371.3	279.6	21.3	173.7	35.9	42.1
17.75	370.0	279.3	20.7	173.6	37.3	42.9
18.25	371.9	60.6	171.8	173.3	36.5	42.6
18.75	351.1	60.3	129.3	171.1	37.7	42.1
19.25	364.3	60.7	126.9	174.2	32.9	42.8
19.75	371.6	61.4	120.8	174.6	32.3	42.5
20.25	370.9	417.1	116.6	174.6	31.9	42.6
20.75	370.2	419.4	113.2	174.9	31.9	42.9
21.25	377.6	61.6	107.1	174.0	31.7	42.6
21.75	370.6	200.6	61.6	170.2	30.4	42.2
22.25	381.7	419.1	121.9	171.6	30.3	42.6
22.75	380.7	416.6	121.6	171.6	30.3	42.6
23.25	387.7	419.1	179.5	174.9	31.3	42.1
23.75	371.5	415.1	177.9	174.9	31.3	42.7
419.75	380.4	277.7	417.2	176.3	34.9	42.6
Solid Arching	Product Arch	Product Arch	Reinforced Arch	Reinforced Arch	Product Arch	Product Arch

BURIED PLASTIC PIPE LOADING WORKSHEET V2.0

Project Instrumentation & Control Engineering



Project CCAW Plastic & Secondary Piping, 40" DIA HDPE Pipe

By: Lape

Date: October 2020

Note: Components or features marked in yellow are:



Instrument Parameters

Material	C Factor	Previous Analysis	Current Material Spec	Lamcarther Rate	B	C
PVC	0.75	0.75				
PPB, PTFE	0	0.0	0.018	0.018	0.102	0.101
Pipe Diameter (in)	17.91					
Pipe ID (in)	15.19					
Weight of Pipe (lb/in)	4.43					
Pipe Compacted Dry	3					
Polymer Coating (Adopt Material Only)	0					
Plasticized PVC Material Only	0.000					
Pipe ID / Wall thickness (in)	17.91					
Pipe Area (in^2) (2D)	1,313					
Pipe ID Radius (in)	9.013					
Polymer Coating (Adopt, E = 30 GPa)	30 GPa					
Ring Compacted Material (only, E = 10 GPa)	10 GPa					
C factor (kN)	0.149					
Number of Joints per 100' Average Length	5.162					
Number of Joints per 100' Average Length (from conservative check)	6.640					
Failure Coefficient						
External Shear	32.6					
Ring Compression Shear	3000.1					

Shear Adhesion Parameters

S-C	7.15	Instrumentation & Control Engineering - Current Analysis & Current Components of Pipe and Soil Interface Integrity				
S-T	10.3	Instrumentation & Control Engineering - Current Analysis & Current Components of Pipe and Soil Interface Integrity				
Pipe Material ID#	401	401	401	401	401	401

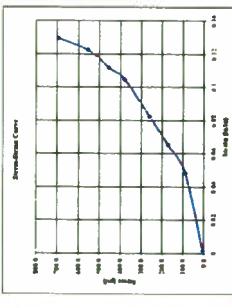
Ring Shear Factor

Ring Shear Force (kN)

Ring Shear Force

Shear Strength (kN)

Pipe Material ID#	401	401	401	401	401	401
Soil ID#	401	401	401	401	401	401
Vertical Soil Stress (kN)	104.8	104.8	104.8	104.8	104.8	104.8
Shear Strength (kN)	20.96	20.96	20.96	20.96	20.96	20.96
Max Shear Force (kN)	20.96	20.96	20.96	20.96	20.96	20.96



Graph of Vertical Load vs. Vertical Deformation

Y-axis: Vertical Load (kN)
X-axis: Vertical Deformation (mm)

Legend:
 ■ C factor in Service Condition
 ■ Critical C factor
 ■ Critical C factor in Service Condition
 ■ Critical C factor in Design Condition
 ■ Critical C factor in Design Condition

Critical C factor = 0.056564 kN/mm²

0.056564

kN/mm²

Individual test	CROWN			SPRINGLINE				
	Initial Service, per initial depth	Initial Service, per final depth	Final Service, per final depth	Initial Service, per initial depth	Initial Service, per final depth	Final Service, per final depth		
9.14	174.2	64.2	515.0	171.9	130.6	427.9	227.9	84.4
9.44	171.0	91.9	497.8	170.2	111.0	300.6	200.6	70.9
9.14	169.6	125.1	493.9	169.5	109.5	260.0	192.1	71.4
9.44	170.1	101.6	511.4	210.0	171.8	311.5	201.6	70.1
10.14	169.8	171.0	497.3	168.6	175.6	211.7	163.9	67.9
10.44	169.3	171.6	494.1	161.1	164.6	252.4	161.3	63.1
11.14	177.5	219.9	499.9	217.7	169.5	351.2	217.9	64.6
11.44	171.8	241.6	499.5	162.2	171.0	349.3	162.9	61.9
12.14	227.9	351.0	476.6	311.5	271.7	371.1	272.9	61.8
12.44	170.6	344.9	424.7	140.2	271.1	344.7	204.9	51.2
13.14	271.4	321.4	321.9	310.8	223.9	371.7	211.1	51.1
13.44	264.7	271.0	369.7	271.7	188.9	376.6	211.9	51.5
14.14	270.3	307.6	471.6	225.7	184.6	327.1	276.9	50.7
14.44	287.1	346.3	388.1	310.6	164.5	326.7	206.0	50.0
15.14	277.9	334.5	471.1	224.2	181.2	322.6	209.5	50.1
15.44	266.0	339.2	386.3	266.0	220.7	320.1	201.6	51.9
16.14	217.0	344.0	327.1	217.1	207.7	320.0	202.6	52.4
16.44	226.1	351.1	351.1	221.2	217.7	320.6	201.6	50.3
17.14	221.9	379.3	367.7	216.2	206.6	324.1	201.1	51.6
17.44	247.2	364.7	461.9	169.8	171.6	321.7	201.2	51.1
18.14	346.0	371.3	471.3	325.6	217.3	320.5	201.1	51.2
18.44	271.6	376.9	344.9	213.2	184.9	319.9	201.8	51.5
19.14	291.1	361.4	321.2	211.1	163.6	317.4	201.2	51.6
19.44	343.9	381.3	326.4	216.6	186.5	315.9	201.5	51.9
20.14	261.2	371.9	371.9	215.5	204.3	316.5	201.3	51.7
20.44	346.9	346.9	377.9	211.8	188.0	314.8	201.8	51.2

BURIED PLASTIC PIPE LOADING WORKSHEET V2.0



Printed based on ASCE Standard:



[Project CFAI Plan 3 Secondary Plan - 12" G3 PVC Pipe](#)

On - Line
Date: March 2020

Area: Comparison to ground surface (inches)

SACL and PPE: Safety Data

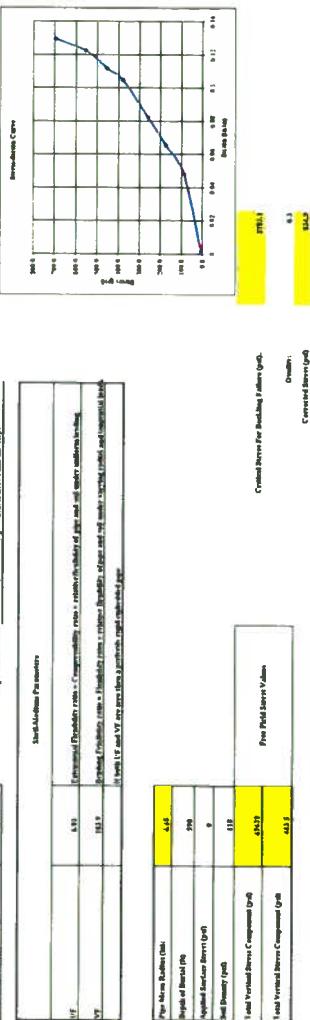
Input Parameters & Assumptions

Material	Coeffice	Profile Angle	C over ground Headline	Laminate Ratio	E
CPE	0.75	45	0.724	0.337	5.071
PVC Schedule 40	0	45	0.724	0.337	5.071
PVC Schedule 80	0	45	0.724	0.337	5.071

Input Parameters & Assumptions

Parameter	Value
Pipe Diameter (in)	12.00
Pipe ID (in)	11.17
Height of Pipe (in)	5.19
Pipe Compacted (yes)	No
Pyramidal Coefficient of Reduction (yes)	No
Pyramidal Coefficient of Reduction (no)	2000
Pipe Wall Thickness (in)	0.13
Pipe Axis (in) (ft)	5.12
Polymer Material (poly. e)	-0.005
Plastic Compaction Factor (yes) Z =	No
Z Factor (ft)	0.00
Z Factor of Filled Soil (ft) When Uncompacted	0.00
Z Factor of Filled Soil (ft) When Compacted	0.00
Soil Compressive Modulus (ft-lb)	0.010
Number of Cells (ft^2)	1000
Radius of Influence (ft)	5.000
Radius of Influence (m)	15.240
Rubber Cylinders	None
Rubber Dumbells	None
Steel Cylinders	None

Applied Vertical Load & Vertical Stress (inches)



Concrete Structural Strength

Concrete Structural Strength	Concrete Structural Strength (yes)	Concrete Structural Strength (no)
Concrete SFC (psi)	4.44	
Concrete SFC (kPa)	270	
Concrete SFC (MPa)	0	
Total Density (g/cm³)	1.19	
Total Vertical Surface Component (in)	620.23	
Total Vertical Surface Component (ft)	40.6	

Point Yield Stress Values

Point Yield Stress Values	Point Yield Stress Values (yes)	Point Yield Stress Values (no)
Point Yield Stress Values (yes)	4.13	
Point Yield Stress Values (no)		53.5

Latitude (deg)	CROWN			SPRINGLINE		
	Stable Survey, prof (m)	Unstable Survey, prof (m)	Stable Survey, prof (m)	Stable Survey, prof (m)	Unstable Survey, prof (m)	Stable Survey, prof (m)
4.65	175.6	177.2	180.6	193.9	181.9	185.6
7.15	189.7	189.3	177.8	112.5	189.8	188.9
7.65	176.2	177.2	174.2	121.8	121.6	121.9
8.15	169.7	169.1	161.3	172.3	153.9	161.0
8.65	176.5	175.9	166.9	131.7	144.9	137.7
9.15	201.4	201.8	201.4	143.2	170.8	151.6
9.65	178.2	182.0	182.9	131.6	129.3	121.9
10.15	215.7	215.2	214.3	180.3	179.1	169.9
10.65	211.6	209.3	181.9	122.6	170.6	151.9
11.15	168.6	170.0	174.0	134.3	139.3	127.8
11.65	220.6	218.8	209.8	212.7	204.2	196.6
12.15	271.6	281.7	277.7	181.7	181.1	121.7
12.65	205.6	214.1	167.6	181.7	189.7	120.9
13.15	261.3	244.5	258.9	213.9	210.2	121.7
13.65	280.3	251.6	251.4	117.6	121.8	99.6
14.15	171.6	171.6	161.9	167.2	173.2	122.4
14.65	260.2	260.2	261.6	135.7	131.6	121.6
15.15	181.3	181.3	181.3	181.3	181.3	181.3
15.65	242.1	242.1	242.1	212.9	212.9	121.6
16.15	184.8	174.6	174.6	211.1	214.8	181.6
16.65	201.4	215.9	186.5	188.6	189.8	121.3
17.15	271.3	271.3	179.9	176.8	173.3	101.1
17.65	263.5	263.5	163.5	210.9	205.7	111.9
18.15	189.8	187.4	181.7	204.6	212.7	98.1
18.65	211.5	211.5	181.6	191.6	181.7	101.2
19.15	187.5	181.4	186.4	186.4	186.4	101.3
19.65	201.6	201.6	196.6	196.6	196.6	101.3

BURIED PLASTIC PIPE LOADING WORKSHEET V2.0

Printed Name _____ Date _____

SAC _____ _____ _____

Project CCA 17' Blue N' Polymer Pipe 14" OD SDR 11

Date March 2010

Line Compensation (1) - None (None = 0.000)

KOLI and API E Input Data



Material	Thickness	Product Angle	Calculated Parameters		
			Laydown Shear Factor	W	C
PVC	.050	W	4.63	5.00	5.51
PE	.048				
Poly Butene (PB)	.045				
Polyethylene (PE)	.040				
Polypropylene (PP)	.038				
Polyvinyl Chloride (PVC)	.035				
Prismatic Contracted Medium (PCM)	.030				
Prismatic Contracted Medium (PCM)	.028				
PVC Wall Thickness (WT)	.028				
Poly Acrylate (PA)	.028				
Patented Medium (PM) &					
Ring Compaction Medium (RC)					
Rigid Compaction Medium (RM)					
Smooth (S)					

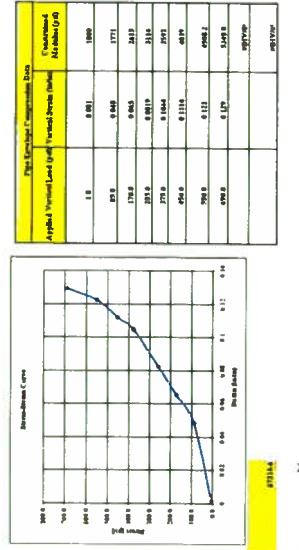
Thickness of Cover Soil (Total cover depth)	3.000	Thickness of Cover Soil (Net cover depth)	2.714
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	

Product Number	4500	Ring Settlement Factor	2.44
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	

Thickness of Cover Soil (Net cover depth)	3.000	Thickness of Cover Soil (Net cover depth)	2.714
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	
Thickness of Cover Soil (Net cover depth)		Thickness of Cover Soil (Net cover depth)	

Ring Settlement Factor	2.44	Ring Settlement Factor	2.44
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	

Ring Settlement Factor	2.44	Ring Settlement Factor	2.44
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	
Ring Settlement Factor		Ring Settlement Factor	



Backfill Compaction Ratio
W = 0.500
C = 0.500

Backfill Compaction Ratio
W = 0.500
C = 0.500

Business (cont'd)	CROWN			SPRINGLINE		
	Initial Service and final days	Initial Service, first days	Stop Service, first days	Initial Service and final days	Initial Service, first days	Stop Service, first days
1.175	595.5	257.2	771.9	525.9	451.9	607.0
1.176	597.6	279.8	469.9	579.6	497.4	571.6
1.177	607.6	251.2	431.3	563.3	479.7	579.7
1.178	670.6	469.7	564.2	546.5	516.2	529.1
1.179	461.0	493.2	519.0	345.7	471.4	517.1
1.180	651.3	414.2	481.0	321.6	471.7	506.6
1.181	511.7	471.1	413.3	212.9	471.3	412.3
1.182	451.2	471.4	411.7	344.2	471.1	471.6
1.183	474.4	451.8	411.3	311.8	471.5	471.1
1.184	555.9	476.9	511.0	341.5	471.7	471.9
1.185	399.2	564.9	346.7	241.3	471.3	471.7
1.186	482.1	511.8	511.6	341.3	471.8	471.1
1.187	461.6	521.3	346.8	241.1	471.1	466.6
1.188	477.3	572.9	347.9	241.3	471.3	471.7
1.189	477.1	511.9	521.6	341.3	471.1	519.5
1.190	491.1	541.3	511.3	341.2	471.3	519.3
1.191	487.1	461.1	366.3	241.4	471.1	471.1
1.192	471.1	561.5	370.1	341.1	471.6	504.6
1.193	477.5	599.9	374.8	341.4	471.6	516.5
1.194	511.8	561.2	379.1	341.2	471.5	477.8
1.195	511.9	561.2	379.1	341.2	471.9	471.7
1.196	566.4	562.9	379.9	411.4	471.1	517.9
1.197	511.1	571.5	381.2	341.9	471.2	461.9
1.198	511.7	579.2	379.0	241.1	469.9	467.1
1.199	566.6	579.7	379.6	341.2	471.0	464.8
1.200	511.2	571.9	373.5	341.5	375.9	371.1
1.201	464.4	566.5	380.3	307.1	444.6	344.3
1.202	561.3	560.6	380.4	307.1	444.6	444.6

Line Number	CROWN				SPRINGLINE			
	Inside Depth inches (in)	Inside Depth, grad (in) depth	Outside Depth, grad (in) depth	Outside Depth, grad (in) depth	Inside Depth, grad (in) depth	Inside Depth, grad (in) depth	Outside Depth, grad (in) depth	Outside Depth, grad (in) depth
9 32	771.9	49.7	1151.1	251.6	161.9	272.9	211.6	1211.1
10 32	771.3	108.6	994.9	275.9	214.6	295.9	413.8	1114.9
11 32	771.2	121.1	899.6	251.7	207.5	218.6	476.9	1271.1
12 32	771.0	105.6	916.6	261.9	201.7	219.1	417.9	1211.3
13 32	771.2	101.6	721.1	208.1	120.8	185.9	561.8	909.8
14 32	813.7	210.9	649.3	214.8	179.5	272.9	397.6	914.6
15 32	372.2	244.4	575.3	377.9	515.5	421.0	511.9	914.6
16 32	261.7	249.2	579.7	319.9	251.9	311.3	547.3	891.8
17 32	260.6	204.6	515.4	379.3	277.1	329.9	441.0	861.1
18 32	261.0	211.8	511.3	318.9	279.6	321.6	583.6	846.8
19 32	377.6	200.1	487.9	218.8	346.8	427.8	641.0	841.9
20 32	311.6	471.6	453.1	416.7	346.1	321.3	448.6	817.9
21 32	361.9	364.2	415.7	315.1	279.3	323.9	473.7	891.3
22 32	243.5	377.9	428.7	314.6	377.6	411.7	477.7	791.8
23 32	377.5	371.6	411.7	311.6	279.6	311.4	440.9	731.9
24 32	379.5	404.8	496.6	309.7	353.2	317.0	483.1	714.8
25 32	383.2	491.1	480.9	367.9	398.7	311.7	468.9	761.9
26 32	371.0	449.9	377.5	305.6	416.6	412.4	468.1	770.7
27 32	406.2	411.3	394.2	306.2	345.3	310.2	467.8	751.2
28 32	413.8	491.3	461.0	361.1	444.3	395.9	487.9	744.3
29 32	411.7	449.7	469.1	393.1	396.3	397.7	467.6	760.8
30 32	412.2	491.3	464.3	395.3	345.9	361.9	468.9	725.9
31 32	441.1	377.4	461.3	329.6	349.2	381.9	487.9	711.8
32 32	451.8	471.0	414.6	329.3	311.5	360.9	467.7	717.5
33 32	451.5	471.2	415.7	325.6	313.9	372.3	467.7	721.5
34 32	311.6	311.6	511.9	256.8	323.2	314.9	581.3	886.1
35 32	311.6	311.6	511.9	256.8	323.2	314.9	581.3	886.1
36 32	311.6	311.6	511.9	256.8	323.2	314.9	581.3	886.1

Building #	CROWN				SPRINGLINE			
	Build. Areas, per 1000 sq ft							
814	879.0	74.2	1184.8	265.2	105.7	273.6	1195.5	
844	179.6	11.0	945.6	211.4	207.0	245.6	1109.8	
914	107.1	10.7	945.1	177.6	105.1	210.5	1029.7	
944	270.3	19.9	105.8	207.3	31.9	104.9	984.6	
1034	211.7	21.0	674.2	183.0	41.8	140.0	951.2	911.9
1044	157.9	20.6	616.7	137.1	34.9	110.0	897.7	917.3
1134	277.6	27.8	564.0	118.4	39.7	177.6	848.3	877.9
1144	276.9	26.4	561.1	115.6	39.8	171.3	845.6	851.3
1234	270.6	27.3	611.6	119.2	34.5	119.3	871.1	852.6
1244	311.3	30.7	611.7	119.9	34.6	114.9	845.7	815.0
1314	243.4	20.4	461.9	214.8	36.1	254.3	671.1	686.8
1344	270.7	27.4	611.1	111.9	39.8	131.3	876.9	
1414	361.9	40.3	601.1	209.7	35.3	110.4	840.1	775.4
1444	271.3	21.9	270.6	107.4	151.2	195.6	487.7	485.7
1514	296.9	32.7	577.1	205.1	36.9	111.7	894.7	777.6
1544	367.0	45.4	364.6	261.8	46.6	110.8	485.6	749.2
1614	412.3	47.1	270.8	200.6	54.3	107.5	482.2	524.5
1644	612.9	617.5	245.2	270.5	33.9	265.9	426.6	734.6
1714	444.8	477.5	346.6	274.0	34.5	801.4	420.7	719.9
1744	479.0	477.1	541.9	274.4	34.2	100.1	420.6	711.6
1814	604.5	605.7	405.1	177.8	37.8	177.9	426.5	731.5
1844	674.6	581.1	521.2	225.7	34.8	275.8	420.9	711.8
1914	681.7	519.2	317.6	237.0	34.8	271.8	420.6	711.6
1944	607.6	517.0	313.8	237.6	34.3	211.3	420.6	711.6
2014	476.9	521.1	297.9	227.8	37.3	176.1	424.2	707.4
Avg Values	341.6	341.3	791.2	246.7	120.5	112.8	516.3	1040.7
Sed. Averages	Prohibited Areas							

Line-Item ID#	CROWN			SPRINGLINE		
	Initial Service, pre-fit days	Staged Service, pre-fit days	Final Service, pre-fit days	Initial Service, post-fit days	Staged Service, post-fit days	Final Service, post-fit days
1.23	119.0	173	110.7	162.2	171.6	205.9
1.71	215.2	211.9	147.3	114.7	104.7	97.6
1.22	172.0	116.6	150.4	114.8	112.2	103.9
1.71	209.1	209.1	115.9	207.7	164.9	204.6
1.21	411.9	411.1	161.7	279.6	151.9	179.9
1.72	651.4	497.2	311.1	271.1	197.3	611.6
1.22	651.2	619.9	311.3	229.9	171.1	611.3
1.71	211.2	212.0	297.7	209.7	194.6	197.7
1.21	611.5	611.9	161.9	276.8	207.9	177.0
1.72	561.9	576.6	311.9	271.8	206.3	177.8
1.21	611.8	611.6	177.4	219.8	219.4	171.9
1.71	671.1	670.3	171.1	167.6	170.1	171.3
1.22	651.2	651.2	287.7	169.3	126.8	189.7
1.71	209.2	169.4	167.8	164.8	171.7	171.7
1.21	209.3	169.7	164.9	164.9	171.6	171.3
1.71	601.5	611.3	311.9	146.7	171.9	181.3
1.22	407.5	411.1	261.6	265.8	172.6	216.9
1.71	611.0	611.0	161.5	204.5	179.5	206.9
1.22	611.5	611.6	212.6	229.9	207.7	166.3
1.72	611.6	611.6	177.9	259.6	167.6	167.7
1.21	611.7	611.7	177.9	259.6	167.6	167.7
1.71	611.3	611.3	177.9	279.1	161.1	124.6
1.22	427.6	411.7	161.7	163.2	121.1	174.0
1.71	429.0	151.1	151.1	151.7	211.1	192.5
1.21	521.0	124.7	181.1	226.2	211.5	161.5
1.71	521.0	124.7	181.1	226.2	211.5	161.5
1.22	521.0	124.7	181.1	226.2	211.5	161.5
1.71	521.0	124.7	181.1	226.2	211.5	161.5

Block (Rep)	CROWN			SPRINGLINE		
	Initial Scores, pre (Rep)	Initial Scores, post (Rep)	Change Scores, pre (Rep)	Initial Scores, pre (Rep)	Initial Scores, post (Rep)	Change Scores, pre (Rep)
1.11	434.9	327.5	-107.4	260.7	461.6	89.3
1.11	276.3	277.4	1.1	345.7	416.9	71.2
1.11	397.9	377.6	-20.3	323.7	419.1	95.4
1.11	444.9	397.3	-47.6	265.7	411.5	45.8
1.11	491.9	361.3	-130.6	351.1	424.9	73.8
1.11	518.6	397.3	-121.3	254.9	381.1	126.2
1.11	533.6	373.8	-160.8	195.9	311.1	115.2
1.11	551.9	394.6	-157.3	262.2	349.8	87.6
1.11	565.6	411.9	-153.7	231.7	321.7	90.0
1.11	570.5	411.4	-159.1	201.2	341.9	140.7
1.11	580.3	417.4	-162.9	279.3	318.9	39.6
1.11	596.3	421.2	-175.1	278.8	343.7	64.9
1.11	611.9	434.4	-177.5	226.1	329.8	103.7
1.11	629.9	472.9	-157.0	271.3	379.9	108.0
1.11	633.5	432.3	-161.2	249.9	328.1	78.2
1.11	617.6	424.6	-153.1	241.7	324.1	82.4
1.11	613.9	423.7	-150.2	249.7	371.9	122.2
1.11	621.2	432.4	11.2	326.4	371.4	45.0
1.11	641.9	431.9	-109.0	349.1	377.1	28.0
1.11	651.2	461.7	-150.5	329.2	371.9	42.7
1.11	651.3	461.5	-150.8	347.9	377.5	30.6
1.11	651.9	461.9	0.0	349.6	377.4	27.8
1.11	654.3	461.2	-153.1	349.8	377.6	27.8
1.11	654.9	461.5	-153.4	349.6	377.6	28.0
1.11	654.9	461.1	-153.8	349.9	377.2	27.3
Avg Values	437.6	361.6	-76.0	271.8	346.8	75.0
Std. Deviation	847.5	423.9	423.9	321.9	155.3	200.3



SMITH WILLIAMS CONSULTANTS, INC.

Appendix C.3.2

Phase 5 VLF Primary Solution Collection Pipe Burial Calculations



SMITH WILLIAMS CONSULTANTS, INC.

CALCULATION TITLE PAGE

CLIENT Cripple Creek & Victor Gold Company	JOB NO. 1125	TASK NO. A100	PAGE 1 OF 3
PROJECT Arequa VLF	CALCULATION No. 1	REV. No. 1	
SUBJECT/ TITLE Primary Pipe Design			
REV. NO.	PREPARER/ DATE	REVIEWER/ DATE	QA REVIEWER/ DATE
1	Amanda L. Dolezal 1/8/08	Derek T. Wittwer 1/26/08	<i>JL Lupo</i> 1/26/08

CALCULATION OBJECTIVE

Size the primary collection pipes in order to handle the maximum flow.

CALCULATION METHODOLOGY/ LIST of ASSUMPTIONS

- $Q_{total} = 14,400 \text{ gpm}$, distribute flow to 3 pipes.
- Consider flow only in primary pipes, not the primary / riser interaction.
- Add factor of safety of 25% for flow of 18,000 gpm for zero deformation.
- Distribute flow evenly between the three pipes for design flow in each pipe of 6,000 gpm.

REFERENCES

Watkins, R., "Plastic Pipes Under High Landfills", 1990, Buried Plastic Pipe Technology, ASTM-STP.1093.
Lupo, J., "Stability of HDPE Pipes Under High Heap Loads", 1991, SME, Denver, Colorado.

CONCLUSIONS

- 26" O.D. pipe with SDR 11 will support the necessary quantities of flow and loads without any deformation.



SMITH WILLIAMS CONSULTANTS, INC.

PROJECT: Arequa VLF	JOB NO: 1125	SHEET <u>2</u> OF <u>2</u>
FEATURE: Primary Solution Collection Pipe	BY: ALD	DATE: 1/8/08
DETAILS: Pipe Sizing	CHKD BY: DTW	DATE: 1/26/08

• Criteria:

- 1) Use pressurized pipe flow calculation.

• Analysis:

Total length = 1200 feet

Average ground slope = 0.004 = 0.4%

Elevation Head = 1200 ft * 0.004 = 4.8 feet

Differential Head = calculate to get $Q \approx 6,000 \text{ gpm}$

Use modified pipe deformation method in Lupo (1991) to test pipe deformation for both maximum and average ore height in PSSA.

Assume pipe is 26" O.D. with SDR of 11, check deformation, check flow, then verify SDR is appropriate.

Attached sheets have pipe deformation calculations for maximum ore height (590 feet).

Results indicate pipe crown deflection of between 10 and 12% (less than 15% threshold), and crown pressures of between 260 and 418 psi. Tensile stresses are less than 1000 psi.

Ignore horizontal strains as these are over predicted.

Deformed pipe analysis indicates a 19% reduction in flow due to maximum crown deflection:

$$Q_{\text{def(max)}} = 6,395 \text{ gpm} * 0.81 = 5,180 \text{ gpm} \text{ (greater than 4,800 gpm)}$$

Deformed pipe analysis indicates a 16% reduction in flow due to minimum crown deflection:

$$Q_{\text{def(min)}} = 6,395 \text{ gpm} * 0.84 = 5,372 \text{ gpm} \text{ (greater than 4,800 gpm)}$$

Now verify SDR 11 is appropriate for loading. Use empirical approach using Watkins Equation.

$$\sigma_R = 0.5P(1+d) \text{ SDR} \quad \text{per Watkins (see Lupo, 1991)}$$

Performance of plastic pipe is governed by:

- 1) ring crushing
- 2) ring deformations

ring deflection \approx vertical strain of pipe envelope

σ_R = ring compression (allowable is 1500psi - Driscopipe)

d = crown deflection (varies between 10 and 12%)

SDR = pipe SDR ratio

$$1500 \text{ psi} = (0.5)^*(420 \text{ psi})^*(1+0.12)\text{SDR}$$

$$\text{SDR} = 6.4 \approx 7 \text{ for maximum ore height}$$

Therefore SDR 11 is suitable for this maximum condition in the PSSA.



8/8

Nom. Size (in)	DR	Weight lb/100ft	Dimensions, Inches			Coil/ Joint feet
			OD	Approx. ID	Min.Wall	
22	9.0	6540	22.000	17.112	2.444	20/40/50
	11.0	5482		18.000	2.000	20/40/50
	13.5	4556		18.740	1.630	20/40/50
	17.0	3680		19.412	1.294	20/40/50
	21.0	3018		19.904	1.048	20/40/50
	26.0	2461		20.308	0.846	20/40/50
24	9.0	7785	24.000	18.666	2.667	20/40/50
	11.0	6524		19.636	2.182	20/40/50
	13.5	5421		20.444	1.778	20/40/50
	17.0	4381		21.176	1.412	20/40/50
	21.0	3591		21.714	1.143	20/40/50
	26.0	2930		22.154	0.923	20/40/50
26	11.0	7657	26.000	21.272	2.364	20/40/50
	13.5	6362		22.148	1.926	20/40/50
	17.0	5139		22.942	1.529	20/40/50
	21.0	4214		23.524	1.238	20/40/50
	26.0	3439		24.000	1.000	20/40/50
28	11.0	8878	28.000	22.910	2.545	20/40/50
	13.5	7378		23.852	2.074	20/40/50
	17.0	5962		24.706	1.647	20/40/50
	21.0	4886		25.334	1.333	20/40/50
	26.0	3988		25.846	1.077	20/40/50
30	13.5	8469	30.000	25.556	2.222	20/40/50
	17.0	6845		26.470	1.765	20/40/50
	21.0	5612		27.142	1.429	20/40/50
	26.0	4578		27.692	1.154	20/40/50
800mm	13.5	9335	31.496	26.830	2.333	20/40/50
	17.0	7545		27.790	1.853	20/40/50
	21.0	6185		28.496	1.500	20/40/50
	26.0	5044		29.074	1.211	20/40/50
32	13.5	9635	32.000	27.260	2.370	20/40/50
	17.0	7786		28.236	1.882	20/40/50
	21.0	6384		28.952	1.524	20/40/50
	26.0	5210		29.538	1.231	20/40/50

Typical Physical Properties* of Driscopipe® 1000 (PE 3408) Polyethylene Pipe Resin

Property	Test Method	Unit	Value
Material Designation	PPI / ASTM	-----	PE 3408
Material Classification	ASTM D 3350	-----	Type III; PE34
Cell Classification	ASTM D 3350	-----	345464C
Density (3)	ASTM D 1505	gms/cm ³	0.955
Melt Flow (4)	ASTM D 1238(2.16/190)	gms/10 min.	0.11 ♦
Flex Modulus (5)	ASTM D 790	psi	110,000
Tensile Strength (4)	ASTM D 638	psi	3,200
PENT (6)	ASTM F 1473	Hours	>100
HDB @ 73.4°F (4)	ASTM D 2837	psi	1,600
U-V Stabilizer (C)	ASTM D 1603	% C	> 2
Hardness	ASTM D 2240	Shore D	65
Tensile Strength @ Yield (Type IV Specimen)	ASTM D 638 (2"/min.)	psi	3,200
Tensile Strength @ Break (Type IV Specimen)	ASTM D 638	psi	5,000
Elongation at Break	ASTM D 638	%, minimum	750
Modulus of Elasticity (Young's Modulus)	ASTM D 638	psi	130,000
ESCR (Cond A,B, C: Mold. Slab) (Compressed Ring - pipe)	ASTM D 1693 ASTM F 1248	F _o , Hours F _o , Hours	>5,000 >3,500
PENT	ASTM F 1473	Hours	>100
Impact Strength (IZOD) (.125" Thick)	ASTM D 256 (Method A)	In-lb/in. notch	42
Linear Thermal Expansion Coeff.	ASTM D 696	in/ in/ °F	1.2 x 10 ⁻⁴
Thermal Conductivity	ASTM D 177	BTU-in/ft ² / hrs/°F	2.7
Brittleness Temperature	ASTM D 746	°F	< -180
Vicat Softening Temperature	ASTM D 1525	°F	257

*This list of typical physical properties is intended for basic characterization of the material and does not represent specific determinations or specifications. The physical properties values reported herein were determined on compression molded specimens prepared in accordance with Procedure C of ASTM D-1928 and may differ from specimens taken from the pipe.

♦ Average Melt Index value with a standard deviation of 0.01

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PIPEFLOW WORKSHEET

Project Name:	CC&V Arequa VLF	
Client:	CC&V	
Date:	1/18/2008	
Pipe Description:	3 primary pipes 14,400gpm total FOS 1.25	
Hazen-Williams		
Parameter	Units	Units
Q	6000 gpm	379 l/s
C factor	150	
Pipe Inside Diameter	20.989 inches	
Pipe loss per 100 ft	0.1563 psi/100 ft.	
Equivalent Water Level:	0.3608 ft. of water	
Hydraulic Gradient	0.0036 ft/ft	
Pipe Inside Diameter	20.989 inches	
Upgradient Elv. (ft)	9730	2966.5 m
Upgradient Water Elv. (ft):	9745	2971.0 m
Downgradient Elv. (ft):	9725	2964.9 m
Downgradient Water Elv. (ft):	9740	2969.5 m
Pipe Elv. Change (ft):	5	1.5 m
Pipe Elevation Change	5	1.5 m
Hydraulic Elv. Change	5	1.5 m
Pipe Length	1255	382.6 m
Slope of Pipe:	0.004	
C factor	150	
Fittings Equivalent Length:	0 feet	
hydraulic gradient	0.00 ft/ft	
Q Max.	6,395 gpm	
Q	14.25 cfs	
Q	403.43 lps	
Velocity	5.93 fps	
Total Head loss (ft)	4.58	



Bore Dia.	CROWN				SPRINGLINE			
	Radius	Radius Sag	Radius Sag	Sag	Radius Sag	Radius Sag	Radius Sag	Sag
11.79	417.2	207.9	503.2	-	170.0	161.7	161.6	0.61.2
11.80	205.1	205.1	409.8	-	163.2	165.7	165.5	0.61.4
11.79	275.7	275.7	515.3	170.0	163.2	161.3	161.2	0.61.1
11.79	261.7	261.7	505.1	171.3	164.2	163.0	162.9	0.61.6
11.79	275.6	275.6	510.8	170.3	167.2	162.9	162.6	0.61.3
11.80	206.8	206.8	408.8	-	170.4	168.3	167.8	0.61.7
11.79	207.0	207.0	409.8	211.4	174.6	167.6	167.5	0.61.9
11.80	205.7	205.7	408.9	212.8	174.3	166.8	166.7	0.61.8
11.79	261.6	261.6	505.0	207.0	173.0	165.9	165.8	0.61.6
11.79	206.9	206.9	408.9	-	170.2	168.1	167.8	0.61.7
11.80	205.1	205.1	407.8	-	170.5	167.6	167.5	0.61.8
11.79	261.0	261.0	505.1	204.1	171.7	164.8	164.7	0.61.9
11.79	205.2	205.2	407.6	-	171.1	171.5	170.5	0.61.7
11.79	205.9	205.9	407.3	211.8	172.9	169.5	169.4	0.61.5
11.80	207.9	207.9	408.4	214.6	174.0	167.6	167.5	0.61.6
11.79	261.1	261.1	504.3	204.3	174.1	166.6	166.5	0.61.7
11.80	261.3	261.3	504.3	204.3	174.1	165.4	165.3	0.61.8
11.79	206.3	206.3	408.3	-	171.4	168.2	167.8	0.61.7
11.79	261.5	261.5	504.5	201.1	174.9	164.3	164.2	0.61.9
11.80	205.9	205.9	407.1	204.0	174.5	165.0	164.9	0.61.7
11.79	205.4	205.4	406.4	-	170.8	170.5	170.4	0.61.9
11.79	271.4	271.4	512.4	209.1	175.9	167.7	167.6	0.61.8
11.79	205.6	205.6	406.6	-	172.8	168.6	168.5	0.61.8
11.79	261.7	261.7	505.1	205.1	175.1	172.6	172.5	0.61.9
11.79	207.7	207.7	410.6	215.9	176.8	169.6	169.5	0.61.6
11.80	207.2	207.2	409.8	215.6	176.6	169.3	169.2	0.61.7
11.79	261.9	261.9	505.1	207.9	176.9	172.2	172.1	0.61.8
11.80	206.4	206.4	406.4	-	175.3	169.7	169.6	0.61.6

Estimate Percent Flow Reduction of Deformed Pipe (Min.)

Project: CC&V Arequa
Date: January 2008
By: Dolezal
Project #: 1125

Max. Ore Height = 590 feet



$$FlowFactor = AR^{\frac{2}{3}}$$

A = Flow Area
R = Hyd. Radius

Circular Pipe Flow

Inside Diameter (inches)	Area Ft^2	Hyd. Radius ft.	Flow Factor
16.00	1.40	0.33	0.67
18.00	1.77	0.38	0.92
20.00	2.18	0.42	1.22
22.00	2.64	0.46	1.57
24.00	3.14	0.50	1.98
26.00	3.69	0.54	2.45
28.00	4.28	0.58	2.99
30.00	4.91	0.63	3.59
32.00	5.59	0.67	4.26
34.00	6.31	0.71	5.01
36.00	7.07	0.75	5.83

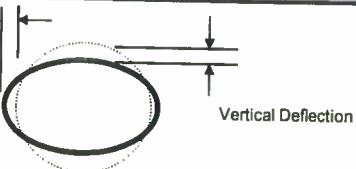
Horizontal Deflection

Ellipse-Shape Pipe Flow

Max. Vertical Pipe Deflection (%): 10

Flow Reduction
0.16

Horizontal Deflection (%): 0



Circular Pipe I.D. (inches)	Vertical Axis	Horizontal Axis	Area Ft^2	Perimeter	Hyd. Radius	Flow Factor
	(in.)	(in.)		(full flow)		
16.00	14.4	16.0	1.26	4.19	0.30	0.56
18.00	16.2	18.0	1.59	4.71	0.34	0.77
20.00	18.0	20.0	1.96	5.24	0.38	1.02
22.00	19.8	22.0	2.38	5.76	0.41	1.32
24.00	21.6	24.0	2.83	6.28	0.45	1.66
26.00	23.4	26.0	3.32	6.81	0.49	2.06
28.00	25.2	28.0	3.85	7.33	0.53	2.50
30.00	27.0	30.0	4.42	7.85	0.56	3.01
32.00	28.8	32.0	5.03	8.38	0.60	3.58
34.00	30.6	34.0	5.67	8.90	0.64	4.20

Estimate Percent Flow Reduction of Deformed Pipe (Max.)

Project: CC&V Arequa
Date: January 2008
By: Dolezal
Project #: 1125

Max. Ore Height = 590 feet



$$FlowFactor = AR^{2/3}$$

A = Flow Area
R = Hyd. Radius

Circular Pipe Flow

Inside Diameter (inches)	Area Ft^2	Hyd. Radius ft.	Flow Factor
16.00	1.40	0.33	0.67
18.00	1.77	0.38	0.92
20.00	2.18	0.42	1.22
22.00	2.64	0.46	1.57
24.00	3.14	0.50	1.98
26.00	3.69	0.54	2.45
28.00	4.28	0.58	2.99
30.00	4.91	0.63	3.59
32.00	5.59	0.67	4.26
34.00	6.31	0.71	5.01
36.00	7.07	0.75	5.83

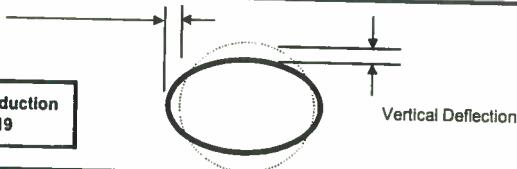
Horizontal Deflection

Ellipse-Shape Pipe Flow

Max. Vertical Pipe Deflection (%): 12

Flow Reduction
0.19

Horizontal Deflection (%): 0



Circular Pipe I.D. (inches)	Vertical Axis (in.)	Horizontal Axis (in.)	Area Ft^2	Perimeter (full flow)	Hyd. Radius	Flow Factor
16.00	14.1	16.0	1.23	4.19	0.29	0.54
18.00	15.8	18.0	1.56	4.71	0.33	0.74
20.00	17.6	20.0	1.92	5.24	0.37	0.98
22.00	19.4	22.0	2.32	5.76	0.40	1.27
24.00	21.1	24.0	2.76	6.28	0.44	1.60
26.00	22.9	26.0	3.24	6.81	0.48	1.98
28.00	24.6	28.0	3.76	7.33	0.51	2.41
30.00	26.4	30.0	4.32	7.85	0.55	2.90
32.00	28.2	32.0	4.91	8.38	0.59	3.44
34.00	29.9	34.0	5.55	8.90	0.62	4.05