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Appendix B.4

Cresson Ore Percolation and Consolidation Tests

Golder Associates Inc.

44 Union Boulevard, Suite 300 Lakewood, CO USA 80228 Telephone (303) 980-0540 Fax (303) 985-2080



October 15, 1999

Our Ref.: 993-2075.003

Cripple Creek & Victor Gold Mining Company P.O. Box 191 2755 State Highway 67 Victor, Colorado 80860

Attention: Mr. Ron Roberts

RE: PERCOLATION-CONSOLIDATION TESTING RESULTS

Golder Associates Inc. (GAI) is pleased to present the results of testing conducted in support of Cripple Creek & Victor Gold Mining Company's (CC&V) Valley Leach Facility. This report details the results for gradation and percolation versus consolidation testing performed on a sample of Cresson ore.

1.0 MATERIAL DESCRIPTION

A sample of Cresson ore was provided by CC&V and used in the percolation-consolidation testing program. The general ore sample gradation and description is provided below and summarized in Table 1:

U.S. Standard Sieve Size	Percent Passing
3-inch	100
1-1/2 inch	89
3/4 inch	64
3/8-inch	. 45
No. 4	31
No. 40	11
No. 200	б

The sample classifies as a fine to coarse gravel with some fine to coarse sand with little fines (Figures 1 and 2).

2.0 CONSOLIDATION AND PERCOLATION TESTING

Consolidation and percolation testing was conducted on the Cresson ore sample. The sample was incrementally loaded to a maximum stress of 432 pounds per square inch (psi) consolidation pressure [equivalent to a heap height of 565 feet based on a bulk ore density

of 110 pounds per cubic foot] and measured for compression, settlement and maximum percolation rate at select load increments. The maximum test pressure of 432 psi is the maximum capacity of the testing apparatus.

2.1 Test Apparatus

The testing apparatus consisted of a 12-inch nominal inside diameter (ID) aluminum tube (testing cell), approximately 18 inches in height. Figure 3 shows the assembled testing cell. The cell was clamped to the base plate and the tie-down rods anchored to the cell base plate. A porous loading plate was placed in contact with the material and a hydraulic jack was used to apply the force to the sample against the top plate. A digital pressure transducer was used to monitor the applied load and a dial gauge measured deformation. The load from the hydraulic jack is adjusted to maintain the desired loading stress throughout the test.

2.2 Test Configuration

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Figure 4 shows the Cresson ore sample prior to testing. The Cresson ore material was placed into the test testing cell (Figure 5), the initial sample height was recorded and the loading plate was secured. The sample was loaded in five increments to approximately 27, 54, 108, 216, and 432 psi. The load increments correspond to ore depths of 35, 70, 140, 280, and 565 feet, respectively, assuming a bulk ore density of 110 pounds per cubic foot (pcf). Vertical displacement values were recorded at each load increment. The sample was loaded to the next increment only after consolidation had ceased. The sample was saturated with water and allowed to drain prior to the first load being applied.

The percolation rate of the material was measured by applying tap water with an electromagnetic pump to simulate various solution application rates. The initial application rate was 0.0045 gallons per minute per square foot (gpm/sf). At each load increment, the application rate was increased to a maximum rate of 0.045 gpm/sf or until ponding was observed on sample. The application rate of 0.045 gpm/sf is ten times greater than the initial application rate and is the maximum flow rating for the testing frame.

The sample was allowed to equilibrate (i.e. inflow equals outflow) before increasing the application rate. During the entire testing period, the surface of the sample was observed for ponding, which would indicate failure of the sample to percolate water at the given application rate.

2.3 Testing Results

The maximum percolation rates of the material at increasing loads are presented on Table 2. The maximum percolation rate of the material at all loads was measured as 0.045 gpm/sf, ten times the solution application rate used at CC&V. At all tested load increments, no ponding of water was observed.

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After the percolation-consolidation tests were completed, the ore sample was tested for gradation to evaluate mechanical degradation under load. The post-test gradation data are presented in Figures 6 and 7. The post-test gradation data indicate an overall decrease in percentage of the fine gravel fraction, with a corresponding increase in percentage of the fine sand fraction. These results indicate that some mechanical degradation of the Cresson ore does occur under loading. The amount of mechanical degradation is considered insignificant. The percolation test data clearly show the ore is capable of supporting high percolation rates, even under an equivalent heap height of 565 feet.

3.0 CLOSURE

If there are any questions or concerns regarding this report or the test data, please call us at (303) 980-0540.

Sincerely,

GOLDER ASSOCIATES INC.

Hallin for,

David M. Dix Laboratory Manager

John F. Lupo, Ph.D., P.E. Sr. Project Manager

DMD/JFL/llr

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Attachments: Tables Figures TABLES

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TABLE	-
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SUMMARY OF ORE DATA

getting and the second s		_				 _	
ESTS 5							
DITIONAL TEX GOMMENTS (See Notes)							
Apbiti 00 (S							
olFic VITY	1						
SPE(1	-					
DRAIN DOWN MOISTURE	ł	7.8					
USSS SOIL ATTERBERG GRAIN SIZE DISTRIBUTION CLASSI- LLATION LL PL PI 34" #4 #200	9	9					
DISTR FINER	31	35					
N SZR							
SRAI SPIN	64	69					
s Pl	1	1					
TER8 LIMIT	1	1					
AT LL	I	1					
S SOIL ASSI- ATION	GP-GC	GP-GC					
USC CL FIO	ษ	G					
SAMPLE USCS SOIL ATTERBERG GRAIN SIZE DISTRIBUTION ORAIN SPECIFIC ADDITTONALTESTS DEPTH CLASSI- LIMITS % FINER % FINE	1	1					
	E	RE					
LE BER	CRESSON ORE	CRESSON ORE					
SAMPLE NUMBER	SSC	SSC				-	
	CRE	CRE					
	ERC	Sc					
BORING NUMBER	R PE	2 PE					
08 NUN	BEFORE PERC	AFTER PERC					
	B	<					

NOTES:

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TABLE 2

	ara i portani Grafication Jaco		Norman Norman Norman Norman	1501 - 43 f. 11940 11940	in transi Rus Anosi
0.1	0	12.2	0.0	97.7	0.045
- 27	38	11.6	4.9	102.7	0.045
54	76	11.3	7.2	105.3	0.045
108	150	10.9	10.2	108.8	0.045
216	295	10.5	13.5	113.0	0.045
432	578	10.1	17.5	118.4	0.045

PERCOLATION-CONSOLIDATION TEST SUMMARY

1. Ore height calculated using the average bulk density for the applied load.

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FIGURES

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LAKEWOOD, COLORADO

FIGURE 1

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PARTICLE-SIZE ANALYSIS OF SOILS ASTM C 117, C 136, D 421, D 422, D 1140, D 2216, D 2217

CC&V/TECHNIC. 993-2075	AL SUPP(DRT/CO	SAMPLE #: CRESSON ORE DEPTH (ft): BEFORE PERC.			
MOISTURE CON	TENT (As	tested)	***********	#200 WAS	H (Percent Fines)	
Tare		XU		Tare		-
Weight Wet Soil & Tare	e, g	289.36		Weight Soil &	t Tare Before Wash, g	-
Weight Dry Soil & Tare	, g	272.88		Weight Soil &	E Tare After Wash, g	-
Weight Tare, g		32.76		Weight Tare,	g _	-
Weight Water, g		16.48		Weight Fines	Lost, g	-
Weight Dry Soil, g		240.12		Weight Dry S	boil, g	16,683.94
Moisture, %		6.86%		Fines Lost, %		-
	SIEVE	Wt. Ret.	% Ret.	% Pass.	SIEVE	
	6.000*	0.00	0.00%	100.00%	6.000"	
Coarse Gravel	3.000"	0.00	0.00%	100.00%	3.000" Coarse Gravel	
	1.500"	1,865.70	11.18%	88.82%	1.500"	
	1.000 ^ª	4,271.10	25.60%	74.40%	1.000"	
Fine Gravel	0.750"	5,969.00	35.78%	64.22%	0.750" Fine Gravel	
	0.375"	9,175.60	55.00%	45.00%	0.375"	
Coarse Sand	#4	11,509.10	68.98%	31.02%	#4 Coarse Sand	
Medium Sand	#10	13,129.88	78.70%	21.30%	#10 Medium Sand	
	#20	14,190.57	85.06%	14.94%	#20	
Fine Sand	#40	14,817.38	88.81%	11.19%	#40 Fine Sand	
	#60	15,181.78	91.00%	9.00%	#60	
	#100	15,462.78	92.68%	7.32%	#100	
	#200	15,711.91	94.17%	5.83%	#200	
Fines	PAN	16,683.94	0.00%	100.00%	PAN Fines	
% C GRVL:	35.8%			Wet Color:	Fine to coarse GRAV	CL
% F GRVL:	33.2%	69.0%				se sand,
% C SAND:	9.7%		little clay (GP-GC)			-
% M SAND:	10.1%		LL:	LL		
% F SAND:	5.4%	25.2%	PL:	PL	DATE:	20-Sep-99
% FINES:	5.8%		· PI:	PI	TECH:	MK
% TOTAL:	100.0%		Gs:	Gs	REVIEW:	DMD

GOLDER ASSOCIATES INC. LAKEWOOD, COLORADO

FIGURE 2





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14 CC+V/TECH SUFFORT/LO 993-2075 LOAD VS PERCOLATION CRUSHED CRESSOU ORE 10/6/99

FIGURE 4 - Cresson Ore Test Material

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FIGURE 5 - Cresson Ore in Test Cell

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FIGURE 6

PARTICLE-SIZE ANALYSIS OF SOILS ASTM C 117, C 136, D 421, D 422, D 1140, D 2216, D 2217

CC&V/TECHNICAL SUPPORT/CO 993-2075

SAMPLE #: CRESSON ORE DEPTH (ft): AFTER PERC.

MOISTURE CONTENT (As tested) #200 WASH (Percent Fines)						
Tore	2	·			- 4	-
Tare		4A		Tare		-
Weight Wet Soil & Tare		266.97		-	t Tare Before Wash. g	-
Weight Dry Soil & Tare	, g	259.47			& Tare After Wash, g	-
Weight Tare, g		32.96		Weight Tare,	•	-
Weight Water, g		7.50		Weight Fines		-
Weight Dry Soil, g		226.51		Weight Dry S		17,357.02
Moisture, %		3.31%		Fines Lost, %		-
	SIEVE	Wt. Ret.	% Ret.	% Pass.	SIEVE	
	6.000"	0.00	0.00%	100.00%	6.000*	
Coarse Gravel	3.000"	0.00	0.00%	100.00%	3.000" Coarse Gravel	
	1.500"	992.30	5.72%	94.28%	1.500"	
	1.000"	3,577.00	20.61%	79.39%	1.000"	
Fine Gravel	0.750"	5,343.20	30.78%	69.22%	0.750" Fine Gravel	
	0.375"	8,825.70	50.85%	49.15%	0.375"	
Coarse Sand	#4	11.278.10	6 4.98%	35.02%	#4 Coarse Sand	
Medium Sand	#10	13,204.06	76.07%	23.93%	#10 Medium Sand	
	#20	14,597.15	84.10%	15.90%	#20	
Fine Sand	#40	15,330.45	88.32%	11.68%	#40 Fine Sand	
	#60	15,734.95	90.65%	9.35%	#60	
	#100	16,040.60	92.42%	7.58%	#100	
	#200	16,328.41	94.07%	5.93%	#200	
Fines	PAN	17,357.02	0.00%	100.00%	PAN Fines	
% C GRVL:	30.8%			Wet Color:	Fine to coarse GRAVE	T
% F GRVL:	34.2%	65.0%		Description:	with some fine to coars	
% C SAND:	11.1%	05.078		Description.	little clay (GP-GC)	se sanu,
% M SAND:	12.3%		LL:	LL		
% F SAND:	5.7%	29.1%	PL:	PL	DATE:	14-Oct-99
% FINES:	5.9%		PI:	PI	TECH:	DBM/PLB
% TOTAL:	100.0%		Gs:	Gs	REVIEW:	DMD

GOLDER ASSOCIATES INC. LAKEWOOD, COLORADO

FIGURE 7

Golder Associates Inc.

44 Union Boulevard, Suite 300 Lakewood, CO USA 80228 Telephone (303) 980-0540 Fax (303) 985-2080



February 25, 2000

Our Ref.: 993-2075

Cripple Creek & Victor Gold Mining Company P.O. Box 191 2755 State Highway 67 Victor, Colorado 80860

Attention: Mr. Ron Roberts

RE: PERCOLATION-CONSOLIDATION TESTING RESULTS ROM AND MINUS 7/8 ORE

Dear Ron:

Golder Associates Inc. (GAI) is pleased to present the results of testing conducted in support of Cripple Creek & Victor Gold Mining Company's (CC&V) Valley Leach Facility. This report details the results for gradation and percolation versus consolidation testing performed on samples of Run of Mine (ROM) and crushed minus 7/8 inch Cresson ore.

1.0 MATERIAL DESCRIPTION

Samples of Cresson ore were provided by CC&V and used in the percolation-consolidation testing program. The general ore sample gradations and description are summarized on Table 1. Detailed gradations are presented in Attachments A and B. Both samples classify as a fine to coarse gravel with some fine to coarse sand with little fines.

2.0 CONSOLIDATION AND PERCOLATION TESTING

Consolidation and percolation tests were conducted on the Cresson ore samples. Each sample was prepared and incrementally loaded to a maximum stress of 432 pounds per square inch (psi) consolidation pressure [equivalent to a heap height of 565 feet based on a bulk ore density of 110 pounds per cubic foot] and measured for compression, settlement and maximum percolation rate at select load increments. The maximum test pressure of 432 psi is the maximum capacity of the testing apparatus.

2.1 Test Apparatus

The testing apparatus consisted of a 12-inch nominal inside diameter (ID) aluminum tube (testing cell), approximately 18 inches in height. Figure 1 shows the assembled testing cell. The cell was clamped to the base plate and the tie-down rods anchored to the cell base plate. A porous loading plate was placed in contact with the material and a hydraulic jack was used to apply the force to the sample against the top plate. A digital pressure transducer was used to

monitor the applied load and a dial gauge measured deformation. The load from the hydraulic jack is adjusted to maintain the desired loading stress throughout the test.

2.2 Test Configuration

ROM Cresson Ore

For the ROM Cresson Ore sample test, the ore material was first screened to remove material larger than 2 inches. The screening was done to keep the ratio of the test vessel diameter to the maximum particle size to around six, thereby minimizing any scaling effects. In addition, a study of ore permeability conducted by Lupo (2000¹) has shown that ore permeability is generally governed by material smaller than 1 to 1 ¹/₂ inches. Figure 2 shows the ROM Cresson ore sample prior to testing. The Cresson ore material was placed into the test cell, the initial sample height was recorded and the loading plate was secured. The sample was loaded in five increments to approximately 27, 54, 108, 216, and 432 psi. The load increments correspond to ore depths of 35, 70, 140, 280, and 565 feet, respectively, assuming a bulk ore density of 110 pounds per cubic foot (pcf). Vertical displacement values were recorded at each load increment. The sample was loaded to the next increment only after consolidation had ceased. The sample was saturated with water and allowed to drain prior to the first load being applied.

The percolation rate of the material was measured by applying tap water with an electromagnetic pump to simulate various solution application rates. The initial application rate was 0.0045 gallons per minute per square foot (gpm/sf). At each load increment, the application rate was increased to a maximum rate of 0.045 gpm/sf or until ponding was observed on sample. The application rate of 0.045 gpm/sf is ten times greater than the initial application rate and is the maximum flow rating for the testing frame.

The sample was allowed to equilibrate (i.e. inflow equals outflow) before increasing the application rate. During the entire testing period, the surface of the sample was observed for ponding, which would indicate failure of the sample to percolate water at the given application rate.

Crushed Minus 7/8 Cresson Ore

The crushed minus 7/8 inch Cresson Ore sample was not screened prior to testing. Figure 3 presents condition of the crushed ore prior to testing. The crushed ore was placed into the test cell, the initial sample height was recorded and the loading plate was secured. The sample was loaded in five increments to approximately 27, 54, 108, 216, and 432 psi. The load increments correspond to ore depths of 35, 70, 140, 280, and 565 feet, respectively, assuming a bulk ore density of 110 pounds per cubic foot (pcf). Vertical displacement values were recorded at each load increment. The sample was loaded to the next increment only after

¹ Lupo, John, 2000. Hydraulic Considerations for Leaching Operations, to be presented at the Society of Mining Engineering (AIME) conference, February 28 - March 1, Salt Lake City, Utah.

consolidation had ceased. The sample was saturated with water and allowed to drain prior to the first load being applied.

The crushed ore was then tested for percolation rate, following the same methodology as that used for the ROM ore sample.

2.3 Testing Results

The maximum percolation rates for the ROM and minus 7/8 inch Cresson Ore samples all measured 0.045 gpm/sf under the incremental loads. This percolation rate is ten times the solution application rate used at CC&V. At all tested load increments, no ponding of water was observed. The percolation test data clearly show the ore is capable of supporting high percolation rates, even under an equivalent heap height of 565 feet.

In addition, the test results show the ROM Cresson Ore will strain approximately 10 percent under the load of 432 psi, while the crushed ore will strain approximately 16 percent under the same loading.

After the percolation-consolidation tests were completed, the ore samples were tested for gradation to evaluate mechanical degradation under load. The post-test gradation data and the consolidation data are presented in Attachments A and B. The ROM Cresson Ore sample did not show any appreciable change in gradation due to the consolidation under load. The minus 7/8 inch ore did show a small increase (about 3 percent) in fines resulting from the consolidation under load.

3.0 CLOSURE

If there are any questions or concerns regarding this report or the test data, please call us at (303) 980-0540.

Sincerely,

GOLDER ASSOCIATES INC.

Laboratory Manager

DMD/JFL/Ijd

ohn F. Lupo, Ph.D., P.E. Sr. Project Manager

Attachments: Tables Figures Attachment A - ROM Cresson Ore Attachment B - Crushed Minus 7/8 inch Cresson Ore

TABLES

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Ç,	ADDITIONAL TESTS COMMENTS (See Notes)				EAR TEST ITY SS
	SPECIFIC GRAVITY		1		DIRECT SHEAR TEST PERM = PERMEABILITY IP = IN PROGRESS
	DRAIN	: :	5		PERM = IP =
		6 +	2		
	GRAIN SIZE DISTRIBUTION % FINER % FINER % FINER 34* #4 #200 93 38 6	48	16		T = TRIAXIAL TEST U = UNCONFINED COMPRESSION TEST C = CONSOLIDATION TEST
0	GRAIN SI 4% FINER 3/4" 93	96 43	48		TRIAXIAL TEST UNCONFINED COMPRESS CONSOLIDATION TEST
ORT /	: PI S	: :	1		TEST NED C DATIO
	ATTERBERG (IMITS LL PL PI	1 1	1		T = TRIAXIAL TEST u = UNCONFINED C C = CONSOLIDATIC
TABLE RY OF S	10 The 2004 C				U = TR C = CO C = CO
CC & V / TECHN 99 TABLE 1 SUMMARY OF SOIL DATA	DELIVERED MOISTURE (%)	: :	B I I I I I I I I I I I I I I I I I I I		F ⊃ 0
N N N N N N N N N N N N N N N N N N N	USCS SOIL DELIVERED CLASSI- MOISTURE FICATION (%) GW	BW GW	G		MIT LIMIT NDEX GE LIMIT
	SAMPLE DEPTH (1)	1	1		LL = LIQUID LIMIT PL = PLASTIC LIMIT PI = PLASTIC INDEX SL = SHRINKAGE LIMIT SL = SHRINKAGE LIMIT
	SAMPLE NUMBER -7/8 INCH CRESSON ORE	-7/8 INCH CRESSON ORE -2 INCH CRESSON ORE	-2 INCH CRESSON ORE		ה = 2 - ביי
$\tilde{\mathbf{O}}$	BORING NUMBER BEFORE PERC.	AFTER PERC. BEFORE PERC.	AFTER PERC.		NOTES:

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FIGURES

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CC+V/Tech SI. 27/CO 993-2075 -2" Cresson Ore. Consolidation VS Percolation

FIGURE 2: ROM CRESSON ORE



February 2000

CC+V/TECH SUPPORT/CO 993-2075 -1/8 Crushed Cresson Ore Consolidation vs Percolation

FIGURE 3: CRUSHED MINUS 7/8 CRESSON ORE

ATTACHMENT A

ROM CRESSON ORE

February 2000

Compression Leach Testing

Deformation vs. Load

Project: CC&V/TECHNICAL SUPPORT/CO Project Number: 998-2075 Date: FEBRUARY 15-22, 2000 Sample: -2 inch Cresson Ore

Initial Conditions:		
Height of Sample =	11.615	inches
Diameter of Sample =	11.91	inches
Area of Sample =	0.77	sq-ft.
Volume of Sample =	0.75	cuft.
Volume of Sample =	21190.9	cc
Wet Weight of Sample =	32272.8	grams
Moisture Content =	0.0%	
Dry Weight of Sample =	32272.8	grams
Specific Gravity =	2.58	
Wet Density =	1.52	g/cc
Dry Density =	1.52	ā/cc
Wet Density =	95.03	lbs/s[-ft.
Dry Density =	95.03	lbs/sf-ft.

Note: The load shown as 0.1 psi is in reality 0 psi, but for graphing purposes is reported as 0.1 psi.

Applied	Equivalent	Equivalent	Sample	Strain	Unit
Load	Ore Height	Ore Height	Height		Weight
(psi)	(f t)	. (m)	(inches)	: (%)	(pcf)
0.1	0	0	11.615	0.0%	95.0
27.0	41	12	11.572	0.4%	95.4
54.0	82	25	11.413	1.7%	96.7
108.0	164	50	11.218	3.4%	98.4
216.0	327	100	10.880	6.3%	101.5
432.0	655	200	10.463	9.9%	105.5



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Page 1



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PARTICLE-SIZE ANALYSIS OF SOILS ASTM C 117, C 136, D 421, D 422, D 1140, D 2216, D 2217

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CC&V/TECHNICAL SUPPORT/CO 993-2075				SAMPLE #: -2 INCH ORE DEPTH (ft): BEFORE PERC			
MOISTURE CONT	ENT (As	tested)			H (Percent Fines)		
Tare	Į	M8		Tare		-	
Weight Wet Soil & Tare, 4	e l	195.56		Weight Soil &	k Tare Before Wash, g		
Weight Dry Soil & Tare, g	-	187.10		-	k Tare After Wash, g	-	
Weight Tare, g		- 25.40		Weight Tare,	•	-	
Weight Water, g		8.46		Weight Fines	Lost, g	•	
Weight Dry Soil, g	(161.70		Weight Dry S	oil, g	58,988.27	
Moisture, %		5.23%		Fines Lost, %		-	
	SIEVE	Wt. Ret.	% Ret.	% Pass.	SIEVE		
	6.000"	0.00	0.00%	100.00%	6.000"		
Coarse Gravel	3.000"	0.00	0.00%	100.00%	-3.000" Coarse Gravel		
	2.000"	0.00	0.00%	100.00%	2.000"		
	1.500"	12,635.50	21.42%	78.58%	1.500"		
	1.000"	26,096.40	44.24%	55.76%	1.000"		
Fine Gravel	0.750"	33,807.90	57.31%	42.69%	0.750" Fine Gravel		
	0.375"	44.968.60	76.23%	23.77%	0.375"		
Coarse Sand	#4	51,258.20	86.90%	13.10%	#4 Coarse Sand		
Medium Sand	#10	54,271.06	92.00%	8.00%	#10 Medium Sand		
	#20	56,103.27	95.11%	4.89%	#20		
Fine Sand	#40	57,037.29	96.69%	3.31%	#40 Fine Sand		
	#60	57,544.30	97.55%	2.45%	#60		
	#100	57,869.95	98.10%	1.90%	#100		
	#200	58,163.95	98.60%	1.40%	#200		
Fines	PAN	58.988.27	0.00%	100.00%	PAN Fines		
. % C GRVL:	57.3%			Wet Color:	Fine to coarse GRAVE	L	
% F GRVL:	29.6%	86.9%		Description:	with little fine to coars	e	
% C SAND:	5.1%				sand, trace clay (GW)		
% M SAND:	4.7%		LL:	NA			
% F SAND:	1.9%	11.7%	PL:	NA	DATE:	14-Feb-0	
% FINES:	1.4%		PI	NA	TECH:	TM	
⊨	100.0%		Gs:	-	REVIEW:	DMD	

GOLDER ASSOCIATES INC. LAKEWOOD, COLORADO

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LAKEWOOD, COLORADO

PARTICLE-SIZE ANALYSIS OF SOILS ASTM C 117, C 136, D 421, D 422, D 1140, D 2216, D 2217

CC&V/TECHNICA	L SUPPO	ORT/CO	SAM	PLE #: -2 INCH ORE		
993-2075			DEF	PTH (ft): POST PERC		
MOISTURE CONT	ENT (As	tested)		#200 WAS	H (Percent Fines)	
Tare		F27		Tare		•
Weight Wet Soil & Tare,	g	312.11		Weight Soil &	k Tare Before Wash, g	-
Weight Dry Soil & Tare,	g	310.58		Weight Soil &	k Tare After Wash, g	-
Weight Tare, g		33.41		Weight Tare,	g	
Weight Water, g		1.53		Weight Fines	Lost, g	-
Weight Dry Soil, g		277.17		Weight Dry S	ioil, g	31,672.79
Moisture, %		0.55%		Fines Lost, %)	-
	SIEVE	Wt. Ret.	% Ret.	% Pass.	SIEVE	
	6.000"	0.00	0.00%	100.00%	6.000"	
Coarse Gravel	3.000"	0.00	0.00%	100.00%	3.000" Coarse Gravel	
	2.000"	0.00	0.00%	100.00%	2.000"	
	1.500"	6,163.30	19.46%	80.54%	1.500"	
.,	1.000"	12,259.90	38.71%	61 .29%	1.000"	
Fine Gravel	0.750"	16,380.10	51. 72%	48.28%	0.750" Fine Gravel	
	0.375"	22,834.20	72.09%	27.91%	0.375"	
Coarse Sand	#4	26,688.60	84.26%	15.74%	#4 Coarse Sand	
Medium Sand	#10	28,866.68	91.14%	8.86%	#10 Medium Sand	
	#20	29,986.32	94.68%	5.32%	#20	
Fine Sand	#40	30,508.77	96.32%	3.68%	#40 Fine Sand	
	#60	30,780.65	97.18%	2.82%	#60	
	#100	30,963.51	97.76%	2.24%	#100	
	#200	31,141.91	98.32%	1.68%	#200	
Fines	PAN	31.672.79	0.00%	100.00%	PAN Fines	
T						
% C GRVL:	51.7%				Fine to coarse GRAVE	
% F GRVL:	32.5%	84.3%		Description:	with some fine to coars	ie
% C SAND:	6.9%				sand, trace clay (GW)	
% M SAND:	5.2%		LL:	NA	1	
% F SAND:	2.0%	14.1%	PL:	NA	DATE:	24-Feb-0
% FINES:	1.7%		Pl:	NA	TECH:	TM
% TOTAL:	100.0%		Gs:	-	REVIEW:	MK

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ATTACHMENT B

CRUSHED MINUS 7/8 INCH CRESSON ORE

February 2000

Compression Leach Testing

Deformation vs. Load

Project: CC&V/TECHNICAL SUPPORT/CO

Project Number: 998-2075

Date: FEBRUARY 9-14, 2000

Sample: -7/8 inch Cresson Ore

Initial Conditions:		
Height of Sample =	11.420	inches
Diameter of Sample =	11.91	inches
Area of Sample =	0.77	sq-ft.
Volume of Sample =	0.74	cuft. –
Volume of Sample =	20835.1	cc
Wet Weight of Sample =	33018.4	grams
Moisture Content =	0.0%	
Dry Weight of Sample =	33018.4	grams
Specific Gravity =	2.58	
Wet Density =	1.58	g/cc
Dry Density =	1.58	g/cc
Wet Density =	98.8 9	lbs/sf-ft.
Dry Density =	98.89	lbs/sf-ft.

Note: The load shown as 0.1 psi is in reality 0 psi, but for graphing purposes is reported as 0.1 psi.

Applied	Equivalent	Equivalent	Sample	Strain	Unit
Load	Ore Height	Ore Height	Height		Weight
(psi)	(<i>:</i> t)	(m)	(inches)	(%)	(pcf)
0.1	0	0	11.420	0.0%	98.9
27.0	39	12	11.160	2.3%	101.2
54.0	79	24	10.790	5.5%	104.7
108.0	157	48	10.410	8.8%	108.5
216.0	315	96	9.980	12.6%	- 113.2
432.0	629	192	9.530	16.5%	118.5

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PARTICLE-SIZE ANALYSIS OF SOILS ASTM C 117, C 136, D 421, D 422, D 1140, D 2216, D 2217

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CC&V TECH SUPPORT 993-2075 MOISTURE CONTENT (As tested)				SAMPLE #: -7/8 CRUSHED ORE				
				DEPTH (ft): BEFORE PERC				
				#200 WASH (Percent Fines)				
MOISTORE CONT	ENT (AS	(esteu)		#200 WAG	LL (reicent rines)			
Tare	Į	F13		Tare		5-9		
Weight Wet Soil & Tare, g 171.1		171.10		Weight Soil &	632.57			
Weight Dry Soil & Tare, g		166.35		Weight Soil & Tare After Wash, g		539.38		
Weight Tare, g		34.19		Weight Tare, g		158.54		
Weight Water, g	eight Water, g			Weight Fines Lost. g		-		
Weight Dry Soil, g		132.16		Weight Dry Soil, g		3,624.27		
Moisture. %		3.59%		Fines Lost. %				
	SIEVE	Wt. Ret.	% Ret.	% Pass.	SIEVE			
	6.000"	0.00	0.00%	100.00%	6.000"			
Coarse Gravel	3.000"	0.00	0.00%	100.00%	3.000" Coarse Gravel			
	1.500"	0.00	0.00%	100.00%	1.500"			
	1.000"	0.00	0.00%	100.00%	1.000"			
Fine Gravel	0.750*	250.10	6.90%	93.10%	0.750" Fine Gravel			
	0.375"	1,612.40	44.49%	55.51%	0.375"			
Coarse Sand	#4	2.254.60	62.21%	3 7.7 9%	#4 Coarse Sand			
Medium Sand	#10	2,697.60	74.43%	25.57%	#10 Medium Sand			
	#20	2,995.43	82.65%	17.35%	#20			
Fine Sand	#10	3,158.27	87.14%	12.86%	#40 Fine Sand			
	#60	3,252.26	89.74%	10.26%	#60			
	#100	3,321.70	91.65%	8.35%	#10C			
	#200	3,391.14	93.57%	6.43%	#200			
Fines	PAN	3.624.27	0.00%	100.00%	PAN Fines			
% C GRVL:	6.9%				Fine to coarse GRAVE	EL		
% F GRVL:	55.3%	62.2%		Description:	and fine to coarse			
% C SAND:	12.2%				sand with little clay (G	W)		
% M SAND:	12.7%		LL:					
% F SAND:	6.4%	31.4%	PL:		DATE:	10-Feb-0		
% FINES:	6.4%		PI:		TECH:	NG		
% TOTAL:	100.0%		Gs:	-	REVIEW:	DMD		

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500.0 450.0 -100.0 _ _ . 350.0 Unit Weight vs. Overburden Load 300.0 FIGURE 5 Overburden Load, psf 250.0 200.0 I 150.0 100.0 50.0 0.0 0.01 120.0 Unit Weight in pcf 0.011 60.0 80.0 70.0

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PARTICLE-SIZE ANALYSIS OF SOILS ASTM C 117, C 136, D 421, D 422, D 1140, D 2216, D 2217

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CC&V TECH SUPPORT				SAMPLE #: -7/8 CRUSHED ORE				
993-2075				DEPTH (ft): POST PERC				
MOISTINE CONT				#200 WAS	H (Percent Fines)			
MOISTURE CONTI	UNI (AS	lested)		#200 WASI	t (i ci cent i mes)	•		
Tare	· ſ	X5		Tare		5-9		
Weight Wet Soil & Tare, g 258.30		258.30	_	Weight Soil &	632.57 539.58			
Weight Dry Soil & Tare, g 249		249.00		Weight Soil & Tare After Wash. g				
Weight Tare, g 32.		32.93	Weight Tare. g			158.54		
Weight Water, g 9.30		9.30		Weight Fines Lost, g				
Weight Dry Soil, g 216.07		216.07	Weight Dry Soil, g			7,785.07		
Moisture, %		4.30%		Fines Lost. %				
	SIEVE	Wt. Ret.	% Ret.	% Pass.	SIEVE			
	6.000"	0.00	0.00%	100.00%	6.000"			
Coarse Gravel	3.000"	0.00	0.00%	100.00%	3.000" Coarse Grave	1		
	1.500"	0.00	0.00%	100.00%	1.500"			
	1.000"	29.00	0.37%	99.63%	1.000"			
Fine Gravel	0.750"	297.30	3.82%	96.18%	0.750" Fine Gravel			
	0.375"	2,431.40	31.23%	68.77%	0.375"			
Coarse Sand	#4	4,074.00	52.33 %	47.67%	#4 Coarse Sand			
Medium Sand	#10	5,200.18	66.80%	33.20%	#10 Medium Sand	1		
	#20	5,992.34	76.97%	23.03%	#2 0			
Fine Sand	#40	6,446.58	82.81%	17.19%	#40 Fine Sand			
-	#60	6,720.74	86.33%	13.67%	#60			
	#100	6.918.08	88.86%	11.14%	#100			
	#200	7,114.14	91.38%	8.62%	#20 0			
Fines	PAN	7.785.07	0.00%	100.00%	PAN Fines			
% C GRVL:	3.8%				Fine to coarse GRAVEL			
% F GRVL:	48.5%	52.3%		Description:	and fine to coarse			
% C SAND:	14.5%		-		sand with little clay	(GW)		
% M SAND:	16.0%		LL:					
% F SAND:	8.6%	39.1%	PL:		DATI	and the second s		
% FINES:	8.6%		PJ:		TECI			
% TOTAL:	100.0%	1	Gs:	•	REVIEV	V: DMD		

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