# Appendix 5

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Date:

To:

March 22, 2004

Subject:

**GROUND MOTION ATTENUATION STUDIES** EAST CRESSON MINE EXTENSION February 25, 2004 Teller County, Colorado

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#### CRIPPLE CREEK & VICTOR GOLD MINING COMPANY GROUND MOTION ATTENUATION STUDIES EAST CRESSON MINE EXTENSION

#### February 25, 2004

#### **Executive Summary**

Matheson Mining Consultants, Inc. (MMC) monitored six test blasts in three directions from the East Cresson Mine Extension (ECME) near the Cripple Creek and Victor Gold Mining Company (CC&V) property northwest of the unincorporated area of Goldfield, Colorado, with eighteen seismographs. All data, the least squares linear regression analyses, a map, photographs, and instrument information and calibration certificates are attached to this report.

Scaled distance is a relationship used in explosives engineering to interrelate blasts with different maximum charge weights per delay period:

$$SD = D / \sqrt{W}$$

Where: SD = Scaled Distance D = Distance, in feet W = Maximum charge weight per delay period, in pounds

The recommended scaled distance to not exceed the regulatory limit of 0.50 inches per second peak particle velocity (ips ppv) for the ECME in the A-Line direction is 34.1, in the B-Line direction is 32.4, and in the C-Line direction is 31.4. The A-Line regression analysis is the most conservative of the three studies.

The A-Line analysis is comprised of thirty-one data points and has a correlation coefficient of 0.894; the B-Line analysis is comprised of thirty data points and has a correlation coefficient of 0.804; and the C-Line analysis is comprised of thirty-six data points and has a correlation coefficient of 0.788.

Below is a table of distances and charge weights per delay based on the regulatory limit of 0.50 ips ppv and the site-specific scaled distance determinations for the three lines. The charge weight per delay is the maximum explosive charge per 8 millisecond (ms) delay that may be fired at a given distance.

Distance, feet	A-Line, SD=34.1 Charge Weight, pounds per 8ms	B-Line, SD=32.4 Charge Weight, pounds per 8ms	C-Line, SD=31.4 Charge Weight, pounds per 8ms
	delay	delay	delay
500	215	239	253
1000	862	954	1012
1500	1939	2147	2277
2000	3448	3817	4047
2500	5387	5964	6324
	7758	8589	9107
3500	10559	11690	12395
4000	13792	15269	16190
4500	17455	19325	20490
5000	21550	23858	25296

### Distance vs. Charge Weight for A-Line, B-Line, and C-Line

#### INTRODUCTION

Matheson Mining Consultants, Inc. (MMC) was retained by Cripple Creek and Victor Gold Mining Company (CC&V) to perform ground motion attenuation studies in three directions from the southern permit boundary of the East Cresson area resulting from ground vibrations created by test blasting. This area is located northwest of the town of Goldfield, Colorado. Appendix I contains a map showing the test shot and seismograph recording locations. Photographs showing test shot and seismograph locations are attached to the end of this report. Eighteen seismographs (six in each of the three directions studied) were used to record the ground motion from each of six test blasts. The seismographs were positioned at varying distances from each test blast towards the nearest structures in three directions.

Particle velocity data acquired in the field are input into a least squares linear regression analysis program. The United States Office of Surface Mining and Reclamation Enforcement (OSMRE) have approved this program. The regression analysis yields a site-specific vibration attenuation formula in the form:

$$PPV = H(SD)^{-B}$$

where,

H = the velocity (y axis intercept) at a scaled distance of one,
B = the slope of the curve,
PPV = the peak particle velocity in inches per second, and
SD = scaled distance = distance from shot to recorder divided by the square root of the charge weight.

The program also yields the correlation coefficient (goodness of fit),  $r^2$ . The procedure for the analysis performed is outlined in the "Blasting Guidance Manual," March, 1987, published by the OSMRE.

The resulting analysis is used to determine distance and charge weight relationships required for ground motion regulatory compliance. These studies were designed to be conservative in nature. The intent was to maximize the ground motion produced by the test shots. Typically in mine production blasting, explosive energy is consumed by fragmentation and displacement of the rock mass. The confined test blasts minimized fragmentation and displacement while maximizing ground motion.

#### **INSTRUMENTATION**

Vibration records were collected using eighteen Instantel Blastmate III and Minimate Plus seismographs. Four CC&V owned seismographs and twelve MMC owned seismographs were used. The seismographs record particle velocity digitally in the frequency range of 1.5 to 250 Hertz. Each shot is measured in three orthogonal channels of ground motion: vertical, longitudinal, and transverse; and one channel of air-overpressure. Zero-crossings of each of the four-waveform components are calculated to determine frequency response.

Attached, as Appendix II, is an excerpt from the Blastmate III User's Manual describing the specifications and function of the instrumentation and record processing.

An independent party using shake table, piston phone, and electronics traceable to the National Institute of Science and Technology has calibrated the instruments within the past year. Copies of the calibration certificates for the instruments, geophones, and microphones are on file at MMC, or CC&V. In addition, the instrument performs a self-test before monitoring. This is a check of the geophone's overswing and dampening. The microphone is also checked.

It is not possible to alter the vibration recordings or file names in any way, other than the ability to add post event notes. For security reasons, the instrument and software manufacturer (Instantel) will not release any of the programming code to any outside interests for any reason.

#### PROCEDURE

The energy source involved the individual detonation of six, 6-inch diameter test holes. The test holes were drilled in a line on 50-foot centers to 40-foot depths. Each hole was loaded with 100 pounds of ANFO, a cast booster, and was then stemmed with cuttings. The test holes were located at the southern permit boundary of the proposed East Cresson Mine Extension. The test hole location and lines toward non-CC&V structures were chosen in as undisturbed areas as was possible. However, due to extensive mining in the area in the past, much of the surface material has been disturbed and is unconsolidated. The drill holes were reported to be in unconsolidated material. The charge weight was selected to maximize the ground motion created by each detonation, while eliminating energy loss due to creation of fly-rock and permanent ground displacement.

Seismographs were placed at distances of from 107 feet to 703 feet on the A-Line, 93 feet to 815 feet on the B-Line, and from 52 feet to 875 feet on the C-Line (see map in Appendix I). These three lines were set up in directions to the nearest non-CC&V structures from the test shots located at the southern boundary of the East Cresson Mine Extension. Care was taken to ensure good geophone coupling with the ground. Snow and the top frozen soil layer were removed when possible and spikes were used on the geophones. Coordinates for the test shot holes and seismograph recording locations were surveyed by CC&V. Surface distances were then calculated from these coordinates.

Ground motion data was obtained for scaled distances in the range from: 10.7 to 70.3 on the A-Line, 9.3 to 81.5 on the B-Line, and 5.2 to 87.5 on the C-Line.

A least squares linear regression analysis was then performed on each data set to determine the +95% confidence equation as recommended by OSMRE and United States Bureau of Mines (USBM) regulatory guidelines. The statistical validity of the data set is evaluated using the correlation coefficient calculated during the analysis. The equation for the +95% confidence interval is then used to calculate the maximum charge weight per delay period for any given particle velocity and distance.

Recommendations are made based on regulatory criteria and historic vibration monitoring from existing mine production.

#### RESULTS

Appendix III contains the regression analysis, data, and tables for the A-Line study, appendix IV contains the regression analysis, data, and tables for the B-Line study, and Appendix V contains the regression analysis, data, and tables for the C-Line study. Each appendix contains the regression analysis, a page of statistics, a +95% confidence distance vs. charge weight per 8ms delay period table for 0.50 ips, a +95% confidence scaled distance vs. peak particle velocity table, a table summarizing the vibration data, followed by the vibration recordings.

The vibration recordings are ordered by shot and distance. The USBM and OSMRE variable particle velocity vs. frequency criteria is plotted on each vibration event report. The upper line represents the threshold level for possible sheetrock damage, while the lower, dashed line represents the threshold level for possible plaster-on-lath damage.

All tables were generated using the +95% confidence equation. The +95% curve is two standard deviations from the mean (50% curve) and is the curve specified for use by the USBM and OSMRE.

For the A-Line study, in the direction towards the residence located northeast of the test shots, the +95% confidence equation is  $PPV = 313.29 * (SD)^{-1.825}$  and the correlation coefficient  $(r^2)$  is 0.894.

For the B-Line study, in the direction towards Goldfield, southeast of the test shots, the +95% confidence equation is  $PPV = 19.89 * (SD)^{-1.059}$  and the correlation coefficient  $(r^2)$  is 0.804.

For the C-Line study, in the direction towards the cabin located southwest of the test shots, the +95% confidence equation is  $PPV = 21.89 * (SD)^{-1.096}$  and the correlation coefficient  $(r^2)$  is 0.788.

Given a not-to-exceed peak particle velocity and a distance, the maximum charge weight per delay may be calculated using the equations above. The tables found in the appropriate appendices listed above use the equations above to calculate maximum allowable charge weights per delay at given distances and a given not-to-exceed peak particle velocity.

The equations above are in accordance with previous studies that have been performed in the area (see: Ground Motion Attenuation Studies, Ajax and Ridge Road Test Sites, May 28 &29, 1997, and Ground Motion Attenuation Study, North Cresson Area, February 25, 2000). All three data sets have good correlation coefficients. A high degree of reliability may be placed on these results.

#### CONCULSIONS

The East Cresson analyses recommend scaled distances of 34.1 in the A-Line direction, 32.4 in the B-Line direction, and 31.4 in the C-Line direction in order to not exceed 0.50 ips ppv limit on ground motion created by CC&V blasting operations at the nearest non-CC&V controlled structures. A high degree of confidence may be placed in the recommended scaled distances. The site-specific ground motion attenuation equations may be used to calculate a scaled distance for any peak particle velocity.

Attached to Appendix III for A-Line, Appendix IV for B-Line, and Appendix V for C-Line, are tables listing maximum particle velocities at varying distances for given charge weights. Corresponding tables list maximum allowable charge weights per delay at varying distances given a peak particle velocity. A summary sheet and the individual seismograph records measured and used in each study are also found the appendices listed above.

Sincerely,

mark Z. Burgas

Mark L. Burgus, P.G. Geophysicist

Col M. Matu

Colin M. Matheson, Mining Engineer, President



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Photo 1 - Test Hole Loading



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Photo 2 - Seismograph at Recording Location A1



Photo 3 - Typical Seismograph Recording Location

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Photo 4 - A-Line looking NE from test shots.



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Photo 5 - B-Line looking SE from test shots.



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Photo 6 - C-Line looking SW from test shots.

# **APPENDIX I**

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# TEST SHOTS & SEISMOGRAPH RECORDING LOCATIONS MAP



# **APPENDIX II**

# **INSTRUMENT SPECIFICATIONS** & PROCESSING INFORMATION

Appendix

# b) Series III Specifications

Seismic	Range	10	
	Resolution	10 in/s (254 mm/s).	
	Trigger Levels	0.005 in/s (0.127 mm/s), to 0.000625 in/s (0.0159 mm/s) with built-in pream	
	Frequency Analysis	0.005 to 10 in/s (0.127 to 254 mm/s) in steps of 0.001 in/s (0.01 mm)	
and the second	Accuracy	National and Local Standards for all countries (see text).	
이 이 승규에서 있는 것이 같아.	Acceleration. Displacemen	3% at 15 Hz.	
Air Linear	Range		
	Resolution	88–148 dB, 7.25 x 10 <sup>-5</sup> psi to 0.0725 psi. 0.5 Pa to 500 Pa.	
	Trigger Levels	0.1 dB above 120 dB (0.25 Pa).	
	Accuracy	100-148 dB in 1 dB steps.	
"A" Weight (optional)	Range	0.2 dB at 30 Hertz and 127 dB.	
Sampling Rate		50 to 110 dB in steps of 0.1 dB. (Impulse Response – 35 milliseconds)	
Event Storage	Eull Would D	Standard 1024 samples per second per channel to 16.384 (8.192 for 8 channel)	
	Full Waveform Events	500 standard and 1500 optional at standard sample rate of 1024	
Frequency Response	Summary Events	1/50 standard and 8750 optional at standard sample rates of 1024	
Full Waveform Recording	2 to 300 Hz	Ground and Air. Independent of record time.	
i un marcionin Recording	Fixed Record Modes	Manual, single shot, continuous and programmed start/stop.	
	Fixed Record Time	I to 100. 300 or 500 sec plus 0.25 sec pre-trigger.	
Strip Chart Recording	Auto Record Mode	1 to 100, 300 or 500 sec plus 0.25 sec pre-trigger.	
Surp Char Recording	Record Method	Record to memory and/or internal printer. Program interval 2, 5, 15, 60, 300 or 000 and	
Histogram Combo Mode	Days Storage	2.8 or 14 days at 5 second interval. 34 or 170 days at 60 second interval	
Combo Mode	Histogram Record Method	Record to memory and/or internal printer. Program interval 2, 5, 15, 60, 300 or 900 cra	
	Histogram Days Storage	2.4 of 12 days at 5 second interval. 29 or 147 days at 60 second interval	
	Waveform Events	Up to 13 one-second events (1024 sample rate, four channels recording).	
Special Functions	Waveform Record Times	1 to 13 seconds plus 0.25 sec pre-trigger.	
	Timer Operation	Programmed start/stop.	
	Self Check	Programmable daily check.	
	Scaled Distance	Weight and distance stored with event.	
	Monitor Log	History printout programmable up to all events stored	
	Automatic download	Automatic downloading of data from a unattended monitor with Auto Call Home.	
	Measurement Units	Imperial or metric, dB or linear air pressure, or in units of custom sensors.	
rinter	Resolution	576 dots/line and 0.0049 inches (0.125 mm) per dot.	
	Print Time	Less than 10 seconds for typical 1 second event with full analysis.	
	Paper Control	Paper tear slot or automatic paper takeup, separate keys for feed and takeup.	
	Rated Life - print head	18 miles (30 km) of printing.	
	Number of Copies	1 to 10 copies automatic, any number manual.	
ser interface	Keyboard	64 domed tactile with separate keys for common functions.	
	Display	4 line by 20 character high contrast backlit display with on line help.	
attery Life		30 days continuous recording. 70 days with timer, printing will decrease life.	
use		5 A/250 V	

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Appendix

		intitueu)
Dimensions		10.6 " x 14.0 " x 6.5 " (269 mm x 355 mm x 165 mm).
Weight		14 lbs. (6.4 kg).
Warranty	2 Years Parts and Labor	Calibration and equipment check required at 1 year to maintain warranty.
Environmental	Printer/ LCD	14 to 122 degrees F (-10 to 50 degrees C) operating.
	Electronics	-4 to 140 degrees F (-20 to 60 degrees C) operating.
물 이 양감을 벗	Humidity	5 – 90% RH non – condensing
stantel resonues the sight to all	Storage	-4 to 160 degrees F (-20 to 70 degrees C).

# Series III Specifications (continued)

Instantel reserves the right to change specifications without notice.

# c) Compliance Reports

The BlastMate III supports numerous Compliance Reports, also called National Frequency Analysis Standards, including U.S.A. USBM/OSMRE, British Standard BS 6472, French GFEE, German DIN 4150, New Zealand 4403:1976, and Spain UNE 22.381. Two frequency standards, U.S.A. USBM/OSMRE and German DIN 4150, appear below. Use the BlastWare III software to choose the Compliance Report used by your monitor.





Note: Data points appearing outside of the report boundaries indicates the recorded data was outside the range of the report. In the DIN 4150 example, some peaks occurred at frequencies greater than 100 Hz and were therefore drawn outside the boundaries of the report.

Using the optional BlastWare III Advanced Module, you can edit Compliance Reports or create an entirely new report to meet your specific needs.

# 3. COMPLIANCE MODULE

This chapter provides instructions to install and setup the BlastMate III.

# 3.1. What is Event Monitoring?

Event monitoring measures both ground vibrations and air pressure. The monitor measures transverse, vertical, and longitudinal ground vibrations. Transverse ground vibrations agitate particles in a side to side motion. Vertical ground vibrations agitate particles in an up and down motion. Longitudinal ground vibrations agitate particles in a forward and back motion progressing outward from the event site. Events also affect air pressure by creating what is commonly referred to as "air blast". By measuring air pressures, we can determine the effect of air blast energy on structures, measured on the Linear "L" scale, or as perceived by the human ear, measured on the "A" Weight scale.





BlastMate III Operator Manual

#### a. Geophone Operation

Functionally a geophone sensor is a coil of wire suspended around a magnet. The magnet is free to move in a field of magnetic flux lines. By Lenzs' Law, induced voltage is proportional to the speed at which flux lines are traversed. Induced coil voltage is therefore proportional to the relative velocity of the coil to the magnet. In practice, it does not matter whether the coil or the magnet moves. Only the motion and speed relative to each other are important.



Figure 5.5 Geophone Sensor Operation.

Geophone sensor specifications give a number known as the Intrinsic Voltage Sensitivity. It is the coil voltage induced for a given coil versus magnet speed with units of V/in/s. In seismic applications, the magnet is moved by the blast energy because it is coupled to the particles of the surrounding terrain. The coil, because of its inertia, does not move and the resulting magnet versus coil motion induces a voltage which is proportional to particle velocity.

### b. Instantel Standard Transducer

Instantel offers a 2 to 300 Hz standard transducer in a round package. The transducer may be installed on a floor, wall, or ceiling using a variety of installation procedures including ground spikes, burying, mounting rod, or optional leveling plate with leveling feet and integrated bubble level. The figure below includes an Instantel Standard Transducer (a) and a Standard Transducer with leveling plate (b).

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Figure 5.6 Instantel Standard Transducer (a) and Standard Transducer with Optional Leveling Plate (b).

# c. Transducer Calibration Requirements

The geophone sensors inside Instantel's transducers must be calibrated annually by Instantel or an authorized Instantel service facility. Contact your dealer for further information.

# 5.2.2. Microphone

The microphone measures air pressure. Instantel offers two types, Linear "L" (standard) and "A" Weight (optional). Both come with a three foot (one meter) microphone mounting stand.

#### a. Measurement Scales

The BlastMate III supports two sound pressure measurement scales: Linear "L" and "A" Weight.

#### (1) Linear "L"

Linear measurement is generally used to measure the effect of low frequency air pressure on buildings. The linear scale records sound pressure without modification in the 2 to 300 Hz range. Measurement units may be in absolute, Pascal, or relative dB scales.

#### (2) Weight

"A" Weight measures noise levels people may consider an annoyance. The signal is then converted to root mean square (RMS). Units are measured using the decibel scale, dB(A).

## b. Microphone Calibration Requirements

Instantel's microphone must be calibrated annually by Instantel or an authorized Instantel service facility. Contact your dealer for further information.

### 5.3. Sensorcheck

Sensorcheck performs a two stage test on the BlastMate III and its sensors. In the first stage, the program displays the BlastMate III serial number, software version, the total amount of memory installed in the BlastMate III, the total amount of memory available to store events, and the number of events presently stored in memory. The second stage tests each geophone within Instantel's transducer and the microphone operation. The program also tests the operation of the BlastMate III itself and the sensor connecting cables. Pass or fail results appear on the display. See the Basic Reference chapter of this manual to choose when Sensorcheck operates automatically.

# 5.3.1. Checking the Transducer's Geophones

Sensorcheck measures a geophone's natural frequency and damping indicated by an Overswing Ratio (OR). Sensorcheck sends an electric pulse to the geophones and measures the response. If the geophone's response falls within a specified calibration range, the geophone is in calibration and monitoring operations can continue. If the geophone's response does not fall within a specified calibration range, the geophone is not calibrated. You cannot record events until you fix or replace the geophones. See the troubleshooting section of this manual for the appropriate procedures to follow.

#### a. Natural Frequency

Waveform measurements check the natural period (t) of a geophone's sensor coil assembly. Referring to the figure below, the distance from  $P_1$  to  $P_2$  represents 0.125 seconds. Since Frequency is the reciprocal of the period, F=1/t, the frequency is approximately 8 Hz. A calibrated sensor has a natural frequency between 6.5 and 9.5 Hertz. Calculations for all geophones appear with each recorded event.



Figure 5.7 Calculating a Geophone's Natural Frequency.

### b. Damping – Overswing Ratio (OR)

The overswing ratio (OR) measures damping and is calculated by computing the ratio of the magnitude of adjacent waveform peaks according to the following formula:

$$OR = \frac{A_1}{A_2}$$

Acceptable overswing ratios range from 2.8 to 4.8. The figure below displays a graph of a geophone coil's "free fall" response.  $A_1$  and  $A_2$  are used for overswing calculations.



#### Chapter 5

## 5.3.2. Checking the Microphone

Sensorcheck tests the microphone's operation by sending a signal to the microphone and measuring its frequency and amplitude response. If the results of the test fall within specified ranges, the microphone is within calibration.

### 5.3.3. Sensorcheck Report

The Sensorcheck report appears on the BlastMate III display. The message "All Channels Working, Press Print to Print" indicates the BlastMate III sensors have passed the Sensorcheck.

### 5.4. Anti-alias Filters

Aliasing occurs when a high-frequency signal appears as an erroneous low frequency because the waveform was sampled at too low a sampling rate. An anti-aliasing filter solves this problem by removing the high-frequencies.

# 5.5. Data Analysis Techniques

The following sections define the BlastMate III data analysis techniques. The first section, ground vibrations, discusses calculations applied to event data recorded by a transducer. The second section, sound pressure, describes the microphone event data calculations.

### 5.5.1. Ground Vibrations

The BlastMate III calculates the Peak Particle Velocity, Zero Crossing Frequency, Peak Acceleration, and Peak Displacement for each of the transverse, vertical, and longitudinal axes. The BlastMate III calculates Peak Vector Sum using data from all three axes.

### a. Peak Particle Velocity (PPV)

Peak Particle Velocity indicates the maximum speed particles travel resulting from an event's ground vibrations. The BlastMate III calculates the PPV for each geophone.



Figure 5.9 Calculating Peak Particle Velocity.

### b. Zero Crossing Frequency (ZC Freq)

The Zero Crossing Frequency calculates the event waveform's frequency at the largest peak.

#### (1) Calculating Zero Crossing Frequency

To calculate the Zero Crossing Frequency, we need to determine the period of oscillation of the waveform. Convenient waveform positions for measuring period, the time for one complete cycle, occur between two successive peaks, troughs, or zero crossings. The BlastMate III measures between zero crossings. Frequency is the number of periods that occur in one second calculated by the formula: Frequency = 1/period.



Figure 5.10 Calculating the Zero Crossing Frequency.

### (2) Zero Crossing Frequency Limitation

The Zero Crossing Frequency calculation is limited because it assumes a single predominant frequency at the peak, typically represented by sinusoidal waveforms. In practice, the peak may be the result of two or more major frequency components representing compound waveforms as illustrated in the figure below. It is therefore only an approximation of the frequency of the Peak Particle Velocity.

Waveforms may have the same Peak Particle Velocities but different Zero Crossing Frequencies depending on the shape of the waveforms involved. With reference to the figures above and below; both waveforms have the same Peak Particle Velocities however their Zero Crossing Frequencies differ. In the figure above, the zero crossing frequency uses the 1/2 period indicated by T<sub>1</sub>. In the figure below, the zero crossing frequency uses the 1/2 period indicated by T<sub>2</sub>. Notice that T<sub>1</sub> is less than T<sub>2</sub> because of the different waveform shapes, therefore the Zero Crossing Frequency in figure above is greater than the Zero Crossing Frequency in the figure below. It is for this reason, the Zero Crossing Frequency may differ for peaks having the same Peak Particle Velocity.



Limitation.

#### (3) Sample Rate Error

The Zero Crossing Frequency requires the period of a wavelength before it can calculate the wavelength's frequency using the formula 1/period. A sampling error occurs for higher frequencies when wavelength periods become relatively small and the sampling rate begins to miss zero crossing points. In other words, the wavelength periods occur much faster than a BlastMate III can sample and use in the calculation.

At higher frequencies there are fewer sample points per cycle and therefore greater error. The following table illustrates how error increases with frequency.

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Frequency Range	Recording Rate				
	Standard	Fast	Faster		
	(1024 Hz)	(2048 Hz)	(4096 Hz)		
0 – 30 Hz	negligible	negligible	negligible		
	error	error	error		
31 – 50 Hz	up to 5 Hz	up to 2.5 Hz	negligible		
	error	error	error		
51 – 70 Hz	up to 8 Hz	up to 4 Hz	up to 2 Hz		
	error	error	error		
71 – 90 Hz	up to 18 Hz	up to 9 Hz	up to 4.5 Hz		
	error	error	error		
91 – 150 Hz	up to 50 Hz error	up to 25 Hz error	up to 12.5 Hz		

The BlastMate III does not calculate frequencies above 100 Hz because of the high error level at 1024 samples per second. The message ">100 Hz" displays. At 2048 samples per second, the message ">200 Hz" displays. When recording at 4096 samples per second, the message ">400 Hz" displays. Furthermore if a waveform is very complex, or if it contains a large offset value, the zero crossings may lie outside an acceptable window. Whenever a frequency cannot be calculated the message "<1 Hz" displays. The message N/A indicates an entire waveform was not captured and therefore no frequency could be calculated. More accurate analysis is available using the BlastWare III software.

#### c. Peak Acceleration

The BlastMate III calculates peak acceleration, the rate of change of velocity, by dividing the difference in velocity by the difference in time. To obtain the peak acceleration, the BlastMate III subtracts two velocity readings and divides the result by the elapsed time between them.

$$a = \frac{dV}{dT} \approx \frac{\Delta V}{\Delta T}$$
 where:

 $\triangle t = a \text{ small interval}$ 

The BlastMate III calculates the peak acceleration at each point along the entire waveform and reports the peak value. Note that this is not necessarily at the peak velocity for an individual waveform.

#### d. Peak Displacement

The BlastMate III calculates peak displacement. or particle distance traveled, by multiplying speed by time. In the BlastMate III the interval velocity is multiplied by the time interval and the resulting displacement segments are summed.

$$s = \int V dt \approx \sum (V \Delta t)$$

where:

V = the velocity in each interval

To obtain the peak displacement, the BlastMate III integrates each wave segment of the entire waveform between zero crossings, selects the largest, then divides the value by half. Note that this is not necessarily at the peak velocity of the waveform.

### e. Peak Vector Sum (PVS)

The figure below displays three event waveforms. The figure illustrates the procedure of graphically calculating peak vector sums. Measured magnitudes are tabulated for six different times and represent velocities in each of the three axes. The vector sum represents the resultant particle velocity magnitude and is calculated by squaring and adding the magnitudes and taking the square root.

$$PVS = \sqrt{T^2 + V^2 + L^2}$$

where:

T = particle velocity along the transverse plane

V = particle velocity along the vertical plane

L = particle velocity along the longitudinal plane

The BlastMate III calculates the peak vector sum for each point of the sampled waveforms and displays the largest value. Note that this is not necessarily at the peak velocity for an individual waveform.

EVENT WAVEFORMS			MAGNITUDE		PEAK	
TRANSVERSE	VERTICAL	LONGITUDINAL	ТТ	v	L	VECTOR
			-0.34	-0.33	0.14	0.494
			0.38	-0.47	0.38	0.714
			0.29	-0.31	0.51	0.663
			-0.53	0.23	-0.31	0.655
			0.24	0.07	0.36	0.440
		<u>P</u>	-0.23	-0.16	-0.15	0.318
A	}	{				
~						
}	{					

Figure 5.12 Calculating the Peak Vector Sum.

### 5.5.2. Sound Pressure

The BlastMate III calculates two sound pressure indicators, peak sound pressure and zero crossing frequency.

### a. Peak Sound Pressure (PSP)

The BlastMate III checks the entire event waveform and displays the largest sound pressure called the Peak Sound Pressure (PSP), also referred to as the Peak Air Over-Pressure. Results appear on the BlastMate III display and in the Event Summary Report.

# b. Zero Crossing Frequency (ZC Freq)

The Zero Crossing Frequency calculation for sound pressure is the same calculation used for ground vibrations. Please see above for a complete discussion.

Note: The Zero Crossing Frequency calculation is performed for Linear microphones only. This calculation does not appear on the BlastMate III display or on Event Summary Reports when using an "A" Weight microphone.

# 5.6. Alternate Manual Waveform Calculations

The following sections discuss manual waveform analysis techniques. These have been included for reference purposes only. They do not represent the calculation techniques employed by the BlastMate III.

Graphical methods for calculating area and slope depend on the shape of the waveform being analyzed. A complete discussion of the procedures is beyond the scope of this manual. Two useful reference texts are G. A. BOLLIGER, *BLAST VIBRATION ANALYSIS*, Southern Illinois University Press and CHARLES H. DOWDING, *BLAST VIBRATION MONITORING AND CONTROL*, Prentice-Hall Inc.

In each of the subsequent examples some formulae appear with no attempt at derivation. The following definitions apply:

- A = amplitude in inches/second measured from the zero line
- $A_m$  = amplitude measured in millimeters/second
- T = period in seconds
- Y = absolute change in amplitude over time measured in inches/second
- $Y_m$  = absolute change in amplitude over time measured in millimeters/second

## 5.6.1. Sinusoidal Waveforms

The motion is essentially sinusoidal with gradual amplitude and frequency changes.

 $\frac{T}{2\pi} \times A_{m}$ 



Figure 5.13 Manual Waveform Calculations on Sinusoidal Waveforms.

### a. Calculating Displacement:

Maximum Displacement (in.) =  $\frac{T}{2\pi} \times A$ 

\_\_\_\_

Maximum Displacement (mm) =

b.

Maximum Acceleration (in./s<sup>2</sup>) = 
$$\frac{2\pi}{T} \times A$$

Reference

Maximum Acceleration (mm/s<sup>2</sup>) = 
$$\frac{2\pi}{T} \times A_{m}$$

# 5.6.2. Nearly Triangular Waveforms

Motion is irregular and has large amplitude.



Figure 5.14 Manual Waveform Calculations on Nearly Triangular Waveforms.

### a. Calculating Displacement:

Maximum Displacement (in.) =  $\frac{T}{8} \times A$ 

Maximum Displacement (mm) =  $\frac{T}{8} \times A_{in}$ 

## b. Calculating Acceleration:

Maximum Acceleration (in./s<sup>2</sup>) =  $\frac{1}{T} \times Y$ 

Maximum Acceleration (mm/s<sup>2</sup>) =  $\frac{1}{T} \times Y_{m}$ 

# 5.6.3. Compound Waveforms

If the record exhibits interference by two or more predominant frequencies then the maximum displacement will be the sum of the maximum of each individual frequency component.



Figure 5.15 Manual Waveform Calculations on Compound Waveforms.

# a. Calculating Displacement:

Maximum Displacement (in.) =  $\frac{T_1}{2\pi} \times A_1 + \frac{T_2}{2\pi} \times A_2$ Maximum Displacement (mm) =  $\frac{T_1}{2\pi} \times A_{1m} + \frac{T_2}{2\pi} \times A_{2m}$ 

## b. Calculating Acceleration:

Maximum Acceleration (in./s<sup>2</sup>) =  $\frac{2\pi}{T_1} \times A_1 + \frac{2\pi}{T_2} \times A_2$ Maximum Acceleration (mm/s<sup>2</sup>) =  $\frac{2\pi}{T_1} \times A_{1m} + \frac{2\pi}{T_2} \times A_{2m}$ 

# 5.6.4. Irregular Waveforms



Figure 5.16 Manual Waveform Calculations on Irregular Waveforms.

### a. Calculating Displacement:

Maximum Displacement = area under curve measured by a planimeter.

# **APPENDIX III**

A-LINE GROUND MOTION ATTENUATION STUDY, SCALED DISTANCE, CHARGE WEIGHT, & PPV TABLES, VIBRATION RECORDINGS



# **A-Line Regression Analysis**

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Data Points	Max SD	Min SD	Max PV	Min PV
31	80.12	10.67	2.09	0.03
Sum of SD 112.3	Sum of PV -52.9	Sum of SD <sup>2</sup> 417.9	Sum of PV <sup>2</sup> 132.1	Sum of SD x P\ -212.1
Sum SD x Sum PV -5937.5		Sum of (SD) <sup>2</sup> 12607.5		Sum of (PV) <sup>2</sup> 2796.3
SSX 11.246	<b>SSY</b> 41.930	SSXY -20.529	Xbar 3.622	<b>Ybar</b> -1.706
S 0,392	Se 4.46		R -0.945	R <sup>2</sup> 0.894
Slope -1.825			Intercept 4.906	n - Carlor A
Regre	ssion Line Equ	ation 50%		
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	V= 4.91	X (SD)	-1.825	

# **Cripple Creek Regression Analysis Statistics**

95% Confidence Equation PV= 313.29 X (SD) -1.825

K Values		Z
135.08	K <sub>50</sub>	
273.67	K <sub>90</sub>	1.645
313.29	K <sub>95</sub>	1.96
366.58	K <sub>98</sub>	2.326
408.11	K <sub>99</sub>	2.576
554.69	K <sub>99.9</sub>	3.291
717.61	K <sub>99.99</sub>	3.891

Z values from Basic Statistical Methods for Engineers and Scientists Neville and Kennedy 1964, Table 10-1 p. 111

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### **Explanation of Regression Analysis**

#### **Data Statistics**

Data Points is the number of data points used in the analysis.

Max PPV is the maximum peak particle velocity measured in inches per second used in the analysis. Min PPV is the minimum peak particle velocity, measured in inches per second used in the data analysis.

Max SD is the maximum scaled distance (SD=  $D/(W^{1/2})$ ) used in the analysis.

Min SD is the minimum scaled distance used in the analysis.

#### **Calculated Sums**

Sum of SD is the sum of the natural log (ln) of the Scaled Distance values Sum of PPV is the sum of the ln of the Peak Particle Velocity values Sum of SD<sup>2</sup> is the sum of the squares of the ln of the Scaled Distance values. Sum of PPV<sup>2</sup> is the sum of the squares of the ln of the Peak Particle Velocity values. Sum of SD x PPV is the sum of the ln of the SD values times the log of the PPV values.

#### Sums of Squares

SSX is the sum of the ln of the SD values squared minus the (Sum of SD)<sup>2</sup> divided by the Number of Data Points or: SSX = Sum of SD<sup>2</sup> – (Sum of SD<sup>2</sup>/Number of Data Points) SSY is the sum of the ln of the PPV values squared minus the (Sum of PPV)<sup>2</sup> divided by the Number of Data Points or: SSY = Sum of PPV<sup>2</sup> – (Sum of PPV<sup>2</sup>/Number of Data Points) SSXY = Sum of SD x PPV– ((Sum of SD\*Sum of PPV)/Number of Data Points) Sum of SD x Sum of PPV is the product of the sum of the ln of the SD's and the ln of the PPV's. (Sum of SD)<sup>2</sup> is the square of the sum of the ln of the SD's.

### Calculated Means & Calculated Coefficients

Xbar is the sum of the ln of the SD's divided by the Number of Data Points.

Ybar is the sum of the ln of the PPV's divided by the Number of Data Points.

Intercept is the value of Particle Velocity at Scaled Distance=1

K50 is the value of the Particle Velocity (Y) intercept of the mean line or  $e^a$ .

K95 is the value of the Particle Velocity (Y) intercept of the second standard deviation line.

K99 is the value of the Particle Velocity (Y) intercept of the third standard deviation line.

Slope is the value of the slope of the mean line and the value of the slope of confidence lines

### Sample Standard Deviation & Coefficient of Correlation

S is the standard deviation.

Se<sub>2</sub> is the variance.

R is the correlation coefficient

 $R^2$  is the multiple correlation coefficient or the "goodness of fit".

The 95% Confidence Level Equation – the equation of the second standard deviation from the mean line or  $Y = K95*X^{(B)}$ 

Where: Y is the PPV

X is the Scaled Distance

### Charge Weight per Delay Calculated From Given Distances for Particle Velocity 0.5 ips

Distance	Charge Weight	Distance	Charge Weight
(feet)	(pounds)	(feet)	(pounds)
100	9	3600	11171
200	34	3700	11801
300	78	3800	12447
400	138	3900	13111
500	215	4000	13792
600	310	4100	14490
700	422	4200	15206
800	552	4300	15938
900	698	4400	16688
1000	862	4500	17455
1100	1043	4600	18240
1200	1241	4700	19041
1300	1457	4800	19860
1400	1690	4900	20696
1500	1939	5000	21550
1600	2207	5100	22420
1700	2491	5200	23308
1800	2793	5300	24213
1900	3112	5400	25136
2000	3448	5500	26075
2100	3801	5600	27032
2200	4172	5700	28006
2300	4560	5800	28997
2400	4965	5900	30006
2500	5387	6000	31032
2600	5827	6100	32075
2700	6284	6200	33135
2800	6758	6300	34212
2900	7249	6400	35307
3000	7758	6500	36419
3100	8284	6600	37548
3200	8827	6700	38695
3300	9387	6800	39858
3400	9965	6900	41039
3500	10559	7000	42238

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# **REGRESSION ANALYSIS**

95% CONFIDENCE LEVEL SCALED DISTANCE TABLE

Scaled Distance	caled Distance Particle Velocity		Particle Velocity
1	313.29	125	0.05
5	16.60	130	0.04
10	4.68	135	0.04
15	2.23	140	0.04
20	1.32	145	0.04
25	0.88	150	0.03
30	0.63	155	0.03
35	0.48	160	0.03
40	0.37	165	0.03
45	0.30	170	0.03
50	0.25	175	0.03
55	0.21	180	0.02
60	0.18	185	0.02
65	0.15	190	0.02
70	0.13	195	0.02
75	0.12	200	0.02
80	0.11	205	0.02
85	0.09	210	0.02
90	0.08	215	0.02
95	0.08	220	0.02
100	0.07	225	0.02
105	0.06	230	0.02
110	0.06	235	0.02
115	0.05	240	0.01
120	0.05	245	0.01

Shot	Recording	Charge Weight	Instrument	Distance	Scaled Distance	Peak Particle Velocit
Number	Station	(pounds)	Number	(feet)	(ft/lb <sup>2</sup> )	(inches per second)
1	A-1	100	BA7882	106,712	10.7	2.09
1	A-2	100	BA7802	215.993	21.6	0.5
1	<u>A-3</u>	100	BA7884	378.924	37.9	0.11
1	A-5	100	BA5546	644.931	64.5	0.050
2	A-1	100	BA7882	108.799	10.9	1.650
2	A-2	100	BA7802	216.702	21.7	0.495
2	A-3	100	BA7884	375.967	37.6	0.140
2	A-5	100	BA5546	641.931	64.2	0.050
3	A-1	100	BA7882	130.574	13.1	1.720
3	A-2	100	BA7802	226.987	22.7	0.475
3	A-3	100	BA7884	377.571	37.8	0.180
3	A-5	100	BA5546	640.619	64.1	0.055
3	A-5	100	BE8979	640.619	64.1	0.040
3	A-6	100	BA7803	801.191	80.1	0.030
4	A-1	100	BA7882	162.244	16.2	0.795
4	A-2	100	BA7802	245.092	24.5	0.410
	A-3	100	BA7884	384.513	38.5	0.235
4	A-5	100	BA5546	642.433	64.2	0.075
4	A-5	100	BE8979	642.433	64.2	0.045
4	A-6	100	BA7803	801.066	80.1	0.030
5	A-1	100	BA7882	205.653	20.6	0.485
5	A-2	100	BA7802	275.232	27.5	0.335
5	A-3	100	BA7884	400.841	40.1	0.220
5	A-5	100	BA5546	650.774	65.1	0.095
5	A-5	100	BE8979	650.774	65.1	0.060
5	A-7	100	BA7803	694,988	69.5	0.190
6	A-1	100	BA7882	246.244	24.6	0.24
6	A-2	100	BA7802	305.554	30.6	
6	A-3	100	BA7884	418.384	41.8	0.235
6	A-5	100	BA5546	659.481	65.9	0.135
6	A-7	100	BA7803	702.682	70.3	0.110
				102.002	10.3	0.135

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