

Design Report Swede Lake Dam Rehabilitation Boulder County, Colorado

Water Division 1, Water District 5, C-2064
DAMID:050304

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Project No. 110480

April 24, 2018



EXECUTIVE SUMMARY

Construction for the Swede Lake Dam Rehabilitation project began in August 2017. The scope of work included: 1) Mitigate seepage through embankment. 2) Repair primary outlet structure. 3) Repair irrigation outlet structure. 4) Repair and replace embankment erosion. 5) Remove sediment from Swede Lake. 6) Repair emergency spillway. 7) Repair spillway ditch. 8) Add erosion control where damaged or missing. 9) Revegetate disturbed areas.

Construction experienced delays from a necessary change in scope of work. After excavation and further examination of the existing embankment, EA observed that the conditions of the existing embankment were unacceptable due to volume of roots and, in some locations, poor soil condition. It was determined that the embankment should be completely removed and replaced, rather than repaired. Apart from this change, only minor field adjustments were needed. Work was substantially completed in March 2018.

Based on our observation and testing throughout the project, the work was conducted in accordance with the approved plans and specifications. Changes to the original plans and issues addressed during construction are described in this report and are shown on the “As-Constructed” drawings.

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1.0 INTRODUCTION

Swede Lake is located in Section 14, Township 2 North, Range 70 West of the 6th Principal Meridian, in Boulder County, Colorado. The project site is located approximately one mile west of the intersection of Pike Road and North 75th Street in rural Boulder County, Colorado. Swede Lake is the largest of three small reservoirs north of Pike Road and northwest of Lagerman Reservoir in unincorporated Boulder County, Colorado. The dam and reservoir lie within an ephemeral drainage with a small drainage area. The reservoir is filled by local irrigation ditches.

Swede Lake has a maximum vertical height of 14.2 feet, a crest length of 1,506 feet, and a crest width of approximately 12 feet. The upstream slope is 2.5H:1V, and the downstream slope is 2.5H:1V.

The proposed scope of work included: 1) Mitigate seepage through embankment. 2) Repair primary outlet structure. 3) Repair irrigation outlet structure. 4) Repair and replace embankment erosion. 5) Remove sediment from Swede Lake. 6) Repair emergency spillway. 7) Repair spillway ditch. 8) Add erosion control where damaged or missing. 9) Revegetate disturbed areas.

This report summarizes the design changes, construction observations, and field testing results for the project.

2.0 DESIGN CHANGES

One change order was submitted to the SEO requesting the complete replacement of the dam embankment. It was determined that the existing embankment was inadequate due to the extent of roots through the embankment and the damage caused by the roots. Also, the sand blanket was removed from the design. The only reason the blanket was included in the original design was due to the uncertainty of potential roots in the embankment, which is now removed. The Change Order Requested dated October 4, 2017 outlines the changes to the original Construction Drawings. No changes to the Construction Specifications were required.

3.0 CONSTRUCTION

The contractor for this project was CAP Excavating and Demolition, out of Lyons, Colorado. Engineering Analytics, Inc. (EA) provided construction oversight throughout the construction phase of the project and provided oversight testing for backfill, bedding, and concrete. Construction at Swede Lake Dam began in August 2017 and was completed in March 2018. The construction progressed without major delays. After the decision was made to completely replace the dam embankment, the construction schedule was revised to construct the outlet works while the new embankment was being designed and approved. There were only a couple of weeks during this process where the contractor was slow on work. The weather conditions for the site during the construction phase are summarized in Appendix A.

The construction milestones are summarized in the following paragraphs. The construction photographs are presented in Appendix B.

3.1 Clay Excavation

The clay material used for the Swede Lake Dam embankment was excavated from the reservoir, 200 feet away from the toe of the dam. Prior to excavation, a dozer was used to strip the top 1 to 2 feet to access usable clay material. Clay was excavated using a loader and two haul trucks. The clay material was stockpiled at the original stock pile location just west of the staging area. Photo 1 shows the excavation of clay in the reservoir bottom.

3.2 Tree Removal and Root Chasing

Over 80 trees were removed from the dam or the immediate area surrounding the dam. Some trees were salvaged and used on another project. The trees were removed down to their root ball, and any remaining roots were chased down to ½ inch in diameter. As can be seen in the photos in Appendix B, there was a large volume of roots within the embankment. Also, some large roots (2 inches or greater) went all the way through the dam embankment. Photos 2-4 show the roots within the existing embankment.

3.3 Outlet Excavation and Installation

The two outlet locations were excavated according to the excavation detail on the drawings. The foundation of the outlet was excavated until good material was found, and then was filled with clay and compacted to meet grade, in accordance to the specifications. Photo 5 shows the excavation for the primary outlet pipe.

The base of the outlet easements and the outlet structures were formed and poured first. Then the two outlet pipes were placed and anchored to the base using metal belts and spacers between the pipe and base. The remainder of the outlet pipe encasement was formed and poured with battered sides. After the concrete set, the excavation was backfilled with compacted clay and the pipes were pressure tested. Both the primary outlet and the irrigation outlet passed the pressure tests. Photo 6 shows the formwork for the base of the outlet pipe encasement. Photos 9 and 10 show the outlet pipes strapped to the base of the encasement. Photo 11 shows the formwork of the irrigation outlet pipe before the remainder of the encasement was poured.

3.4 Emergency Spillway

The cutoff wall was constructed per the drawings and specifications. Both sides of the cutoff wall were filled and compacted simultaneously. A spillway channel was constructed and armored with bedding. Riprap was placed just downstream of the cutoff wall, along the outside of the channel's bend. Photos 12 and 14 show the construction of the emergency spillway cutoff wall.

3.5 Tower Installation

The outlet towers were formed and poured according to the Construction Drawings and Specifications. The towers were constructed with two separate pours – one for the base and one

for the walls. Lids with hatches were placed on top of the towers. Photos 7 and 8 show the heavy-duty sluice gates for the outlet works. Photo 13 shows the construction of the primary outlet tower.

3.6 Complete Removal and Replacement of Dam Embankment

The embankment required complete removal and replacement. The Contractor excavated the existing embankment and segregated out material with large quantities of roots for disposal in the reservoir bottom. Approved material was moisture conditioned and placed in the new embankment.

Prior to placing the new embankment, the Engineer inspected and approved the foundation. Material used for the embankment came from either the clay borrow from the far end of the reservoir or from the reusable material from the existing embankment. The material was moisturized and placed in lifts between about 8 and 12 inches of loose material. The material was compacted to 95% compaction or greater using a sheepfoot roller.

3.7 Riprap and Bedding

Existing riprap was removed and sorted through. The unwanted debris was separated and disposed of. The riprap was evaluated, and the portion that passed visual inspection was reused later in the project. The contractor placed 24-inch layer of riprap on top a 6-inch layer of bedding. Existing riprap that could be salvaged and reused was mixed in with imported Class 12 ($D_{50} = 12''$) riprap. Photo 15 shows the placement of bedding and riprap on the dam embankment.

3.8 Toe Drain

The toe drain was installed with the use of a box being pulled along the embankment. No. 8 Gavel was placed in the trench, then the box was placed on the gravel. C33 sand was placed in the box along with the toe drain. The box was then pulled across the embankment. The top gravel layer was placed on top of the sand, and the drain was covered with 2 feet of embankment. The sand, gavel, and embankment cover were all compacted according to the specifications.

4.0 MATERIALS TESTING

Quality assurance testing was conducted on the project as work progressed. Appendix C of this report provides a summary of all testing conducted. The summary includes gradations for the riprap bedding, proctor density curves for the backfill, moisture and density tests for the backfill, and concrete test data. As the tests indicate, the materials used during construction meet the project requirements except for some of the concrete strength tests. The 28-day strength of the concrete placed in the vault structure at Station 4+00 on November 20, 2017 required structural calculations to check that the structure still met design requirements. EA addressed the concrete strength with calculations in a technical letter dated January 8, 2018, which is included in Appendix D. It was concluded that the structures pass the structural design criteria with the low break strengths.

5.0 STANDARD OF CARE

The information contained in this report represents our findings at the time and location as indicated in this report. The methods utilized are in accordance with currently accepted engineering and testing procedures and other than this, no warranty, either expressed or implied, is intended.

APPENDIX A

WEATHER CONDITIONS
































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Today Forecast

Weather History for KLMO - August, 2017

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
		1 <div></div> <div>Actual: 91° 57° 0.00 in</div> <div>Average: - - - in</div>	2 <div></div> <div>Actual: 90° 54° 0.00 in</div> <div>Average: - - - in</div>	3 <div></div> <div>Actual: 69° 57° 0.10 in</div> <div>Average: - - - in</div>	4 <div></div> <div>Actual: 90° 54° 0.03 in</div> <div>Average: - - - in</div>	5 <div></div> <div>Actual: 85° 57° 0.27 in</div> <div>Average: - - - in</div>
6 <div></div> <div>Actual: 74° 54° 0.00 in</div> <div>Average: - - - in</div>	7 <div></div> <div>Actual: 64° 58° 0.31 in</div> <div>Average: - - - in</div>	8 <div></div> <div>Actual: 77° 57° 0.31 in</div> <div>Average: - - - in</div>	9 <div></div> <div>Actual: 78° 56° 0.01 in</div> <div>Average: - - - in</div>	10 <div></div> <div>Actual: 78° 55° 0.09 in</div> <div>Average: - - - in</div>	11 <div></div> <div>Actual: 80° 57° 0.00 in</div> <div>Average: - - - in</div>	12 <div></div> <div>Actual: 82° 55° 0.00 in</div> <div>Average: - - - in</div>
13 <div></div> <div>Actual: 88° 57° 0.00 in</div> <div>Average: - - - in</div>	14 <div></div> <div>Actual: 92° 56° 0.00 in</div> <div>Average: - - - in</div>	15 <div></div> <div>Actual: 84° 56° 0.02 in</div> <div>Average: - - - in</div>	16 <div></div> <div>Actual: 78° 58° 0.01 in</div> <div>Average: - - - in</div>	17 <div></div> <div>Actual: 90° 51° 0.00 in</div> <div>Average: - - - in</div>	18 <div></div> <div>Actual: 89° 52° 0.00 in</div> <div>Average: - - - in</div>	19 <div></div> <div>Actual: 98° 53° 0.00 in</div> <div>Average: - - - in</div>
20 <div></div> <div>Actual: 90° 57° 0.00 in</div> <div>Average: - - - in</div>	21 <div></div> <div>Actual: 90° 55° 0.00 in</div> <div>Average: - - - in</div>	22 <div></div> <div>Actual: 83° 55° 0.00 in</div> <div>Average: - - - in</div>	23 <div></div> <div>Actual: 91° 57° 0.00 in</div> <div>Average: - - - in</div>	24 <div></div> <div>Actual: 89° 54° 0.00 in</div> <div>Average: - - - in</div>	25 <div></div> <div>Actual: 91° 49° 0.00 in</div> <div>Average: - - - in</div>	26 <div></div> <div>Actual: 96° 54° 0.00 in</div> <div>Average: - - - in</div>
27 <div></div> <div>Actual: 88° 59° 0.00 in</div> <div>Average: - - - in</div>	28 <div></div> <div>Actual: 91° 54° 0.00 in</div> <div>Average: - - - in</div>	29 <div></div> <div>Actual: 92° 53° 0.00 in</div> <div>Average: - - - in</div>	30 <div></div> <div>Actual: 90° 54° 0.00 in</div> <div>Average: - - - in</div>	31 <div></div> <div>Actual: 88° 54° 0.00 in</div> <div>Average: - - - in</div>		

Calendar Legend



Sunny
Clear



Mostly Cloudy



Partly Cloudy



Cloudy



Rain



Snow



Hail Flurries



Thunderstorms



Hazy
Fog



Sleet



'?' denotes
'chance of'



Unknown

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Today Forecast

Weather History for KLMO - September, 2017

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
					1 Actual: 90° 59° Average: - - - in	2 Actual: 91° 54° Average: - - - in
3 Actual: 99° 52° Average: - - - in	4 Actual: 90° 55° Average: - - - in	5 Actual: 72° 51° Average: - - - in	6 Actual: 81° 46° Average: - - - in	7 Actual: 85° 47° Average: - - - in	8 Actual: 86° 50° Average: - - - in	9 Actual: 93° 53° Average: - - - in
10 Actual: 92° 53° Average: - - - in	11 Actual: 87° 59° Average: - - - in	12 Actual: 93° 52° Average: - - - in	13 Actual: 88° 55° Average: - - - in	14 Actual: 90° 57° Average: - - - in	15 Actual: 84° 50° Average: - - - in	16 Actual: 66° 48° Average: - - - in
17 Actual: 76° 45° Average: - - - in	18 Actual: 84° 44° Average: - - - in	19 Actual: 88° 48° Average: - - - in	20 Actual: 77° 40° Average: - - - in	21 Actual: 90° 40° Average: - - - in	22 Actual: 74° 44° Average: - - - in	23 Actual: 56° 47° Average: - - - in
24 Actual: 52° 47° Average: - - - in	25 Actual: 57° 43° Average: - - - in	26 Actual: 65° 46° Average: - - - in	27 Actual: 55° 51° Average: - - - in	28 Actual: 59° 51° Average: - - - in	29 Actual: 62° 44° Average: - - - in	30 Actual: 71° 40° Average: - - - in

Calendar Legend



Sunny
Clear



Mostly Cloudy



Partly Cloudy



Cloudy



Rain



Snow



Hail Flurries



Thunderstorms



Hazy
Fog



Sleet



'?' denotes
'chance of'



Unknown
































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Today Forecast

Weather History for KLMO - October, 2017

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
1 Actual: 70° 50° Average: - - - in 	2 Actual: 50° 39° Average: - - - in 	3 Actual: 58° 34° Average: - - - in 	4 Actual: 69° 40° Average: - - - in 	5 Actual: 68° 43° Average: - - - in 	6 Actual: 72° 48° Average: - - - in 	7 Actual: 77° 40° Average: - - - in 
8 Actual: 65° 37° Average: - - - in 	9 Actual: 43° 31° Average: - - - in 	10 Actual: 60° 26° Average: - - - in 	11 Actual: 72° 30° Average: - - - in 	12 Actual: 79° 34° Average: - - - in 	13 Actual: 65° 35° Average: - - - in 	14 Actual: 64° 32° Average: - - - in 
15 Actual: 62° 28° Average: - - - in 	16 Actual: 79° 32° Average: - - - in 	17 Actual: 81° 31° Average: - - - in 	18 Actual: 79° 41° Average: - - - in 	19 Actual: 74° 32° Average: - - - in 	20 Actual: 80° 39° Average: - - - in 	21 Actual: 63° 33° Average: - - - in 
22 Actual: 72° 29° Average: - - - in 	23 Actual: 65° 36° Average: - - - in 	24 Actual: 64° 29° Average: - - - in 	25 Actual: 84° 34° Average: - - - in 	26 Actual: 66° 33° Average: - - - in 	27 Actual: 46° 22° Average: - - - in 	28 Actual: 63° 37° Average: - - - in 
29 Actual: 77° 34° Average: - - - in 	30 Actual: 43° 32° Average: - - - in 	31 Actual: 61° 28° Average: - - - in 				

Calendar Legend



Sunny
Clear



Mostly Cloudy



Partly Cloudy



Cloudy



Rain



Snow



Hail Flurries



Thunderstorms



Hazy
Fog



Sleet



'?' denotes
'chance of'



Unknown

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Today Forecast

Weather History for KLMO - November, 2017

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
			1	2	3	4
			Actual: 75° 57° 0.00 in Average: - - - in	Actual: 60° 32° 0.00 in Average: - - - in	Actual: 57° 33° 0.00 in Average: - - - in	Actual: 72° 31° 0.00 in Average: - - - in
5	6	7	8	9	10	11
Actual: 48° 35° 0.09 in Average: - - - in	Actual: 43° 34° MM in Average: - - - in	Actual: 35° 28° MM in Average: - - - in	Actual: 46° 29° 0.03 in Average: - - - in	Actual: 42° 28° 0.00 in Average: - - - in	Actual: 58° 24° 0.00 in Average: - - - in	Actual: 62° 30° 0.00 in Average: - - - in
12	13	14	15	16	17	18
Actual: 55° 26° 0.00 in Average: - - - in	Actual: 73° 32° 0.00 in Average: - - - in	Actual: 73° 35° 0.00 in Average: - - - in	Actual: 53° 28° 0.00 in Average: - - - in	Actual: 73° 27° 0.00 in Average: - - - in	Actual: 65° 39° 0.07 in Average: - - - in	Actual: 52° 25° 0.00 in Average: - - - in
19	20	21	22	23	24	25
Actual: 56° 19° 0.00 in Average: - - - in	Actual: 71° 37° 0.00 in Average: - - - in	Actual: 57° 32° 0.00 in Average: - - - in	Actual: 72° 31° 0.00 in Average: - - - in	Actual: 70° 36° 0.00 in Average: - - - in	Actual: 75° 40° 0.00 in Average: - - - in	Actual: 63° 32° 0.00 in Average: - - - in
26	27	28	29	30		
Actual: 68° 32° 0.00 in Average: - - - in	Actual: 78° 41° 0.00 in Average: - - - in	Actual: 49° 27° 0.00 in Average: - - - in	Actual: 67° 23° 0.00 in Average: - - - in	Actual: 54° 22° 0.00 in Average: - - - in		

Calendar Legend

-  Sunny Clear
-  Mostly Cloudy
-  Partly Cloudy
-  Cloudy
-  Rain
-  Snow
-  Hail Flurries
-  Thunderstorms
-  Hazy Fog
-  Sleet
-  '?' denotes 'chance of'
-  Unknown

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Today Forecast

Weather History for KLMO - December, 2017

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
					<div>1</div> <div>Actual: 60° 26° Average: - - - in</div> <div></div>	<div>2</div> <div>Actual: 63° 32° Average: - - - in</div> <div></div>
<div>3</div> <div>Actual: 62° 30° Average: - - - in</div> <div></div>	<div>4</div> <div>Actual: 45° 19° Average: - - - in</div> <div></div>	<div>5</div> <div>Actual: 48° 12° Average: - - - in</div> <div></div>	<div>6</div> <div>Actual: 43° 19° Average: - - - in</div> <div></div>	<div>7</div> <div>Actual: 38° 10° Average: - - - in</div> <div></div>	<div>8</div> <div>Actual: 63° 24° Average: - - - in</div> <div></div>	<div>9</div> <div>Actual: 64° 21° Average: - - - in</div> <div></div>
<div>10</div> <div>Actual: 61° 19° Average: - - - in</div> <div></div>	<div>11</div> <div>Actual: 59° 22° Average: - - - in</div> <div></div>	<div>12</div> <div>Actual: 66° 23° Average: - - - in</div> <div></div>	<div>13</div> <div>Actual: 56° 35° Average: - - - in</div> <div></div>	<div>14</div> <div>Actual: 45° 19° Average: - - - in</div> <div></div>	<div>15</div> <div>Actual: 65° 16° Average: - - - in</div> <div></div>	<div>16</div> <div>Actual: 58° 33° Average: - - - in</div> <div></div>
<div>17</div> <div>Actual: 42° 21° Average: - - - in</div> <div></div>	<div>18</div> <div>Actual: 54° 17° Average: - - - in</div> <div></div>	<div>19</div> <div>Actual: 51° 23° Average: - - - in</div> <div></div>	<div>20</div> <div>Actual: 67° 23° Average: - - - in</div> <div></div>	<div>21</div> <div>Actual: 36° 7° Average: - - - in</div> <div></div>	<div>22</div> <div>Actual: 40° 3° Average: - - - in</div> <div></div>	<div>23</div> <div>Actual: 34° 10° Average: - - - in</div> <div></div>
<div>24</div> <div>Actual: 28° -3° Average: - - - in</div> <div></div>	<div>25</div> <div>Actual: 27° 11° Average: - - - in</div> <div></div>	<div>26</div> <div>Actual: 14° 6° Average: - - - in</div> <div></div>	<div>27</div> <div>Actual: 55° 0° Average: - - - in</div> <div></div>	<div>28</div> <div>Actual: 50° 23° Average: - - - in</div> <div></div>	<div>29</div> <div>Actual: 67° 16° Average: - - - in</div> <div></div>	<div>30</div> <div>Actual: 24° 13° Average: - - - in</div> <div></div>
<div>31</div> <div>Actual: 27° 15° Average: - - - in</div> <div></div>						

Calendar Legend

Sunny Clear

Mostly Cloudy

Partly Cloudy

Cloudy

Rain

Snow

Hail Flurries

Thunderstorms

Hazy Fog

Sleet

'?' denotes 'chance of'

Unknown

Lemoore (Abandoned) Willett A, CO 🏠

Lemoore (Abandoned) Willett A

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Today Forecast

Weather History for KLMO - January, 2018

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
	<div>1</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 30° 11° MM in Average: - - - in</div>	<div>2</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 46° 8° 0.00 in Average: - - - in</div>	<div>3</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 52° 14° 0.00 in Average: - - - in</div>	<div>4</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 54° 23° 0.00 in Average: - - - in</div>	<div>5</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 53° 21° 0.00 in Average: - - - in</div>	<div>6</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 54° 24° 0.00 in Average: - - - in</div>
<div>7</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 54° 26° 0.00 in Average: - - - in</div>	<div>8</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 48° 20° 0.00 in Average: - - - in</div>	<div>9</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 69° 33° 0.00 in Average: - - - in</div>	<div>10</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 52° 25° 0.00 in Average: - - - in</div>	<div>11</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 47° 17° 0.00 in Average: - - - in</div>	<div>12</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 48° 23° 0.00 in Average: - - - in</div>	<div>13</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 50° 17° 0.00 in Average: - - - in</div>
<div>14</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 52° 20° 0.00 in Average: - - - in</div>	<div>15</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 31° 4° MM in Average: - - - in</div>	<div>16</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 35° -3° 0.01 in Average: - - - in</div>	<div>17</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 55° 8° 0.00 in Average: - - - in</div>	<div>18</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 61° 18° 0.00 in Average: - - - in</div>	<div>19</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 74° 32° 0.00 in Average: - - - in</div>	<div>20</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 50° 24° MM in Average: - - - in</div>
<div>21</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 32° 23° MM in Average: - - - in</div>	<div>22</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 49° 7° 0.11 in Average: - - - in</div>	<div>23</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 42° 15° 0.00 in Average: - - - in</div>	<div>24</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 52° 12° 0.00 in Average: - - - in</div>	<div>25</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 46° 21° 0.00 in Average: - - - in</div>	<div>26</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 42° 24° 0.00 in Average: - - - in</div>	<div>27</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 42° 21° 0.00 in Average: - - - in</div>
<div>28</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 56° 18° 0.00 in Average: - - - in</div>	<div>29</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 60° 21° 0.00 in Average: - - - in</div>	<div>30</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 66° 29° 0.00 in Average: - - - in</div>	<div>31</div> <div><div><div></div><div></div><div></div></div><div></div></div> <div>Actual: 58° 23° 0.00 in Average: - - - in</div>			

Calendar Legend



Sunny
Clear



Mostly Cloudy



Partly Cloudy



Cloudy



Rain



Snow



Hail Flurries



Thunderstorms



Hazy
Fog



Sleet



'?' denotes
'chance of'



Unknown

Lemoore (Abandoned) Willett A, CO 🏠

Lemoore (Abandoned) Willett A

© 2:22 PM MDT on April 13, 2018 (GMT -0600)

Today Forecast

Weather History for KLMO - February, 2018

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
				1 Actual: 33° 25° Average: - - MM in - in	2 Actual: 44° 24° Average: - - 0.00 in - in	3 Actual: 62° 29° Average: - - 0.00 in - in
4 Actual: 52° 16° Average: - - MM in - in	5 Actual: 59° 22° Average: - - MM in - in	6 Actual: 51° 25° Average: - - 0.00 in - in	7 Actual: 51° 27° Average: - - 0.00 in - in	8 Actual: 61° 27° Average: - - 0.00 in - in	9 Actual: 56° 14° Average: - - MM in - in	10 Actual: 20° 3° Average: - - MM in - in
11 Actual: 36° 2° Average: - - MM in - in	12 Actual: 25° 17° Average: - - MM in - in	13 Actual: 60° 13° Average: - - 0.00 in - in	14 Actual: 65° 42° Average: - - 0.00 in - in	15 Actual: 54° 23° Average: - - MM in - in	16 Actual: 44° 23° Average: - - 0.00 in - in	17 Actual: 59° 37° Average: - - 0.00 in - in
18 Actual: 68° 25° Average: - - MM in - in	19 Actual: 23° 5° Average: - - MM in - in	20 Actual: 18° -9° Average: - - MM in - in	21 Actual: 28° -6° Average: - - MM in - in	22 Actual: 34° 6° Average: - - 0.00 in - in	23 Actual: 36° 8° Average: - - MM in - in	24 Actual: 39° 8° Average: - - 0.07 in - in
25 Actual: 45° 25° Average: - - 0.00 in - in	26 Actual: 53° 21° Average: - - 0.00 in - in	27 Actual: 55° 23° Average: - - 0.00 in - in	28 Actual: 53° 25° Average: - - 0.00 in - in			

Calendar Legend



Sunny
Clear



Mostly Cloudy



Partly Cloudy



Cloudy



Rain



Snow



Hail Flurries



Thunderstorms



Hazy
Fog



Sleet



'?' denotes
'chance of'



Unknown

Lemoore (Abandoned) Willett A, CO 🏠

Lemoore (Abandoned) Willett A

© 2:22 PM MDT on April 13, 2018 (GMT -0600)

Today Forecast

Weather History for KLMO - March, 2018

Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday
				1 Actual: 52° 22° Average: - - - in	2 Actual: 72° 28° Average: - - - in	3 Actual: 70° 27° Average: - - - in
4 Actual: 69° 26° Average: - - - in	5 Actual: 44° 29° Average: - - - in	6 Actual: 51° 20° Average: - - - in	7 Actual: 55° 16° Average: - - - in	8 Actual: 67° 22° Average: - - - in	9 Actual: 68° 43° Average: - - - in	10 Actual: 57° 25° Average: - - - in
11 Actual: 54° 17° Average: - - - in	12 Actual: 59° 19° Average: - - - in	13 Actual: 60° 22° Average: - - - in	14 Actual: 70° 25° Average: - - - in	15 Actual: 67° 29° Average: - - - in	16 Actual: 57° 33° Average: - - - in	17 Actual: 64° 26° Average: - - - in
18 Actual: 59° 28° Average: - - - in	19 Actual: 50° 30° Average: - - - in	20 Actual: 56° 26° Average: - - - in	21 Actual: 64° 26° Average: - - - in	22 Actual: 78° 35° Average: - - - in	23 Actual: 71° 48° Average: - - - in	24 Actual: 68° 31° Average: - - - in
25 Actual: 64° 30° Average: - - - in	26 Actual: 53° 34° Average: - - - in	27 Actual: 53° 31° Average: - - - in	28 Actual: 48° 30° Average: - - - in	29 Actual: 51° 25° Average: - - - in	30 Actual: 66° 27° Average: - - - in	31 Actual: 60° 32° Average: - - - in

Calendar Legend



Sunny
Clear



Mostly Cloudy



Partly Cloudy



Cloudy



Rain



Snow



Hail Flurries



Thunderstorms



Hazy
Fog



Sleet



'?' denotes
'chance of'



Unknown

APPENDIX B
CONSTRUCTION PHOTOGRAPHS



Photo 01 (08-04-2017) Excavation of clay



Photo 02 (08-22-2017) Roots in embankment by primary spillway (1)



Photo 03 (08-22-2017) Roots in embankment by primary spillway (2)



Photo 04 (08-25-2017) Roots in north dam embankment



Photo 05 (09-20-2017) Outlet excavation



Photo 06 (10-18-2017) Irrigation outlet rebar



Photo 07 (10-24-2017) 15-inch heavy duty slide gate



Photo 08 (10-24-2017) 24-inch heavy duty slide gate



Photo 09 (10-24-2017) Irrigation PIP anchored to base of encasement



Photo 10 (10-24-2017) Primary outlet DIP anchored to base of encasement



Photo 11 (11-03-2017) Irrigation outlet ecasement rebar and formwork



Photo 12 (11-20-2017) Spillway grade beam reinforcement



Photo 13 (11-21-2017) Northeast wingwall foundation after form removal



Photo 14 (12-14-2017) Spillway grade control beam backfill



Photo 15 (01-02-2018) Bedding and riprap on upstream face

APPENDIX C

MATERIALS TESTING

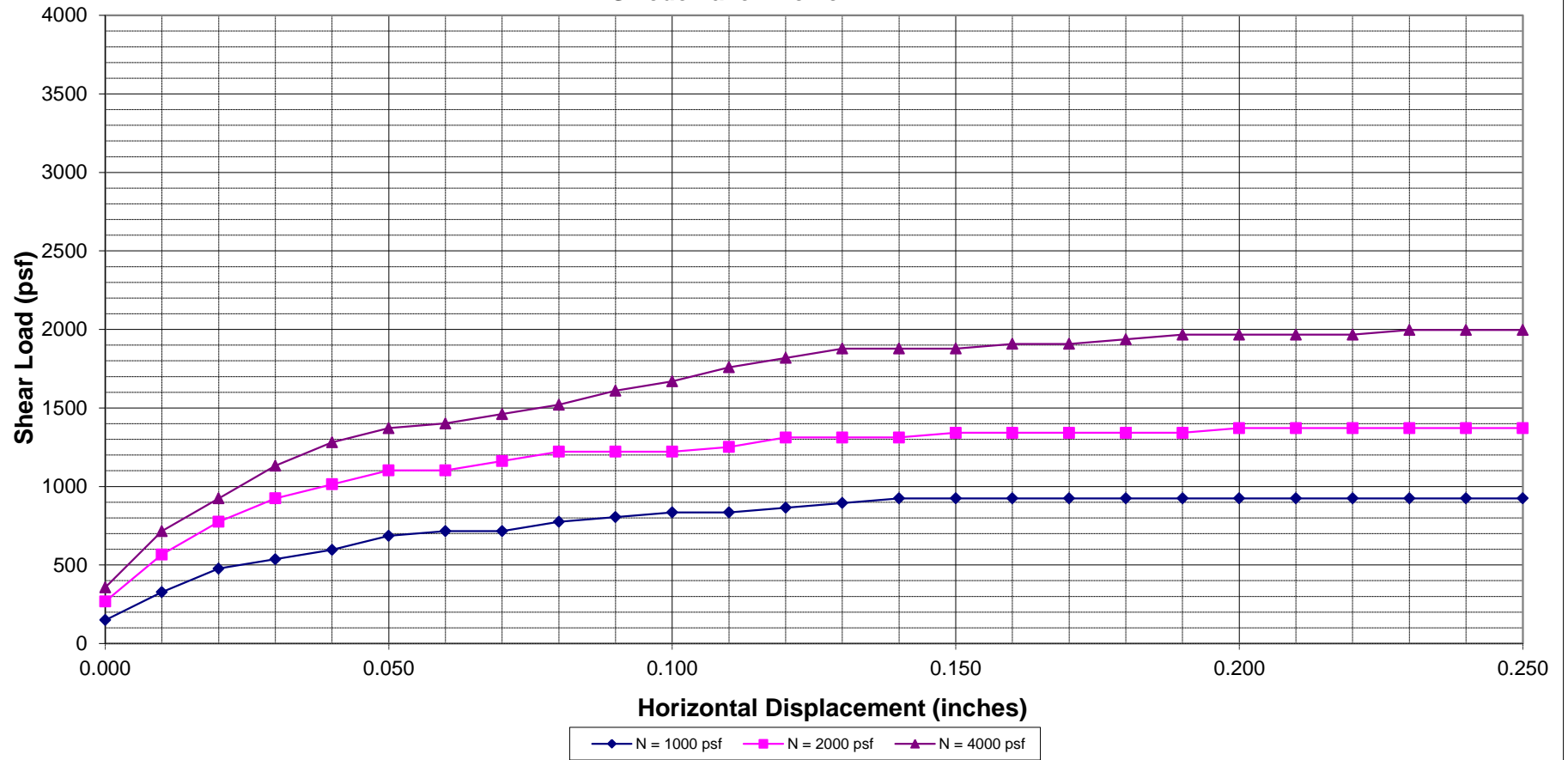
[illegible]

ENGINEERING ANALYTICS							
CONSOLIDATED DRAINED DIRECT SHEAR TEST							
		Swede Lake		Borrow 1	0		
NORMAL	SHEAR	SHEAR	HORIZ	HORIZ		HORIZ	SHEAR
LOAD	LOAD	LOAD	DIAL	DISP		DISP	LOAD
(psf)	(lbs)	(psf)	0.001(inch)	(inch)		(inch)	(psf)
2,000	0	0	660	0.000		0.000	0
2,000	9	268	670	0.010		0.010	268
2,000	19	566	680	0.020		0.020	566
2,000	26	775	690	0.030		0.030	775
2,000	31	924	700	0.040		0.040	924
2,000	34	1014	710	0.050		0.050	1014
2,000	37	1103	720	0.060		0.060	1103
2,000	37	1103	730	0.070		0.070	1103
2,000	39	1163	740	0.080		0.080	1163
2,000	41	1222	750	0.090		0.090	1222
2,000	41	1222	760	0.100		0.100	1222
2,000	41	1222	770	0.110		0.110	1222
2,000	42	1252	780	0.120		0.120	1252
2,000	44	1312	790	0.130		0.130	1312
2,000	44	1312	800	0.140		0.140	1312
2,000	44	1312	810	0.150		0.150	1312
2,000	45	1341	820	0.160		0.160	1341
2,000	45	1341	830	0.170		0.170	1341
2,000	45	1341	840	0.180		0.180	1341
2,000	45	1341	850	0.190		0.190	1341
2,000	45	1341	860	0.200		0.200	1341
2,000	46	1371	870	0.210		0.210	1371
2,000	46	1371	880	0.220		0.220	1371
2,000	46	1371	890	0.230		0.230	1371
2,000	46	1371	900	0.240		0.240	1371
2,000	46	1371	910	0.250		0.250	1371
2,000	46	1371	920	0.260		0.260	1371
2,000	46	1371	930	0.270		0.270	1371

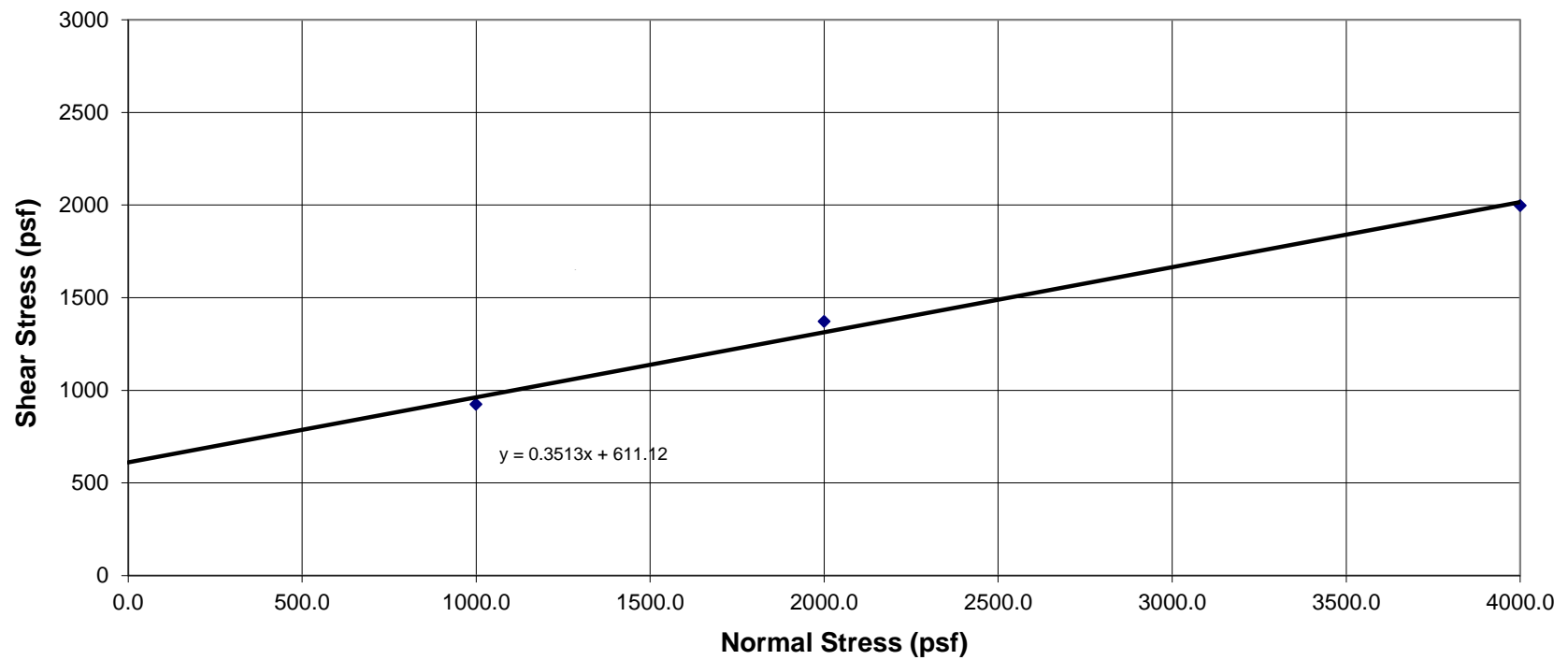
ENGINEERING ANALYTICS							
CONSOLIDATED DRAINED DIRECT SHEAR TEST							
		Swede Lake		Borrow 1	0		
NORMAL	SHEAR	SHEAR	HORIZ	HORIZ		HORIZ	SHEAR
LOAD	LOAD	LOAD	DIAL	DISP		DISP	LOAD
(psf)	(lbs)	(psf)	0.001(inch)	(inch)		(inch)	(psf)
4,000	0	0	660	0.000		0.000	0
4,000	12	358	670	0.010		0.010	358
4,000	24	715	680	0.020		0.020	715
4,000	31	924	690	0.030		0.030	924
4,000	38	1133	700	0.040		0.040	1133
4,000	43	1282	710	0.050		0.050	1282
4,000	46	1371	720	0.060		0.060	1371
4,000	47	1401	730	0.070		0.070	1401
4,000	49	1461	740	0.080		0.080	1461
4,000	51	1520	750	0.090		0.090	1520
4,000	54	1610	760	0.100		0.100	1610
4,000	56	1669	770	0.110		0.110	1669
4,000	59	1759	780	0.120		0.120	1759
4,000	61	1818	790	0.130		0.130	1818
4,000	63	1878	800	0.140		0.140	1878
4,000	63	1878	810	0.150		0.150	1878
4,000	63	1878	820	0.160		0.160	1878
4,000	64	1908	830	0.170		0.170	1908
4,000	64	1908	840	0.180		0.180	1908
4,000	65	1938	850	0.190		0.190	1938
4,000	66	1967	860	0.200		0.200	1967
4,000	66	1967	870	0.210		0.210	1967
4,000	66	1967	880	0.220		0.220	1967
4,000	66	1967	890	0.230		0.230	1967
4,000	67	1997	900	0.240		0.240	1997
4,000	67	1997	910	0.250		0.250	1997
4,000	67	1997	920	0.260		0.260	1997
4,000	67	1997	930	0.270		0.270	1997

Direct Shear Test ASTM D3080

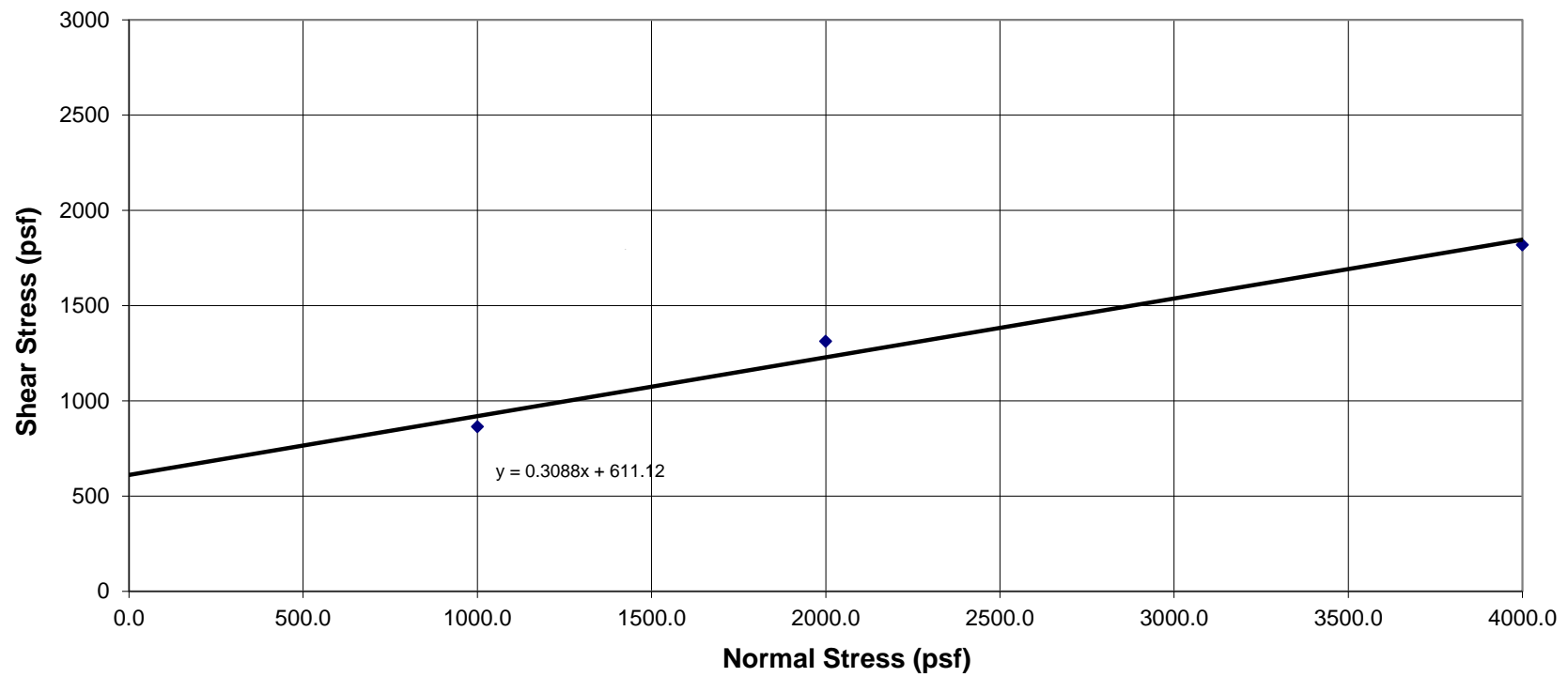
Swede Lake - Borrow 1



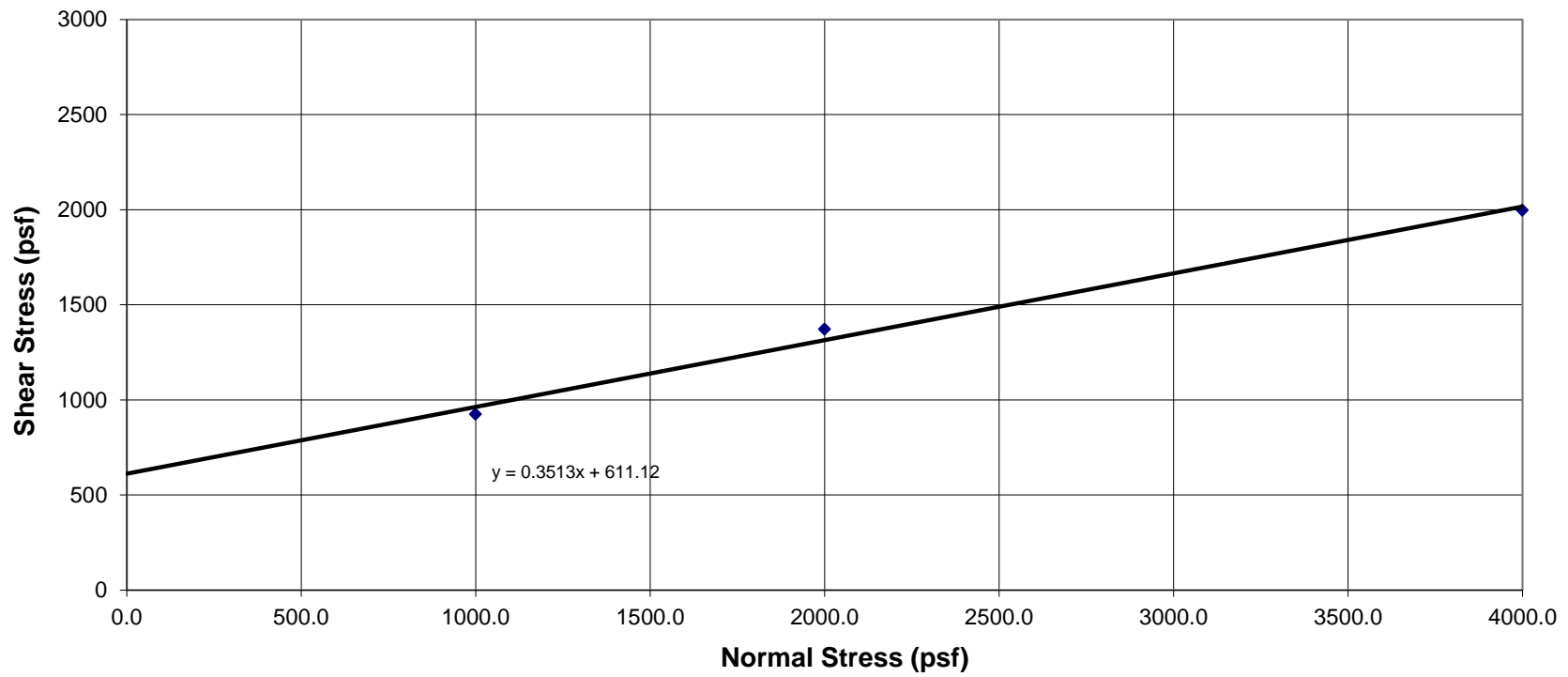
Direct Shear Test ASTM D3080
Swede Lake - Borrow 1
Max Stress



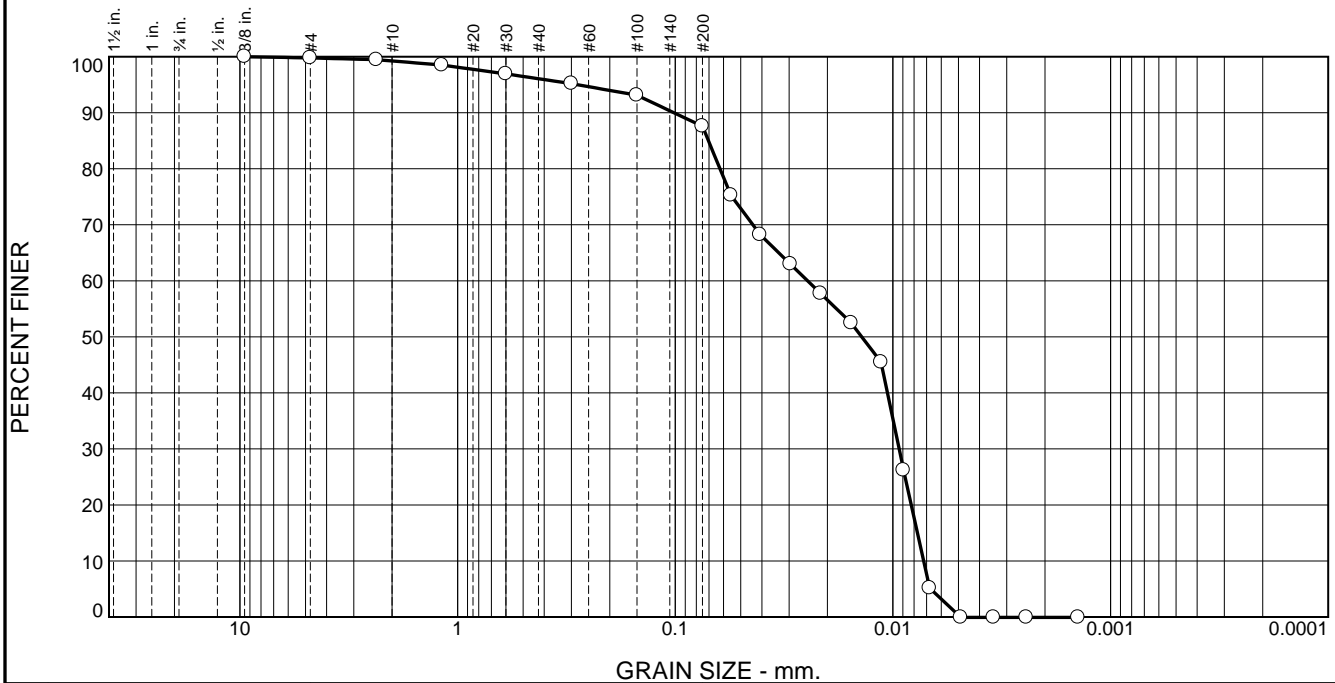
Direct Shear Test ASTM D3080
Swede Lake - Borrow 1
5% Strain



Direct Shear Test ASTM D3080
Swede Lake - Borrow 1
10% Strain



Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.2	0.6	3.1	8.5	87.3	0.3

TEST RESULTS (AASHTO T 27)			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
3/8	100.0		
#4	99.8		
#8	99.5		
#16	98.5		
#30	96.9		
#50	95.2		
#100	93.1		
#200	87.6		
0.055 mm.	75.2		
0.0407 mm.	68.2		
0.0296 mm.	63.0		
0.0215 mm.	57.7		
0.0156 mm.	52.5		
0.0113 mm.	45.5		
0.0089 mm.	26.2		
0.0068 mm.	5.2		
0.0049 mm.			
0.0034 mm.			
0.0024 mm.			
0.0014 mm.			

* (no specification provided)

Material Description

Atterberg Limits (ASTM D 4318)

PL= LL= PI=

Classification

USCS (D 2487)= AASHTO (M 145)=

Coefficients

D₉₀= 0.1015 D₈₅= 0.0704 D₆₀= 0.0247
D₅₀= 0.0139 D₃₀= 0.0094 D₁₅= 0.0077
D₁₀= 0.0072 C_u= 3.41 C_c= 0.49

Remarks

Date Received: 8/14/17

Date Tested: 8/17/17

Tested By: KG

Checked By: KG

Title:

Source of Sample: Borrow 1
Sample Number: 1

Date Sampled: 8/14/17

ENGINEERING ANALYTICS, INC.

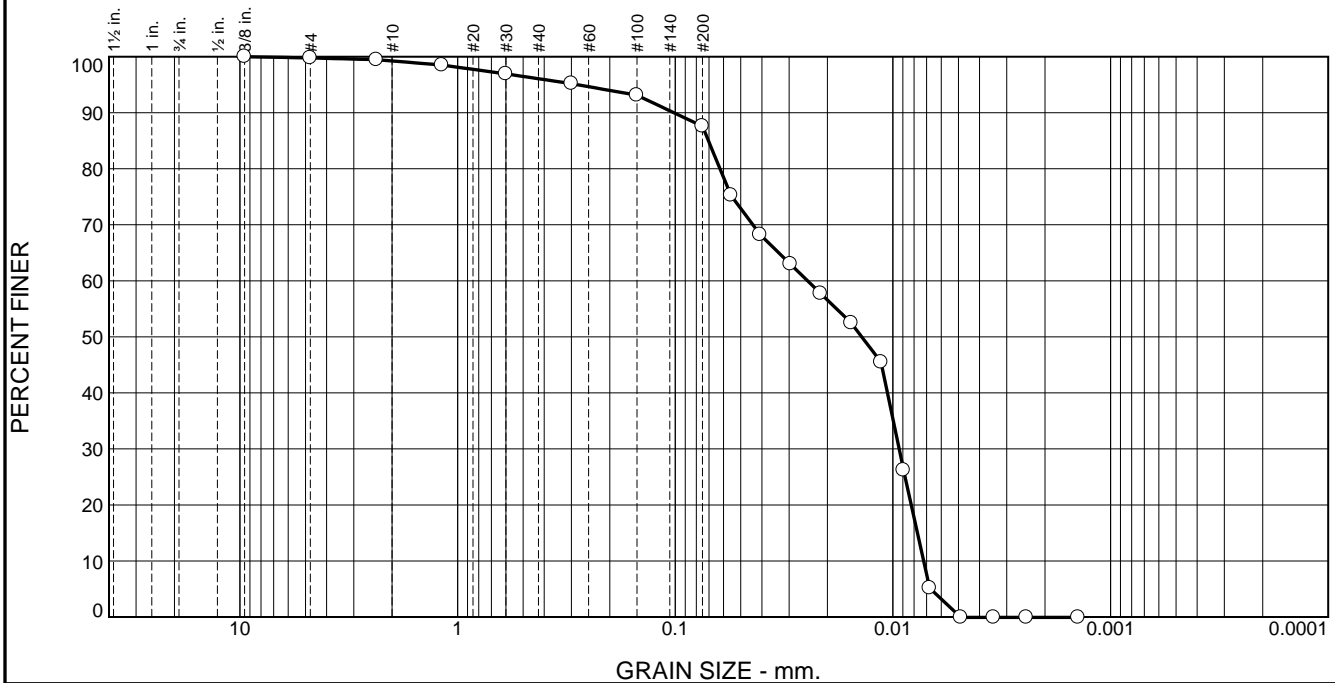
Client: Boulder County Parks & open Space

Project: Swede Lake

Project No: 110480

Figure

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.2	0.6	3.1	8.5	87.3	0.3

TEST RESULTS (AASHTO T 27)			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
3/8	100.0		
#4	99.8		
#8	99.5		
#16	98.5		
#30	96.9		
#50	95.2		
#100	93.1		
#200	87.6		
0.0555 mm.	75.2		
0.0407 mm.	68.2		
0.0296 mm.	63.0		
0.0215 mm.	57.7		
0.0156 mm.	52.5		
0.0113 mm.	45.5		
0.0089 mm.	26.2		
0.0068 mm.	5.2		
0.0049 mm.			
0.0034 mm.			
0.0024 mm.			
0.0014 mm.			

* (no specification provided)

Material Description

Clay

Atterberg Limits (ASTM D 4318)

PL= 15 LL= 42 PI= 27

Classification

USCS (D 2487)= CL AASHTO (M 145)= A-7-6(24)

Coefficients

D₉₀= 0.1015 D₈₅= 0.0704 D₆₀= 0.0247
D₅₀= 0.0139 D₃₀= 0.0094 D₁₅= 0.0077
D₁₀= 0.0072 C_u= 3.41 C_c= 0.49

Remarks

Date Received: 8/14/17

Date Tested: 8/17/17

Tested By: KG

Checked By: KG

Title:

Source of Sample: Borrow 1
Sample Number: 1

Date Sampled: 8/14/17

ENGINEERING ANALYTICS, INC.

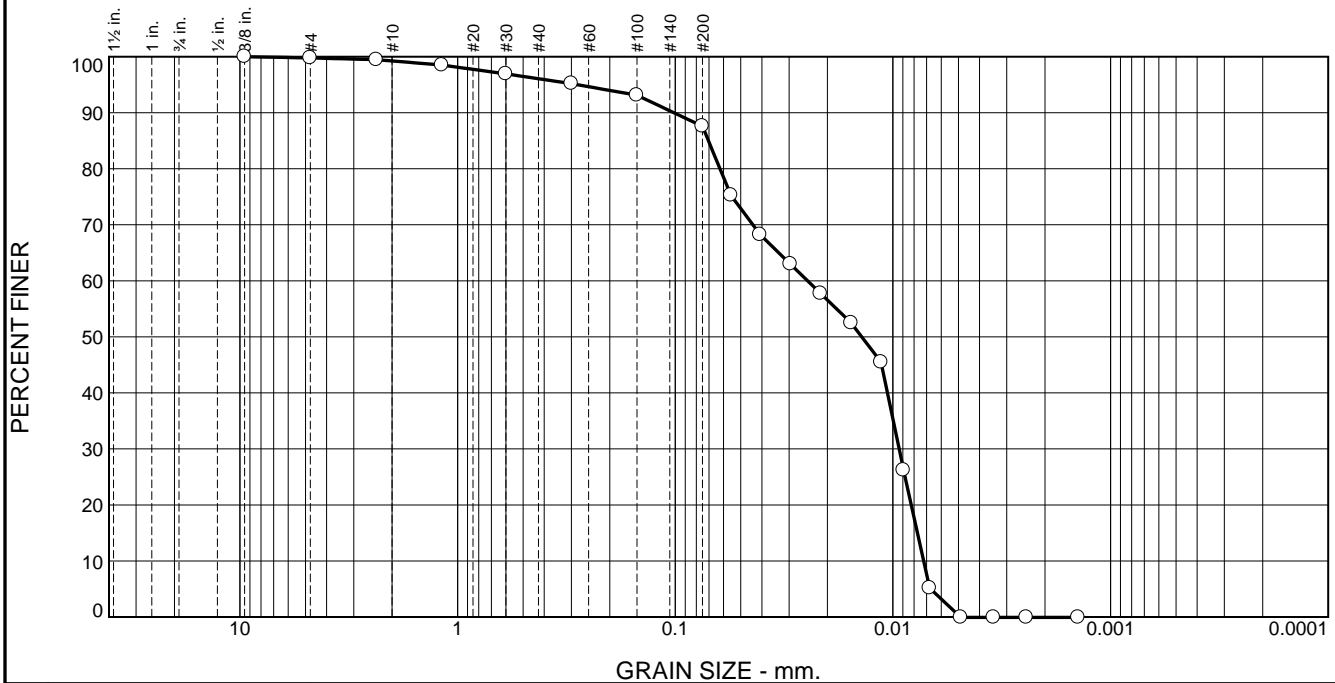
Client: Boulder County Parks & Open Space

Project: Swede Lake

Project No: 110480

Figure

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.2	0.6	3.1	8.5	87.3	0.3

TEST RESULTS (AASHTO T 27)			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
3/8	100.0		
#4	99.8		
#8	99.5		
#16	98.5		
#30	96.9		
#50	95.2		
#100	93.1		
#200	87.6		
0.0555 mm.	75.2		
0.0407 mm.	68.2		
0.0296 mm.	63.0		
0.0215 mm.	57.7		
0.0156 mm.	52.5		
0.0113 mm.	45.5		
0.0089 mm.	26.2		
0.0068 mm.	5.2		
0.0049 mm.			
0.0034 mm.			
0.0024 mm.			
0.0014 mm.			

* (no specification provided)

Material Description

Clay

Atterberg Limits (ASTM D 4318)

PL= 15 LL= 42 PI= 27

Classification

USCS (D 2487)= CL AASHTO (M 145)= A-7-6(24)

Coefficients

D₉₀= 0.1015 D₈₅= 0.0704 D₆₀= 0.0247
D₅₀= 0.0139 D₃₀= 0.0094 D₁₅= 0.0077
D₁₀= 0.0072 C_u= 3.41 C_c= 0.49

Remarks

Date Received: 8/14/17

Date Tested: 8/17/17

Tested By: KG

Checked By: KG

Title:

Source of Sample: Borrow 1
Sample Number: 1

Date Sampled: 8/14/17

ENGINEERING ANALYTICS, INC.

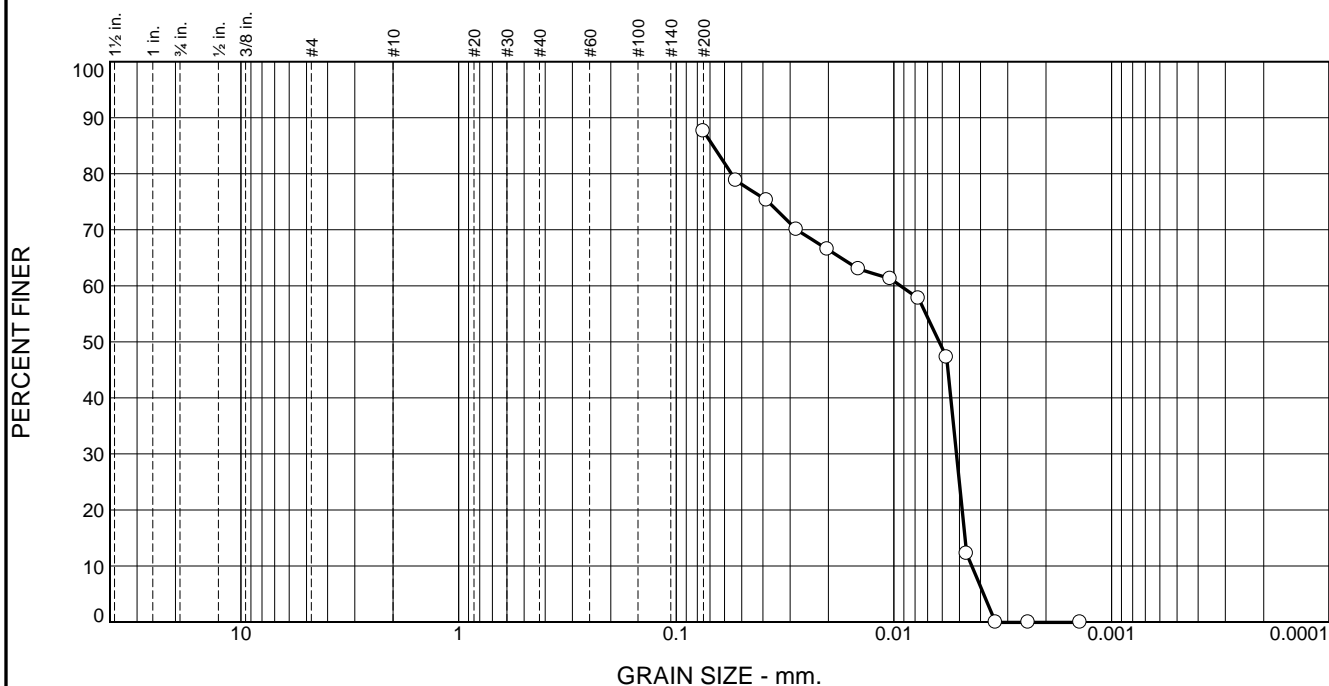
Client: Boulder County Parks & Open Space

Project: Swede Lake

Project No: 110480

Figure

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
						62.8	24.8

TEST RESULTS			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
#200	87.6		
0.0532 mm.	78.8		
0.0384 mm.	75.3		
0.0280 mm.	70.0		
0.0202 mm.	66.5		
0.0145 mm.	63.0		
0.0104 mm.	61.3		
0.0077 mm.	57.7		
0.0057 mm.	47.2		
0.0046 mm.	12.2		
0.0034 mm.			
0.0024 mm.			
0.0014 mm.			

* (no specification provided)

Material Description		
Clay		
Atterberg Limits (ASTM D 4318) PL= 15 LL= 40 PI= 25		
Classification USCS (D 2487)= AASHTO (M 145)=		
Coefficients D ₉₀ = D ₈₅ = 0.0678 D ₆₀ = 0.0093 D ₅₀ = 0.0062 D ₃₀ = 0.0052 D ₁₅ = 0.0047 D ₁₀ = 0.0044 C _u = 2.13 C _c = 0.65		
Remarks		
Date Received:	Date Tested:	
Tested By:		
Checked By:		
Title:		

Source of Sample: Borrow 3
Sample Number: 1

Date Sampled:

ENGINEERING ANALYTICS, INC.

Client: Boulder County Parks & Open Space
Project: Swede Lake

Project No: 110480

Figure

COMPACTION TEST REPORT

Curve No.: 1

Project No.: 110480

Date: 9/18/2017

Project: Swede Lake

Client: Boulder County Parks & Open Space

Source of Sample: Borrow 1

Sample Number: 1

Remarks:

MATERIAL DESCRIPTION

Description: Clay

Classifications -

USCS: CL

AASHTO: A-7-6(24)

Nat. Moist. =

Sp.G. =

Liquid Limit = 42

Plasticity Index = 27

%<No.10 = 99.2 %

%<No.40 = 96.1 %

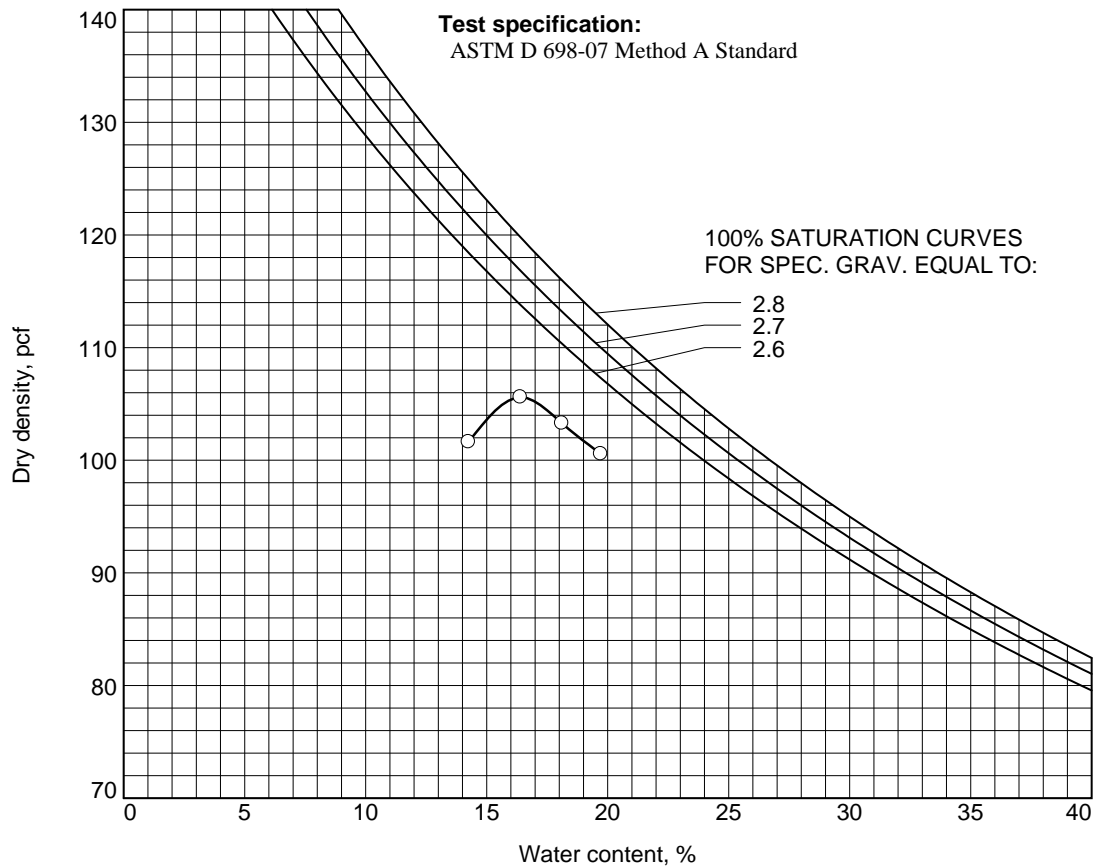
%<No.60 = 94.6 %

%<No.200 = 87.6 %

TEST RESULTS

Maximum dry density = 105.6 pcf

Optimum moisture = 16.4 %



Figure

ENGINEERING ANALYTICS, INC.

Tested By: KG

COMPACTION TEST REPORT

Curve No.: 2

Project No.: 110480

Date: 9/19/2017

Project: Swede Lake

Client: Boulder County Parks & Open Space

Source of Sample: Borrow 3

Sample Number: 1

Remarks:

MATERIAL DESCRIPTION

Description: Clay

Classifications -

USCS:

AASHTO:

Nat. Moist. =

Sp.G. =

Liquid Limit = 40

Plasticity Index = 25

%<No.10 =

%<No.40 =

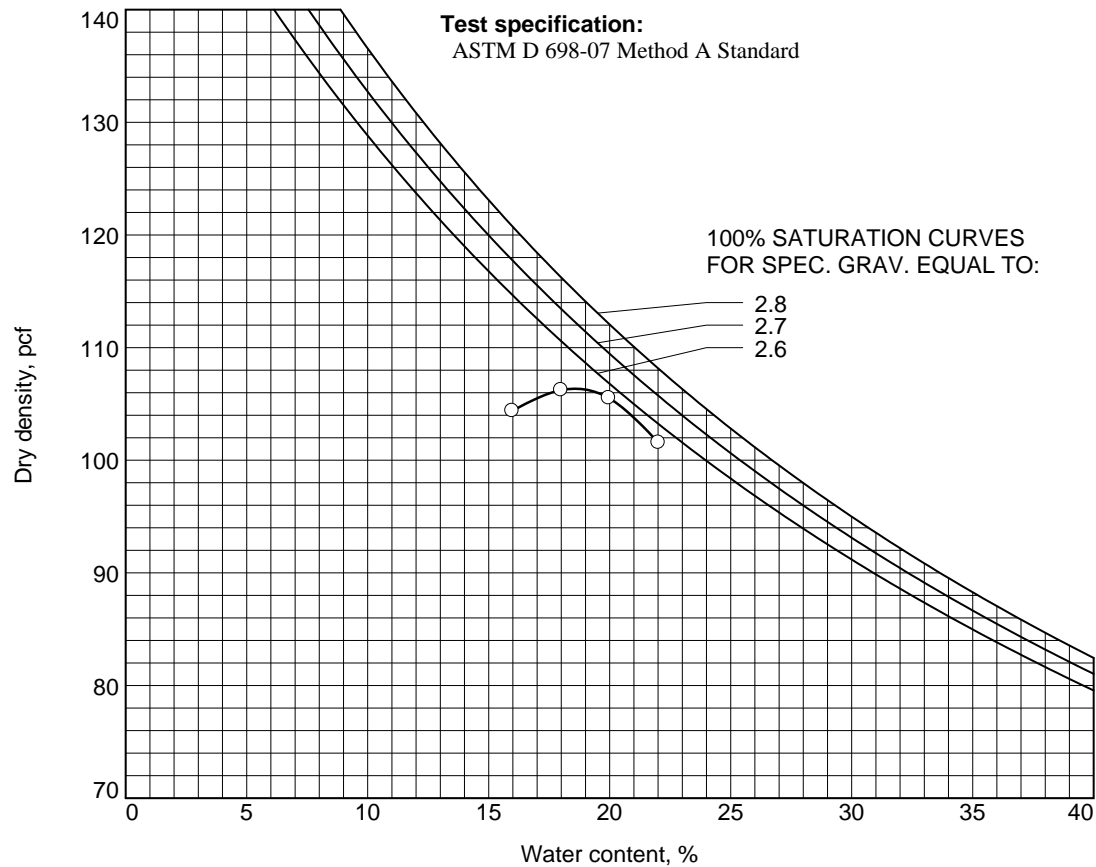
%<No.60 =

%<No.200 = 87.6 %

TEST RESULTS

Maximum dry density = 106.4 pcf

Optimum moisture = 18.6 %



Figure

ENGINEERING ANALYTICS, INC.

Tested By: KG

COMPACTION TEST REPORT

Curve No.: 3

Project No.: 110480

Date: 10/20/2017

Project: Swede Lake

Client: Boulder County Parks & Open Space

Source of Sample: Borrow 4

Sample Number: 1

Remarks:

MATERIAL DESCRIPTION

Description: Clay

Classifications -

USCS:

AASHTO:

Nat. Moist. =

Sp.G. =

Liquid Limit =

Plasticity Index =

%<No.10 =

%<No.40 =

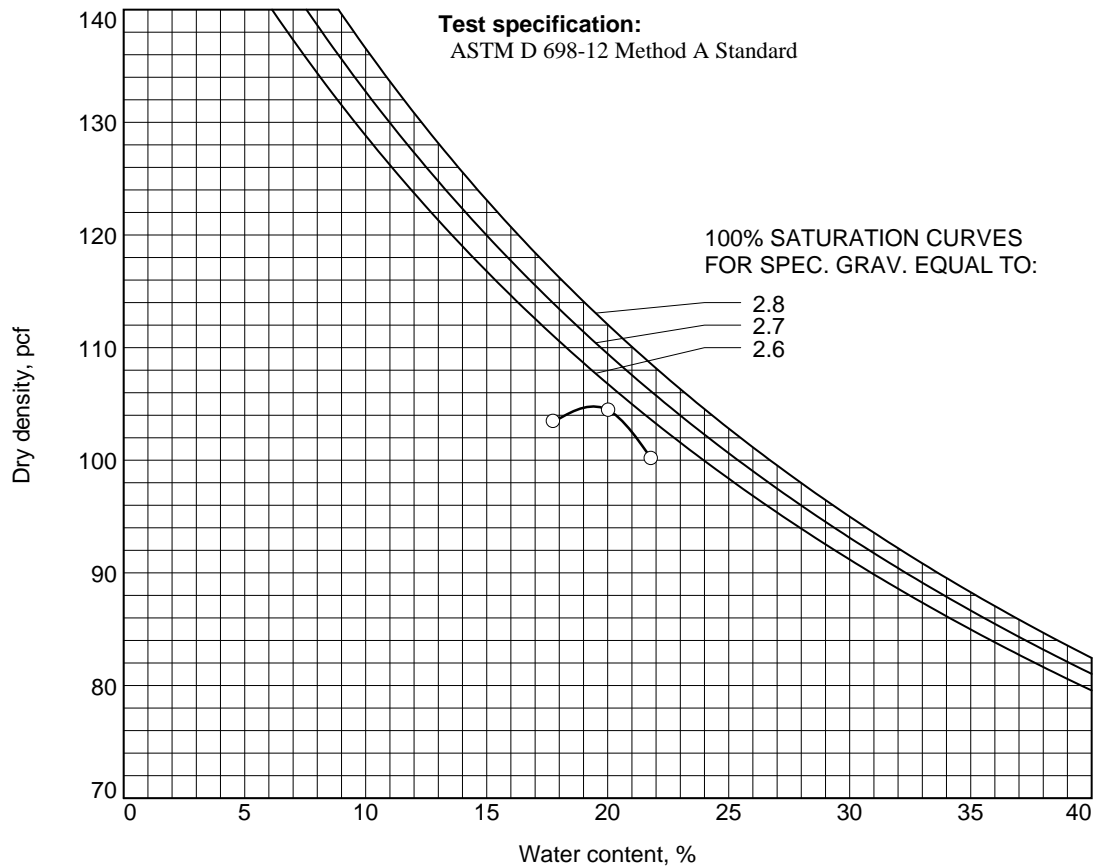
%<No.60 =

%<No.200 =

TEST RESULTS

Maximum dry density = 104.8 pcf

Optimum moisture = 19.4 %



Figure

ENGINEERING ANALYTICS, INC.

Tested By: KG Checked By: KG

COMPACTION TEST REPORT

Curve No.: 4

Date: 10/30/17

Project No.: 110480

Project: Swede Lake

Client: Boulder County Parks & Open Space

Source of Sample: Borrow 5

Sample Number: 1

Remarks:

MATERIAL DESCRIPTION

Description: Silty Clay

Classifications -

USCS:

AASHTO:

Nat. Moist. =

Sp.G. =

Liquid Limit =

Plasticity Index =

%<No.10 =

%<No.40 =

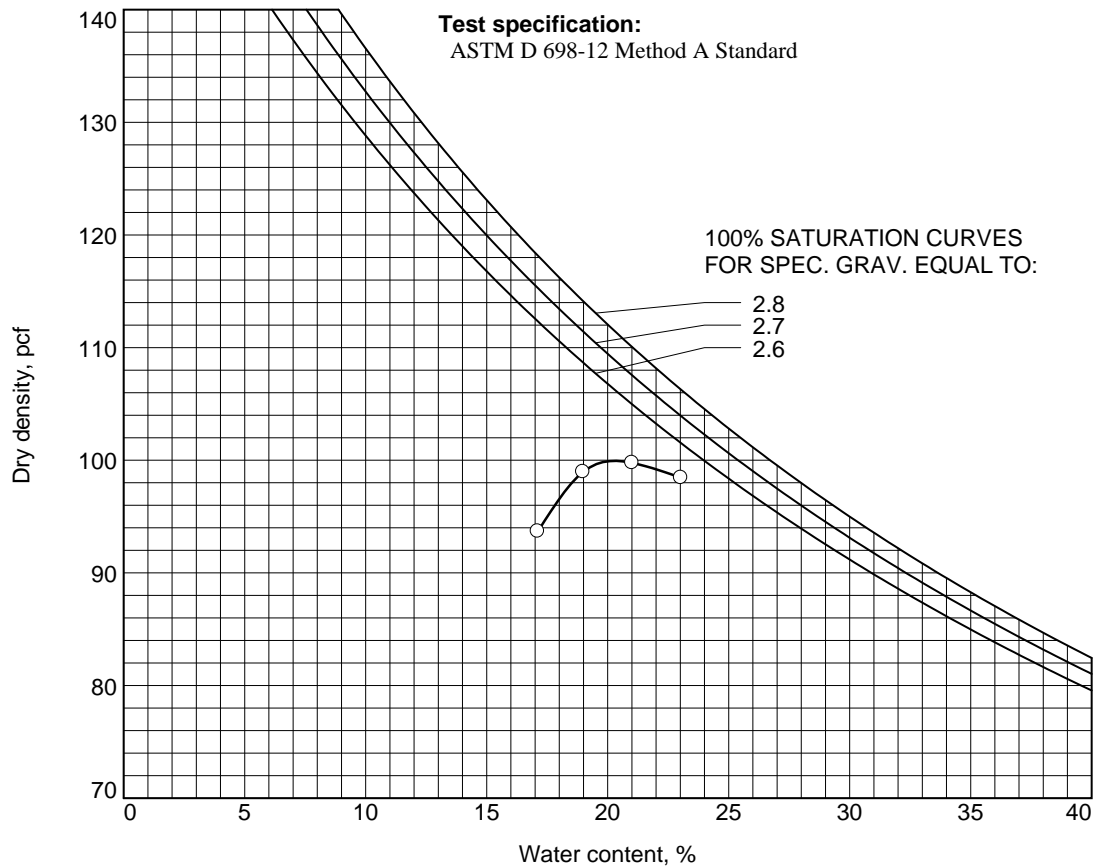
%<No.60 =

%<No.200 =

TEST RESULTS

Maximum dry density = 99.9 pcf

Optimum moisture = 20.3 %



Figure

ENGINEERING ANALYTICS, INC.

Tested By: KG

SUMMARY OF LABORATORY TEST RESULTS

JOB NAME:

Swede Lake

JOB NUMBER:

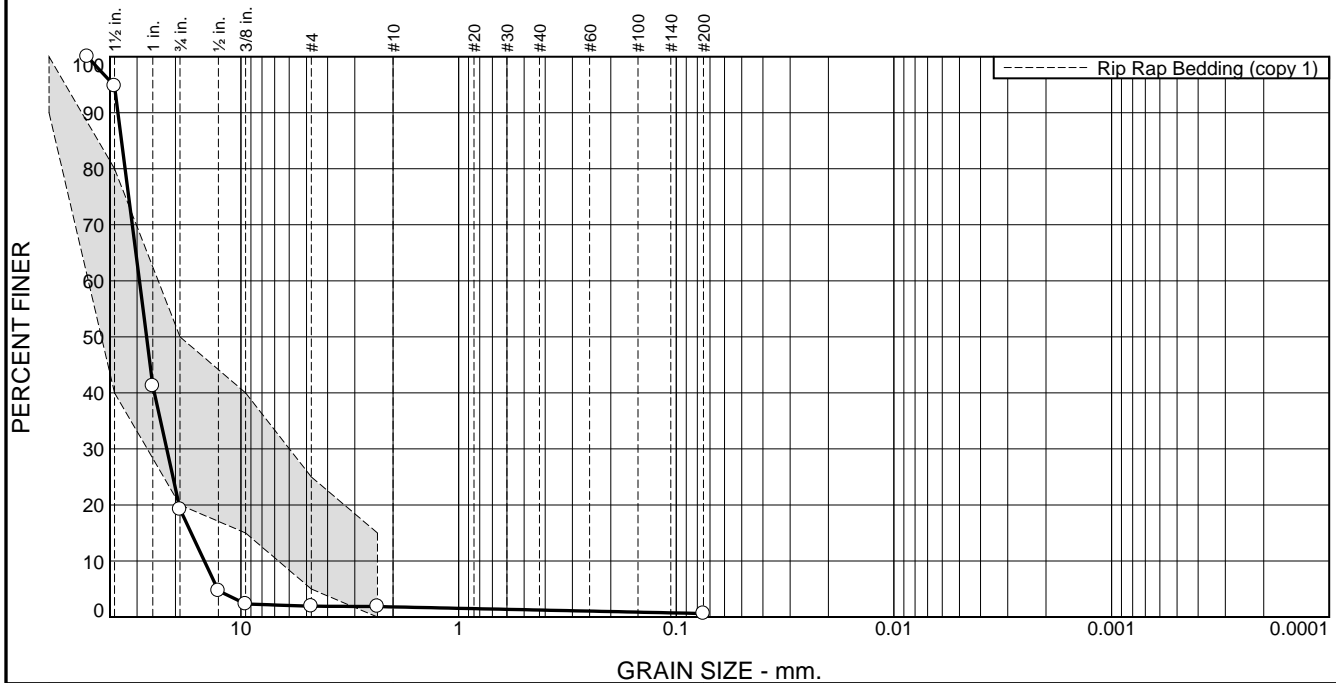
110480

DATE:

9/27/2017

Depth (ft.)	Sample Type	Moisture (%)	Falling Head Permeability	Atterbergs LL / PL / PI	Grain Size Analysis	Percent Passing No. 200 (%)	Hydrometer	D698 Standard Proctor
Borrow 1								
	BKT		3.60E-07	42 / 15 / 27	(1)	87.2	(1)	105.6 @ 16.4%
Borrow 2								
	BKT			33 / 18 / 15		79.1		
Borrow 3								
	BKT			40 / 15 / 25		87.6	(1)	106.4 @ 18.6%
*LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index N.P. = Non Plastic						(1) = See Attached		

Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0.0	98.2	0.6	0.6	0.6	

TEST RESULTS (AASHTO T 27)			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
2'	100.0		
1-1/2"	94.8	40.0 - 80.0	X
1"	41.2		
3/4"	19.2	20.0 - 50.0	X
1/2"	4.7		
3/8"	2.3	15.0 - 40.0	X
#4	1.9	5.0 - 25.0	X
#8	1.9	0.0 - 15.0	
#200	0.6		

* Rip Rap Bedding (copy 1)

Material Description

Bedding Material

Atterberg Limits (ASTM D 4318)

PL= LL= PI=

Classification

USCS (D 2487)= GP AASHTO (M 145)=

Coefficients

D₉₀= 36.7456 D₈₅= 35.3803 D₆₀= 29.2783
D₅₀= 27.1431 D₃₀= 21.9317 D₁₅= 16.9321
D₁₀= 14.7256 C_u= 1.99 C_c= 1.12

Remarks

Date Received: 12/15/17

Date Tested: 12/20/2017

Tested By: KG

Checked By: KG

Title:

Source of Sample: Bedding Material
Sample Number: 1

Date Sampled: 12/15/17

ENGINEERING ANALYTICS, INC.

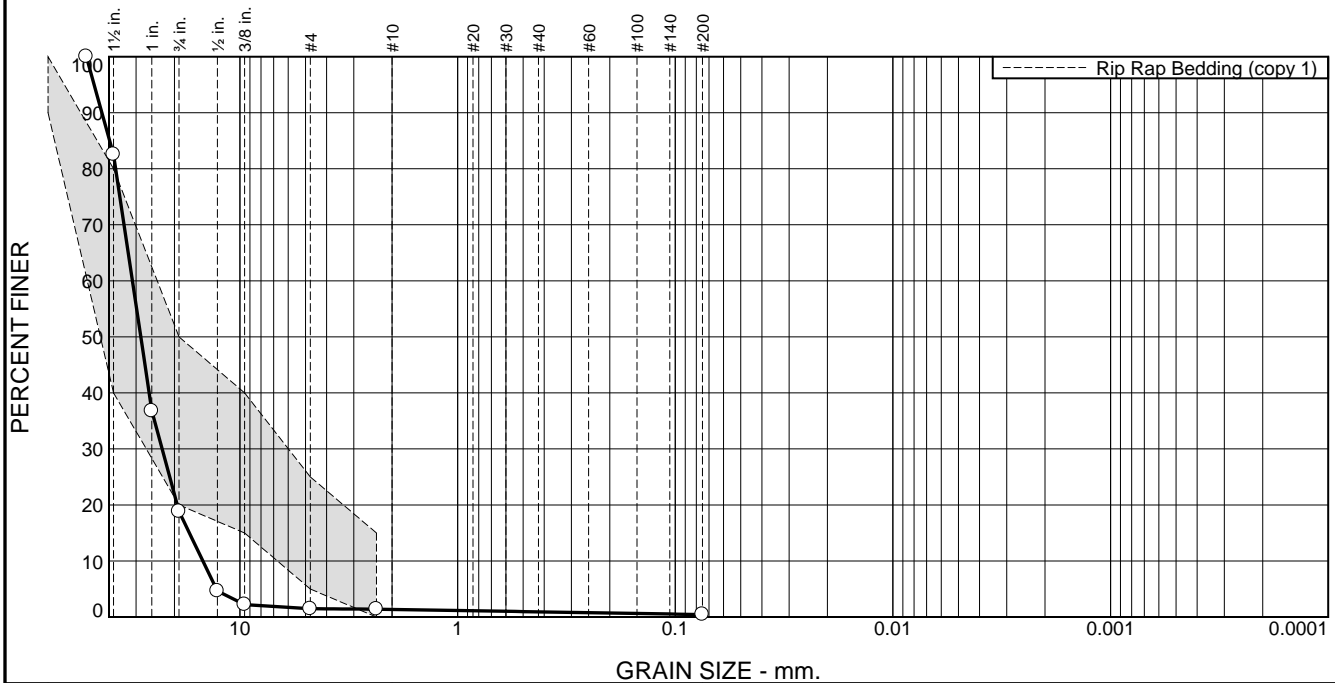
Client: Boulder County Parks & Open Space

Project: Swede Lake

Project No: 110480

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0.0	98.6	0.5	0.5	0.4	

TEST RESULTS (AASHTO T 27)			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
2"	100.0		
1-1/2"	82.5	40.0 - 80.0	X
1"	36.8		
3/4"	18.8	20.0 - 50.0	X
1/2"	4.7		
3/8"	2.2	15.0 - 40.0	X
#4	1.5	5.0 - 25.0	X
#8	1.4	0.0 - 15.0	
#200	0.4		

* Rip Rap Bedding (copy 1)

Material Description

Rip Rap Bedding Material

Atterberg Limits (ASTM D 4318)

PL= LL= PI=

Classification

USCS (D 2487)= GP AASHTO (M 145)=

Coefficients

D₉₀= 43.0840 D₈₅= 39.6773 D₆₀= 31.2013
D₅₀= 28.5550 D₃₀= 22.7826 D₁₅= 17.0742
D₁₀= 14.7990 C_u= 2.11 C_c= 1.12

Remarks

Date Received: 12/21/17

Date Tested: 12/27/2017

Tested By: KG

Checked By: KG

Title:

Source of Sample: Bedding Material
Sample Number: 2

Date Sampled: 12/21/17

ENGINEERING ANALYTICS, INC.

Client: Boulder County Parks & Open Space

Project: Swede Lake

Project No: 110480

Figure

Relative Density Testing

Project: Swede Lake Date: 10/27/2017

Material: Sand Description: Sand

Tested By: KG TEST PROCEDURE: ASTM 4253 & D4254

NOTE: Smith Geotechnical standard bucket: vol. = 0.50 ft³, Diam = 11" = 0.9167'
and depth 9.125 = 0.760'

Density		Left	Right
Empty Bucket	<u>21.20</u> lb	Initial dial reading: L <u>0</u> in <u>0</u> in	
Bucket+ Loose Soil	<u>68.30</u> lb		
		Compacted dial reading: L <u>1.985</u> in R <u>1.985</u> in	
WT of soil:	<u>47.10</u> lb	Change in Height: F <u>1.99</u> in B <u>1.99</u> in	
Volume at start:	<u>0.50</u> ft ³	Average: <u>1.99</u> in <u>0.17</u> ft	

Change in Volume: 0.11 ft³ [(change in ht)*Area of cylinder(0.66)]

Compacted Volume: 0.39 ft³ [(Volume at start)-(change in vol.)]

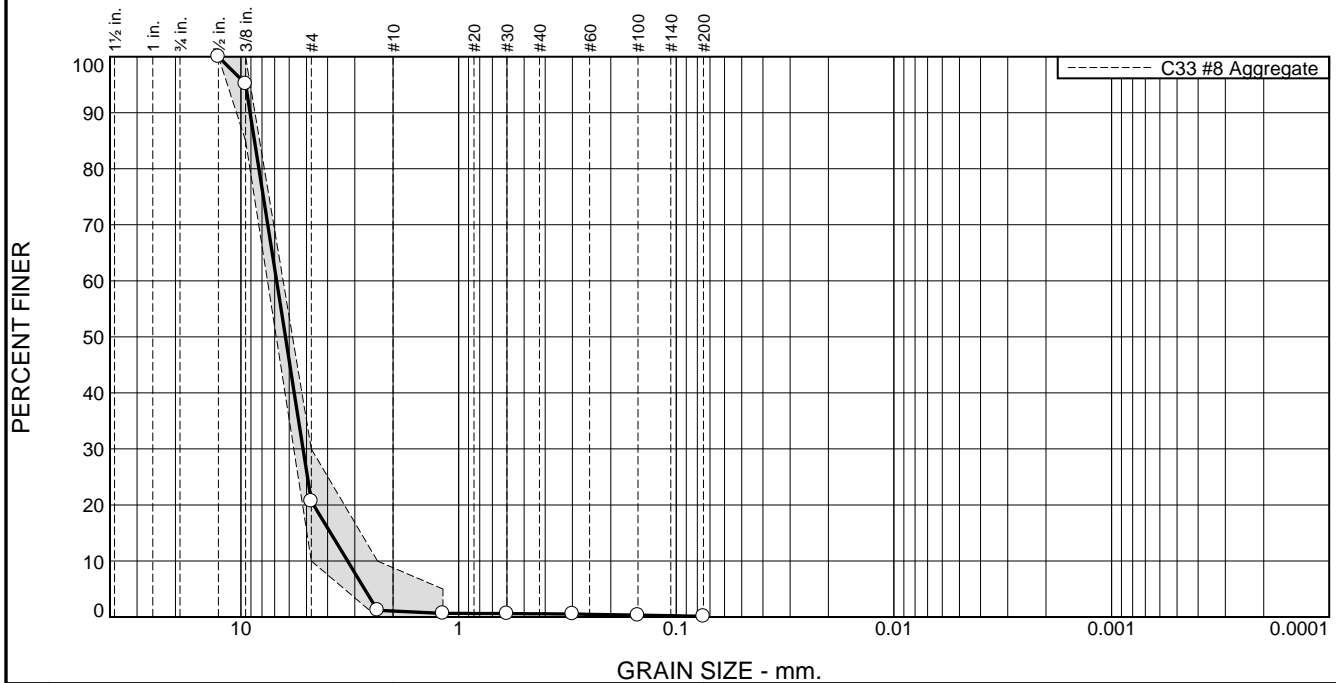
Minimum unit wt γ : 93.9 pcf [(wt of soil)/Volume at start]

Maximum unit wt γ : 119.9 pcf [(wt of soil)/(compacted volume)]

70% unit wt γ : 112.1 pcf [$\gamma_{min} + 0.7*(\gamma_{max}-\gamma_{min})$]

Relative Density	Dry Unit Weight		Relative Density	Dry Unit Weight	
55% unit wt	<u>108.2</u>	pcf	71% unit wt	<u>112.4</u>	pcf
56% unit wt	<u>108.5</u>	pcf	72% unit wt	<u>112.6</u>	pcf
57% unit wt	<u>108.7</u>	pcf	73% unit wt	<u>112.9</u>	pcf
58% unit wt	<u>109.0</u>	pcf	74% unit wt	<u>113.2</u>	pcf
59% unit wt	<u>109.3</u>	pcf	75% unit wt	<u>113.4</u>	pcf
60% unit wt	<u>109.5</u>	pcf	76% unit wt	<u>113.7</u>	pcf
61% unit wt	<u>109.8</u>	pcf	77% unit wt	<u>113.9</u>	pcf
62% unit wt	<u>110.0</u>	pcf	78% unit wt	<u>114.2</u>	pcf
63% unit wt	<u>110.3</u>	pcf	79% unit wt	<u>114.5</u>	pcf
64% unit wt	<u>110.6</u>	pcf	80% unit wt	<u>114.7</u>	pcf
65% unit wt	<u>110.8</u>	pcf	81% unit wt	<u>115.0</u>	pcf
66% unit wt	<u>111.1</u>	pcf	82% unit wt	<u>115.3</u>	pcf
67% unit wt	<u>111.3</u>	pcf	83% unit wt	<u>115.5</u>	pcf
68% unit wt	<u>111.6</u>	pcf	84% unit wt	<u>115.8</u>	pcf
69% unit wt	<u>111.9</u>	pcf	85% unit wt	<u>116.0</u>	pcf
70% unit wt	<u>112.1</u>	pcf			

Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0.0	98.9	0.5	0.5	0.1	

TEST RESULTS (AASHTO T 27)			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
1/2	100.0	100.0	
3/8	95.2	85.0 - 100.0	
#4	20.7	10.0 - 30.0	
#8	1.2	0.0 - 10.0	
#16	0.7	0.0 - 5.0	
#30	0.6		
#50	0.5		
#100	0.3		
#200	0.1		

* C33 #8 Aggregate

Material Description

#8 Aggregate

Atterberg Limits (ASTM D 4318)

PL= LL= PI=

Classification

USCS (D 2487)= GP AASHTO (M 145)=

Coefficients

D₉₀= 9.0768 D₈₅= 8.6626 D₆₀= 6.8585
D₅₀= 6.2468 D₃₀= 5.1823 D₁₅= 3.8737
D₁₀= 3.2366 C_u= 2.12 C_c= 1.21

Remarks

Date Received: 1/5/18

Date Tested: 1/10/2018

Tested By: KG

Checked By: KG

Title:

Source of Sample: #8 Aggregate
Sample Number: 1

Date Sampled: 1/5/18

ENGINEERING ANALYTICS, INC.

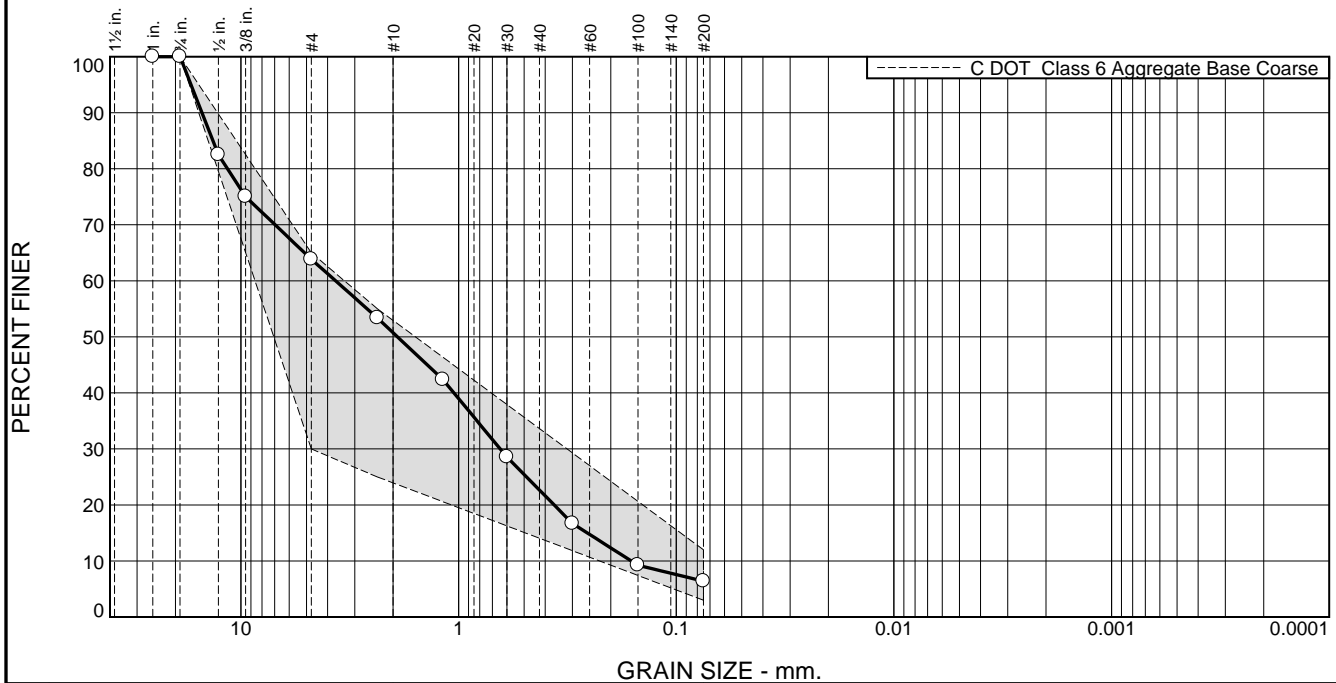
Client: Boulder County Parks & Open Space

Project: Swede Lake

Project No: 110480

Figure

Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0.0	49.3	28.0	16.3	6.4	

TEST RESULTS (AASHTO T 27)			
Opening Size	Percent Finer	Spec.* (Percent)	Pass? (X=Fail)
1	100.0		
3/4	100.0	100.0	
1/2	82.5		
3/8	75.0		
#4	63.8	30.0 - 65.0	
#8	53.4	25.0 - 55.0	
#16	42.4		
#30	28.6		
#50	16.7		
#100	9.2		
#200	6.4	3.0 - 12.0	

* C DOT Class 6 Aggregate Base Coarse

Material Description

Class 6

Atterberg Limits (ASTM D 4318)

PL= LL= PI=

Classification

USCS (D 2487)= AASHTO (M 145)=

Coefficients

D₉₀= 15.1056 D₈₅= 13.4512 D₆₀= 3.6740
D₅₀= 1.9090 D₃₀= 0.6439 D₁₅= 0.2562
D₁₀= 0.1609 C_u= 22.84 C_c= 0.70

Remarks

Date Received: 2/09/18

Date Tested: 2/14/2018

Tested By: KG

Checked By: KG

Title:

Source of Sample: Class 6
Sample Number: 1

Date Sampled: 2/09/18

ENGINEERING ANALYTICS, INC.

Client: Boulder County Parks & Open Space

Project: Swede Lake

Project No: 110480

Figure

REPORT OF CONCRETE COMPRESSIVE STRENGTH TESTS



PROJECT: Swede Lake
 JOB NO.: 110480
 PLACEMENT DATE: 10/18/2017
 CLIENT: Boulder County (BCPOS)
 CONTRACTOR: CAP Excavation

SUPPLIER: Bestway
 MIX CODE: 45VND01E4G
 SPECIFIED STRENGTH: 4,500 psi
 TESTED BY: DCH

	CYLINDER NUMBER	SLUMP (INCH)	AIR (%)	AIR TEMP (°F)	CONCRETE TEMP (°F)	WATER ADDED (GAL)	DATE TESTED	TEST AGE (DAYS)	MAX APPLIED LOAD (LBS)	COMPRESSIVE STRENGTH (PSI)	TYPE OF FAILURE	PLACEMENT LOCATION
BATCH # 20051938	1-1 A	3.50	6.0	87	77	10	10/26/17	7	49,820	3,965	5	Primary outlet, bottom 6", base of outlet structure
TRUCK # 1303	1-1 B						11/16/17	28	56,490	4,495	3	
TIME 3:43 PM	1-1 C						11/16/17	28	56,760	4,517	3	
	1-1 D											
BATCH # 20051950		3.50	5.5	90	79	3 gal after						Primary outlet, bottom 6", base of outlet structure
TRUCK # 1504												
TIME 4:16 PM												
BATCH # 20051960	1-2 A	5.00	5.5	75	78	3 gal before	10/26/17	7	41,710	3,319	3	Bottom 6" of irrigation outlet
TRUCK # 0715	1-2 B						11/16/17	28	46,080	3,667	3	
TIME 4:39 PM	1-2 C						11/16/17	28	47,220	3,757	3	
	1-2 D											
BATCH #												
TRUCK #												
TIME												

TYPE OF FAILURE

4-inch Diameter Cylinders Unless Noted Otherwise

Remarks:



1
CONE



2
SPLIT
CONE



3
SHEAR
CONE



4
SHEAR



5
SPLIT

All samples prepared and tested in accordance with the following ASTM standards: Sampling C172; Curing C31; Slump C143; Air C231; Temperature C1064; Compression C39

REPORT OF CONCRETE COMPRESSIVE STRENGTH TESTS



PROJECT: Swede Lake
 JOB NO.: 110480
 PLACEMENT DATE: 10/18/2017
 CLIENT: Boulder County (BCPOS)
 CONTRACTOR: CAP Excavation

SUPPLIER: Bestway
 MIX CODE: 45VND01E4G
 SPECIFIED STRENGTH: 4,500 psi
 TESTED BY: DCH

	CYLINDER NUMBER	SLUMP (INCH)	AIR (%)	AIR TEMP (°F)	CONCRETE TEMP (°F)	WATER ADDED (GAL)	DATE TESTED	TEST AGE (DAYS)	MAX APPLIED LOAD (LBS)	COMPRESSIVE STRENGTH (PSI)	TYPE OF FAILURE	PLACEMENT LOCATION
BATCH # 20057120 TRUCK # 613 TIME 2:45 PM 3:05 PM			4.0	55	76	11 before						Primary outlet pipe encasement
		4.00	5.3		76	12						
BATCH # 20057141 TRUCK # 1313 TIME 3:25 PM	2-1 A 2-1 B 2-1 C 2-1 D	4.25	6.0	55	70	10 before	11/10/17 12/4/18 12/4/18	7 28 28	45,680 57,990 60,530	3,634 4,615 4,817	3 3 3	
BATCH # 20057154 TRUCK # 714 TIME 3:40 PM		3.25	5.0	58	71							
BATCH # 20057169 TRUCK # 1717 TIME 4:30 PM	2-2 A 2-2 B 2-2 C 2-2 D	3.50	3.5 5.6	55	67		11/10/17 12/4/18 12/4/18	7 28 28	44,710 58,460 55,750	3,558 4,652 4,436	3 3 3	Farmer's irrigation outlet

TYPE OF FAILURE

4-inch Diameter Cylinders Unless Noted Otherwise

Remarks:



1
CONE



2
SPLIT
CONE



3
SHEAR
CONE



4
SHEAR



5
SPLIT

All samples prepared and tested in accordance with the following ASTM standards: Sampling C172; Curing C31; Slump C143; Air C231; Temperature C1064; Compression C39

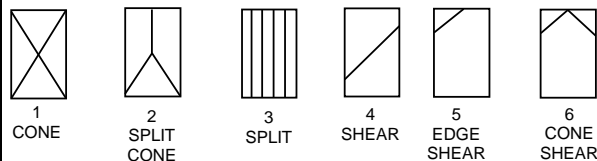
REPORT OF CONCRETE COMPRESSIVE STRENGTH TESTS



PROJECT: Swede Lake
 JOB NO.: 110480
 PLACEMENT DATE: 11/20/2017
 CLIENT: Boulder County
 CONTRACTOR: CAP

SUPPLIER: Martin Marietta
 MIX CODE: CD4995
 SPECIFIED STRENGTH: 4,500 psi
 TESTED BY: EAH

	CYLINDER NUMBER	SLUMP (INCH)	AIR (%)	AIR TEMP (°F)	CONCRETE TEMP (°F)	WATER ADDED (GAL)	DATE TESTED	TEST AGE (DAYS)	MAX APPLIED LOAD (LBS)	COMPRESSIVE STRENGTH (PSI)	TYPE OF FAILURE	PLACEMENT LOCATION
BATCH # 46332331	3-1 A	5.00	5.5	67	71	0	11/27/17	7	45,680	3,635	3	Grade control beam spillway
TRUCK # 8906	3-1 B						12/18/17	28	62,180	4,948	3	
TIME 2:15 PM	3-1 C						12/18/17	28	56,620	4,505	3	
	3-1 D											
BATCH # 35054319	3-2 A	4.00	6.0	67	78	0	11/27/17	7	47,590	3,787	3	NE & SE wingwall foundations at approx. STA 9+00
TRUCK # 1619	3-2 B						12/18/17	28	61,570	4,900	3	
TIME 2:45 PM	3-2 C						12/18/17	28	66,780	5,314	3	
	3-2 D											
BATCH # _____												
TRUCK # _____												
TIME _____												
BATCH # _____												
TRUCK # _____												
TIME _____												



TYPE OF FAILURE

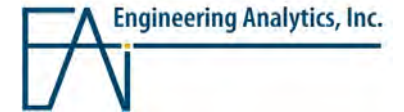
4-inch Diameter Cylinders Unless Noted Otherwise

All samples prepared and tested in accordance with the following ASTM standards: Sampling C172; Curing C31; Slump C143; Air C231; Temperature C1064; Compression C39

Remarks:

Initial check test had 5" slump. Retested in middle 1/3 of land out of pump house and got a 4" slump result.

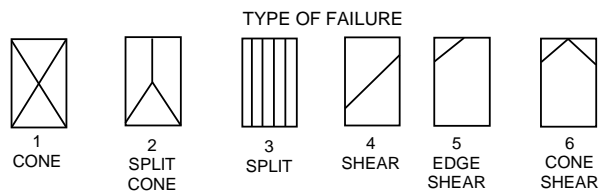
REPORT OF CONCRETE COMPRESSIVE STRENGTH TESTS



PROJECT: Swede Lake
 JOB NO.: 110480
 PLACEMENT DATE: 11/20/2017
 CLIENT: Boulder County
 CONTRACTOR: CAP

SUPPLIER: Martin Marietta
 MIX CODE: CD4995
 SPECIFIED STRENGTH: 4,500 psi
 TESTED BY: EAH

	CYLINDER NUMBER	SLUMP (INCH)	AIR (%)	AIR TEMP (°F)	CONCRETE TEMP (°F)	WATER ADDED (GAL)	DATE TESTED	TEST AGE (DAYS)	MAX APPLIED LOAD (LBS)	COMPRESSIVE STRENGTH (PSI)	TYPE OF FAILURE	PLACEMENT LOCATION
BATCH # 46332499	4-1 A						12/4/17	7	28,606	2,275	3	Spillway wall/drop structure at STA 4+00. *
TRUCK # 1517	4-1 B						12/26/17	28	40,450	3,219	3	
TIME 10:10 AM	4-1 C		8.7	59	70		12/26/17	28	41,090	3,270	3	
	4-1 D						1/22/18	63	42,710	3,399	3	
	4-1 E						12/7/17	10	33,890	2,697	3	
BATCH # 4.63E+08	4-2 A						12/4/17	7	38,600	3,072	3	Vault structure at STA 4+00
TRUCK # 0309	4-2 B						12/26/17	28	48,480	3,858	5	
	4-2 C						12/26/17	28	48,330	3,846	5	
TIME 10:30 AM	4-2 D	4.50	7.4	59	68	10	1/22/18	63	54,490	4,336	3	
	4-2 E						12/7/17	10	40,780	3,245	3	
	4-2 F											
BATCH # 46332505												**
TRUCK # 1701		5.00	7.4	59	70							
TIME 11:00 AM												
BATCH # 46332517												
TRUCK # 1741						6						
TIME 12:50 PM												



4-inch Diameter Cylinders Unless Noted Otherwise

All samples prepared and tested in accordance with the following ASTM standards: Sampling C172; Curing C31; Slump C143; Air C231; Temperature C1064; Compression C39

Remarks:

*Rejected due to high air content

**Visual check only

REPORT OF CONCRETE COMPRESSIVE STRENGTH TESTS



PROJECT: Swede Lake
 JOB NO.: 110480
 PLACEMENT DATE: 11/20/2017
 CLIENT: Boulder County
 CONTRACTOR: CAP

SUPPLIER: Martin Marietta
 MIX CODE: CD4995
 SPECIFIED STRENGTH: 4,500 psi
 TESTED BY: EAH

	CYLINDER NUMBER	SLUMP (INCH)	AIR (%)	AIR TEMP (°F)	CONCRETE TEMP (°F)	WATER ADDED (GAL)	DATE TESTED	TEST AGE (DAYS)	MAX APPLIED LOAD (LBS)	COMPRESSIVE STRENGTH (PSI)	TYPE OF FAILURE	PLACEMENT LOCATION
BATCH # 35054767 TRUCK # 0703 TIME 1:40 PM	5-1 A 5-1 B 5-1 C 5-1 D 5-1 E 5-1 F	3.75	5.5	47	73		12/12/17 1/3/18 1/3/18	7 28 28	56,300 70,090 72,460	4,480 5,572 5,764	3 3 3	Wing walls and outlet structure at STA 9+00
BATCH # 35054768 TRUCK # 8620 TIME 2:05 PM		3.00	5.2	46	70							
BATCH # 35054773 TRUCK # 8601 TIME 2:25 PM		4.00	5.9	44	70	8						
BATCH # 35054777 TRUCK # 8687 TIME 3:00 PM		3.50	5	44	71	8						Measuring weirs and headwall at STA 9+00; pipe encasement at STA 4+00; *



1
CONE



2
SPLIT
CONE



3
SPLIT



4
SHEAR



5
EDGE
SHEAR



6
CONE
SHEAR

TYPE OF FAILURE

4-inch Diameter Cylinders Unless Noted Otherwise

All samples prepared and tested in accordance with the following ASTM standards: Sampling C172; Curing C31; Slump C143; Air C231; Temperature C1064; Compression C39

Remarks:

*8 gallons were added after initial test.

REPORT OF CONCRETE COMPRESSIVE STRENGTH TESTS



PROJECT: Swede Lake
 JOB NO.: 110480
 PLACEMENT DATE: 11/20/2017
 CLIENT: Boulder County
 CONTRACTOR: CAP

SUPPLIER: Martin Marietta
 MIX CODE: CD4995
 SPECIFIED STRENGTH: 4,500 psi
 TESTED BY: EAH

	CYLINDER NUMBER	SLUMP (INCH)	AIR (%)	AIR TEMP (°F)	CONCRETE TEMP (°F)	WATER ADDED (GAL)	DATE TESTED	TEST AGE (DAYS)	MAX APPLIED LOAD (LBS)	COMPRESSIVE STRENGTH (PSI)	TYPE OF FAILURE	PLACEMENT LOCATION
BATCH # 35054779	5-2 A						12/12/17	7	59,300	4,719	3	Measuring weirs and headwall at STA 9+00; pipe encasement at STA 4+00
TRUCK # 8671	5-2 B						1/3/18	28	75,440	6,003	3	
TIME 3:20 PM	5-2 C	3.25	5.6	44	72		1/3/18	28	74,520	5,928	3	
	5-2 D											
	5-2 E											
BATCH #												
TRUCK #												
TIME												
BATCH #												
TRUCK #												
TIME												
BATCH #												
TRUCK #												
TIME												



1
CONE



2
SPLIT
CONE



3
SPLIT



4
SHEAR



5
EDGE
SHEAR



6
CONE
SHEAR

TYPE OF FAILURE

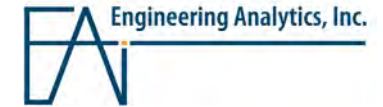
4-inch Diameter Cylinders Unless Noted Otherwise

All samples prepared and tested in accordance with the following ASTM standards: Sampling C172; Curing C31; Slump C143; Air C231; Temperature C1064; Compression C39

Remarks:

Observed use of concrete vibrator during/after placement.

REPORT OF CONCRETE COMPRESSIVE STRENGTH TESTS



PROJECT: Swede Lake Dam
 JOB NO.: 110480
 PLACEMENT DATE: 12/12/2017
 CLIENT: BCPOS
 CONTRACTOR: CAP Excavation

SUPPLIER: Best Way Concrete
 MIX CODE: 45VN01E4G
 SPECIFIED STRENGTH: 4,500 psi
 TESTED BY: Tyler Davis

	CYLINDER NUMBER	SLUMP (INCH)	AIR (%)	AIR TEMP (°F)	CONCRETE TEMP (°F)	WATER ADDED (GAL)	DATE TESTED	TEST AGE (DAYS)	MAX APPLIED LOAD (LBS)	COMPRESSIVE STRENGTH (PSI)	TYPE OF FAILURE	PLACEMENT LOCATION	REMARKS
BATCH # <u>20067737</u>	6-1 A						12/19/17	7	52,850	4,206	3	Outlet Structure. Outlet pipe tie in encasements to structure	Poured ~3yards
TRUCK # <u>1107</u>	6-1 B						1/9/18	28	60,520	4,816	3		
TIME <u>12:45 PM</u>	6-1 C	3.25	6.3	58	80	0	1/9/18	28	65,100	5,181	3		
	6-1 D												
	6-1 E												
BATCH # _____													
TRUCK # _____													
TIME _____													
BATCH # _____													
TRUCK # _____													
TIME _____													
BATCH # _____													
TRUCK # _____													
TIME _____													

TYPE OF FAILURE



1
CONE



2
SPLIT
CONE



3
SPLIT



4
SHEAR



5
EDGE SHEAR



6
CONE
SHEAR

4-inch Diameter Cylinders Unless Noted Otherwise

All samples prepared and tested in accordance with the following ASTM standards:
 Sampling C172; Curing C31; Slump C143; Air C231; Temperature C1064; Compression C39

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Clint Brown

TESTED BY: Walter Kramb

NOTES: 1) First lift of fill

2) Compacted subgrade

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
1	9/22/2017	Outlet breach, station 0+50	5118.5	18.4	128.0	108.1	100+	95	2
2	9/22/2017	Outlet breach, station 0+20	5118	16.4	129.5	111.2	100+	95	2
3	9/22/2017	Outlet breach, station 0+20	5119.0	19.2	123.4	103.5	97	95	2
4	9/22/2017	Outlet breach, station 0+80	5119.0	19.4	121.9	102.1	96	95	2
5	9/22/2017	Outlet breach, station 0+40	5119.5	19.3	122.8	102.6	97	95	2
6	9/22/2017	Outlet breach, station 0+50	5120.0	17.9	125.3	106.2	100	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
7	9/27/2017	Outlet breach, sta 0+40 right side of fill	5121.5	18.1	127.7	108.2	100+	95	1
8	9/27/2017	Outlet breach sta 0+50 right side of fill	5121.0	17.6	128.9	109.7	100+	95	1
9	9/27/2017	Outlet breach sta 0+40 right side of fill	5120.5	15.3	126.2	109.5	100+	95	1

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
10	10/26/2017	STA 1+25 (Ref. sheet 6)	5132.0	17.9	124.4	105.6	99	95	2
11	10/26/2017	STA 2+25	5132.0	19.2	120.9	101.4	95	95	2
12	10/26/2017	STA 1+00	5132.5	18.3	127.1	107.4	100+	95	2
13	10/26/2017	STA 1+50	5133.0	18.4	104.4	123.6	98	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
14	10/27/2017	STA 2+50 (Ref.sheet 6)	5133.0	17.5	129.1	109.9	100+	95	2
15	10/27/2017	STA 1+70 (Ref. sheet 6)	5134.0	17.9	128.1	108.6	100+	95	2
16	10/27/2017	STA 2+05 (Ref. sheet 6)	5134.5	19.9	122.4	102.1	96	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
17	11/1/2017	STA 5+25 (Ref. sheet 6)	5125.5	19.6	127.8	107.1	100+	95	2
18	11/1/2017	STA 6+50 (Ref. sheet 6)	5126	18.0	127.9	108.0	100+	95	2
19	11/1/2017	STA 7+50 (Ref. sheet 6)	5126	18.3	127.2	107.5	100+	95	2
20	11/1/2017	STA 7+20 (Ref. sheet 6)	5125.5	17.0	126.5	108.1	100+	95	2
21	11/1/2017	STA 6+50 (Ref. sheet 6)	5126.5	18.3	125.6	106.1	100	95	2
22	11/1/2017	STA 4+80 (Ref. sheet 6)	5126.0	19.4	124.9	104.7	98	95	2
23	11/1/2017	STA 7+30 (Ref. sheet 6)	5126.5	18.9	124.0	104.3	98	95	2
24	11/1/2017	STA 5+25 (Ref. sheet 6)	5127.0	18.0	125.1	106.0	100	95	2
25	11/1/2017	STA 6+30 (Ref. sheet 6)	5127	20.0	126.0	105.0	99	95	2
26	11/1/2017	STA 7+60 (Ref. sheet 6)	5127.5	17.5	127.3	108.7	100+	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
27	11/1/2017	STA 4+70 (Ref. sheet 6)	5128.0	17.8	125.5	106.5	100+	95	2
28	11/1/2017	STA 6+55 (Ref. sheet 6)	5128	18.9	125.9	105.9	100	95	2
29	11/1/2017	STA 7+75 (Ref. sheet 6)	5128.58	18.3	127.9	108.1	100+	95	2
30	11/1/2017	STA 5+10 (Ref. sheet 6)	5129	18.5	127.1	107.3	100+	95	2
31	11/1/2017	STA 6+40 (Ref. sheet 6)	5129	20.6	125.4	104.0	98	95	2
32	11/1/2017	STA 7+40 (Ref. sheet 6)	5129.5	17.4	125.7	107.1	100+	95	2
33	11/1/2017	STA 5+20 (Ref. sheet 6)	5130	17.7	125.7	106.8	100+	95	2
34	11/1/2017	STA 5+00 (Ref. sheet 6)	5130.5	18.4	124.6	105.3	99	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
35	11/2/2017	STA 5+60 (Ref.sheet 6)	5131.5	18.1	126.7	107.3	100+	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
36	11/2/2017	Embankment STA 7+50	5130.5	18.5	125.7	106.1	99	95	2
37	11/3/2017	Embankment STA 6+50	5131.5	23.4	124.0	101.5	95	95	2
37R	11/3/2017	Embankment STA 6+50 move 10'	5131.5	20.5	125.9	104.4	98	95	2
38	11/3/2017	Embankment STA 5+00	5131.4	20.4	125.9	104.5	98	95	2
39	11/3/2017	SKIP							
40	11/3/2017	Embankment STA 4+50	3132.0	18.1	126.2	106.8	100	95	2
41	11/3/2017	Embankment STA 7+00	3133.5	22.9	120.9	98.4	92	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4
2	106.4	18.6

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County Parks & Open Space

CONTRACTOR: CAP Excavating & Construction

ENGINEER: Clint Brown

TESTED BY: Dylan Hoehn

NOTES: See dwg 11 for station#

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
42	11/5/2017	STA 7+00 Retest of test No. 41 (Ref. sheet 6)	5132	17.9	124.4	105.5	99	95	2
43	11/5/2017	STA 6+50	5133	17.9	126.0	106.9	100+	95	2
44	11/5/2017	STA 5+70	5133	17.8	125.8	106.8	100+	95	2
45	11/5/2017	STA 4+90, Need to Retest	5133.5	23.8	122.6	99.0	92	95	2
46	11/5/2017	STA 6+10, Need to Retest	5133.5	25.9	119.0	94.5	89	95	2
47	11/5/2017	STA 9+75	5124.5	17.2	125.2	106.8	100+	95	2
48	11/5/2017	STA 10+30	5124.5	18.1	120.1	101.7	95	95	2
49	11/5/2017	STA 11+50	5124.5	18.9	121.2	101.9	95	95	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES: Test No. 50 and 51 will be retested at a later date

*Indicates failure to meet moisture specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
*50	11/9/2017	STA 9+60 (Ref. sheet 6)	5125.5	14.60%	123.8	108.0	100+%	95%	2
*51	11/9/2017	STA 10+85 (Ref. sheet 6)	5125.5	14.90%	123.1	107.1	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
52	11/10/2017	Retest of No. 50, STA 9+60 (Ref. sheet 6)	5125.5	17.00%	126.7	108.3	100+%	95%	2
53	11/10/2017	Retest of No. 51, STA 10+85 (Ref. sheet 6)	5125.5	17.40%	126.1	107.4	100+%	95%	2
54	11/10/2017	STA 12+90	5125.5	18.30%	126.8	107.2	100+%	95%	2
55	11/10/2017	STA 14+00	5128.5	16.70%	125.7	107.7	100+%	95%	2
56	11/10/2017	STA 15+25	5130.5	19.20%	116.2	97.5	98%	95%	4
57	11/10/2017	STA 12+00	5125.5	17.70%	126.4	107.4	100+%	95%	2
58	11/10/2017	STA 9+75	5126.3	21.30%	121.4	100.1	100+%	95%	4
59	11/10/2017	STA 13+53	5127.0	20.60%	121.2	100.5	100+%	95%	4
60	11/10/2017	STA 14+50	5128.3	18.20%	126.9	107.4	100+%	95%	2
61	11/10/2017	STA 15+25	5131.3	20.30%	120.8	100.4	100+%	95%	4

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet moisture specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
62	11/10/2017	STA 11+00 (Ref. sheet 6)	5126.5	22.30%	121.2	99.1	99%	95%	4
63	11/10/2017	STA 12+30	5126.5	17.50%	126.9	108.0	100+%	95%	2
**64	11/10/2017	STA 13+70	5128.0	22.60%	123.8	101.0	100+%	95%	4
65	11/10/2017	STA 14+90	5130.3	20.60%	127.2	105.5	99%	95%	4

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet moisture specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
66	11/11/2017	STA 10+30 (Ref. sheet 6)	5127.0	16.60%	118.2	101.4	95%	95%	2
67	11/11/2017	STA 11+60 (Ref. sheet 6)	5127.3	16.70%	126.0	108.0	100+%	95%	2
68	11/11/2017	STA 13+20 (Ref. sheet 6)	5128.8	16.80%	125.8	107.7	100+%	95%	2
69	11/11/2017	STA 14+40 (Ref. sheet 6)	5131.0	21.10%	121.2	100.1	100+%	95%	4
70	11/11/2017	STA 15+30 (Ref. sheet 6)	5132.0	20.00%	121.1	100.9	100+%	95%	4
71	11/11/2017	STA 9+65 (Ref. sheet 6)	5127.5	17.00%	126.2	107.9	100+%	95%	2
72	11/11/2017	STA 11+10 (Ref. sheet 6)	5128.0	16.80%	124.6	106.7	100+%	95%	2
**73	11/11/2017	STA 12+30 (Ref. sheet 6)	5128.0	22.90%	124.1	101.0	100+%	95%	4
74	11/11/2017	STA 13+55 (Ref. sheet 6)	5129.5	21.40%	121.5	100.1	100+%	95%	4
75	11/11/2017	STA 14+50 (Ref. sheet 6)	5132	21.70%	122.1	100.3	100+%	95%	4

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet moisture specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
76	11/11/2017	STA 10+50 (Ref. sheet 6)	5128.7	17.80%	125.9	106.9	100+%	95%	2
77	11/11/2017	STA 12+20 (Ref. sheet 6)	5128.7	22.20%	123.4	101.0	100+%	95%	4
78	11/11/2017	STA 13+40 (Ref. sheet 6)	5130.3	22.20%	123.8	101.3	100+%	95%	4
79	11/11/2017	STA 14+50 (Ref. sheet 6)	5133.0	21.80%	123.1	101.1	100+%	95%	4
80	11/11/2017	STA 15+30 (Ref. sheet 6)	5133.7	20.10%	122.5	102.0	100+%	95%	4
81	11/11/2017	STA 10+00 (Ref. sheet 6)	5129.5	21.40%	122.7	101.1	100+%	95%	4
**82	11/11/2017	STA 11+30 (Ref. sheet 6)	5129.5	22.50%	123.2	100.6	100+%	95%	4
83	11/11/2017	STA 10+85 (Ref. sheet 6)	5130.5	21.30%	121.4	100.1	100+%	95%	4
84	11/11/2017	STA 12+05 (Ref. sheet 6)	5130.0	20.60%	120.2	99.7	100%	95%	4
85	11/11/2017	STA 13+05 (Ref. sheet 6)	5131.0	18.70%	124.9	105.2	99%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
86	11/13/2017	STA 10+15 (Ref. sheet 6)	5131.0	20.00%	127.4	106.2	100%	95%	2
87	11/13/2017	STA 11+10 (Ref. sheet 6)	5131.0	18.60%	126.9	107.0	100+%	95%	2
88	11/13/2017	STA 12+05 (Ref. sheet 6)	5131.0	18.40%	126.5	106.8	100+%	95%	2
89	11/13/2017	STA 13+25 (Ref. sheet 6)	5131.5	16.70%	125.1	107.2	100+%	95%	2
90	11/13/2017	STA 14+20 (Ref. sheet 6)	5133.5	16.60%	125.1	107.3	100+%	95%	2
91	11/13/2017	STA 15+15 (Ref. sheet 6)	5134.3	17.10%	125.4	107.1	100+%	95%	2
92	11/13/2017	STA 10+05 (Ref. sheet 6)	5131.5	18.00%	122.8	104.1	98%	95%	2
93	11/13/2017	STA 11+40 (Ref. sheet 6)	5131.5	20.70%	121.2	100.4	100+%	95%	4
94	11/13/2017	STA 12+60 (Ref. sheet 6)	5132.0	19.00%	126.7	106.5	100+%	95%	2
95	11/13/2017	STA 13+95 (Ref. sheet 6)	5132.5	19.60%	127.5	106.6	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
96	11/13/2017	STA 9+90 (Ref. sheet 6)	5132.0	18.90%	122.6	103.1	97%	95%	2
97	11/14/2017	STA 11+15 (Ref. sheet 6)	5132.7	21.80%	121.9	100.1	100+%	95%	4
98	11/14/2017	STA 12+05 (Ref. sheet 6)	5133.0	19.00%	126.7	106.5	100+%	95%	2
99	11/14/2017	STA 13+30 (Ref. sheet 6)	5134.0	22.10%	123.3	101.0	100+%	95%	4
100	11/14/2017	STA 14+00 (Ref. sheet 6)	5135.0	21.00%	121.8	100.7	100+%	95%	4
101	11/14/2017	STA 15+20 (Ref. sheet 6)	5132.7	17.70%	125.9	107.0	100+%	95%	2
102	11/14/2017	STA 10+15 (Ref. sheet 6)	5133.0	16.90%	125.6	107.4	100+%	95%	2
103	11/14/2017	STA 11+40 (Ref. sheet 6)	5133.3	17.30%	125.5	107.0	100+%	95%	2
104	11/14/2017	STA 12+50 (Ref. sheet 6)	5133.5	17.10%	125.9	107.5	100+%	95%	2
105	11/14/2017	STA 13+80 (Ref. sheet 6)	5135.0	18.40%	127.2	107.4	97%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
106	11/14/2017	STA 15+00 (Ref. sheet 6)	5135.0	21.30%	117.7	97.0	97%	95%	4
107	11/15/2017	STA 10+50 (Ref. sheet 6)	5133.3	16.70%	125.3	107.4	100+%	95%	2
108	11/15/2017	STA 12+25 (Ref. sheet 6)	5134.0	17.40%	126.3	107.6	100+%	95%	2
109	11/15/2017	STA 14+50 (Ref. sheet 6)	5135.0	18.00%	125.9	106.7	100+%	95%	2
110	11/15/2017	STA 10+00 (Ref. sheet 6)	5133.8	19.40%	128.1	107.3	100+%	95%	2
111	11/15/2017	STA 12+20 (Ref. sheet 6)	5134.5	18.40%	123.8	104.6	98%	95%	2
112	11/15/2017	STA 10+25 (Ref. sheet 6)	5134.5	18.20%	127.5	107.9	100+%	95%	2
113	11/15/2017	STA 11+25 (Ref. sheet 6)	5134.5	17.70%	127.1	108.0	100+%	95%	2
114	11/15/2017	STA 13+00 (Ref. sheet 6)	5134.0	18.80%	127.0	106.9	100+%	95%	2
115	11/15/2017	STA 14+15 (Ref. sheet 6)	5135.3	17.40%	126.6	107.8	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet moisture specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
*116	11/15/2017	STA 10+30 (Ref. sheet 6)	5135.0	16.20%	125.6	108.1	100+%	95%	2
117	11/15/2017	STA 12+00 (Ref. sheet 6)	5135.0	19.00%	125.7	105.6	99%	95%	2
118	11/15/2017	STA 13+00 (Ref. sheet 6)	5135.0	17.00%	125.9	107.6	100+%	95%	2
119	11/15/2017	STA 14+00 (Ref. sheet 6)	5135.7	22.10%	122.2	100.1	100+%	95%	4
120	11/15/2017	STA 10+30 (Ref. sheet 6) (Retest of Test No. 116)	5135.0	18.20%	126.4	106.9	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet moisture specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
121	11/16/2017	STA 10+50 (Ref. sheet 6)	5136.0	20.50%	127.9	106.1	100%	95%	2
122	11/16/2017	STA 11+40 (Ref. sheet 6)	5136.0	18.80%	125.9	106.0	100%	95%	2
123	11/16/2017	STA 12+50 (Ref. sheet 6)	5136.0	20.50%	124.6	103.4	97%	95%	2
124	11/16/2017	STA 13+50 (Ref. sheet 6)	5136.0	17.40%	126.0	107.3	100+%	95%	2
125	11/16/2017	STA 14+50 (Ref. sheet 6)	5136.0	17.60%	125.8	107.0	100+%	95%	2
126	11/16/2017	STA 15+25 (Ref. sheet 6)	5136.0	16.80%	126.1	108.0	100+%	95%	2
**127	11/16/2017	STA 7+50 (Ref. sheet 6)	5133.5	23.20%	121.0	98.2	98%	95%	4
**128	11/16/2017	STA 6+10 (Ref. sheet 6) (Retest of Test No. 46)	5133.5	20.70%	126.0	104.4	98%	95%	2
129	11/16/2017	STA 4+90 (Ref. sheet 6) (Retest of Test No. 46)	5133.5	19.40%	124.8	104.5	98%	95%	2
130	11/16/2017	STA 5+10 (Ref. sheet 6)	5134.5	19.50%	124.3	104.0	98%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
131	11/16/2017	STA 6+25 (Ref. sheet 6)	5134.5	22.10%	121.1	99.2	99%	95%	4
132	11/16/2017	STA 7+40 (Ref. sheet 6)	5134.5	16.80%	125.4	107.4	100+%	95%	2
133	11/16/2017	STA 5+75 (Ref. sheet 6)	5135.3	20.00%	122.6	102.2	100+%	95%	4
134	11/16/2017	STA 4+85 (Ref. sheet 6)	5135.3	18.90%	115.6	97.2	97%	95%	4

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
135	11/17/2017	STA 5+00 (Ref. sheet 6)	5136.0	17.80%	125.1	106.2	100%	95%	2
136	11/17/2017	STA 6+15 (Ref. sheet 6)	5136.0	17.70%	126.3	107.3	100+%	95%	2
137	11/17/2017	STA 7+00 (Ref. sheet 6)	5136.0	18.00%	127.3	107.9	100+%	95%	2
138	11/17/2017	STA 7+60 (Ref. sheet 6)	5135.5	19.50%	126.0	105.4	99%	95%	2
139	11/17/2017	STA 2+50 (Ref. sheet 6)	5135.3	21.00%	121.1	100.1	100+%	95%	4
140	11/17/2017	STA 1+50 (Ref. sheet 6)	5135.5	19.00%	125.4	105.4	99%	95%	2
141	11/17/2017	STA 1+40 (Ref. sheet 6)	5136.0	18.10%	127.1	107.6	100+%	95%	2
142	11/17/2017	STA 2+75 (Ref. sheet 6)	5136.0	18.00%	127.2	107.8	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:

*Indicates failure to meet specifications

**Indicates approval by Engineer

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
143	11/20/2017	STA 4+35 (Ref. sheet 6)	5126.0	20.50%	127.0	105.4	99%	95%	2
144	11/20/2017	STA 4+40 (Ref. sheet 6)	5128.0	19.40%	127.6	106.9	100+%	95%	2
145	11/20/2017	STA 4+30 (Ref. sheet 6)	5130.0	19.80%	124.8	104.2	98%	95%	2
146	11/20/2017	STA 4+40 (Ref. sheet 6)	5132.0	20.00%	127.9	106.6	100+%	95%	2
147	11/20/2017	STA 9+20 (Ref. sheet 6)	5126.5	19.20%	126.2	105.9	100%	95%	2
148	11/20/2017	STA 9+35 (Ref. sheet 6)	5127.5	19.60%	128.2	107.2	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: Emmett Hite

NOTES: Test 154 - Location received extra passes with sheep's foot compactor after testing. Test 152 failed to meet expectations. Its retest is shown in Test 158.

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
149	12/11/2017	Irrigation structure backfill, STA 0+50 (Ref. sheet 17), west side of pipe	5123.0	14.0%	121.0	106.1	100%	95%	2
150	12/11/2017	Irrigation structure backfill, STA 1+00 (Ref. sheet 17), west side of pipe	5123.0	19.5%	121.9	102.0	96%	95%	2
151	12/11/2017	Irrigation structure backfill, STA 1+05 (Ref. sheet 17), east side of pipe	5123.0	18.1%	123.8	104.8	99%	95%	2
152	12/11/2017	Irrigation structure backfill, STA 0+50 (Ref. sheet 17), east side of pipe	5123.0	15.4%	122.9	106.5	100+%	95%	2
153	12/11/2017	Irrigation structure backfill, STA 0+80 (Ref. sheet 17), west side of pipe	5123.5	18.7%	124.9	105.2	99%	95%	2
154	12/11/2017	Irrigation structure backfill, STA 0+80 (Ref. sheet 17), east side of pipe	5123.5	18.3%	119.6	101.1	95%	95%	2
155	12/11/2017	Irrigation structure backfill, STA 1+10 (Ref. sheet 17), west side of pipe	5124.5	16.7%	125.1	107.2	100+%	95%	2
156	12/11/2017	Irrigation structure backfill, STA 1+12 (Ref. sheet 17), east side of pipe	5124.5	18.0%	123.1	104.3	98%	95%	2
157	12/11/2017	Irrigation structure backfill, STA 0+50 (Ref. sheet 17), west side of pipe (Retest of Test 149)	5123.0	16.9%	125.1	107.0	100+%	95%	2
158	12/11/2017	Irrigation structure backfill, STA 0+50 (Ref. sheet 17), east side of pipe (Retest of Test 152)	5123.0	17.0%	125.1	106.9	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: Emmett Hite & Tyler Davis

NOTES: 8" Depth

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
159	12/12/2017	Irrigation structure backfill, outlet towers STA 0+40 (Ref. sheet 17), west side of pipe	~5142.0	17.9%	125.2	106.2	100%	95%	2
160	12/12/2017	Irrigation structure backfill, outlet towers STA 0+40 (Ref. sheet 17), east side of pipe	5124.0	20.4%	123.0	102.2	96%	95%	2
161	12/12/2017	Irrigation structure backfill, outlet towers (Ref. sheet 17), east side of pipe	5125.0	18.7%	130.8	110.2	100+%	95%	2
162	12/13/2017	Irrigation structure backfill, outlet towers STA 0+60 (Ref. sheet 17), west side of pipe	5126.3	18.4%	130.2	110.0	100+%	95%	2
163	12/13/2017	Irrigation structure backfill, outlet towers STA 0+50 (Ref. sheet 17), east side of pipe	5127.0	16.6%	125.8	107.9	100+%	95%	2
164	12/13/2017	Irrigation structure backfill, outlet towers STA 0+40 (Ref. sheet 17), west side of pipe	5127.0	16.7%	125.3	107.4	100+%	95%	2
165	12/13/2017	Irrigation structure backfill, outlet towers STA 0+60 (Ref. sheet 17), east side of pipe	5127.7	17.2%	126.2	107.7	100+%	95%	2
166	12/13/2017	Irrigation structure backfill, outlet towers STA 0+50 (Ref. sheet 17), west side of pipe	5132.0	20.1%	129.1	107.5	100+%	95%	2
167	12/13/2017	Irrigation structure backfill, outlet towers STA 0+60 (Ref. sheet 17), east side of pipe	5132.7	17.9%	128.5	109.0	100+%	95%	2
168	12/13/2017	Irrigation structure backfill, outlet towers STA 0+55 (Ref. sheet 17), west side of pipe	5133.3	18.3%	128.0	108.2	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: Emmett Hite

NOTES: Test 169 approved by engineer. Test 175 failed to meet specification. Its retest is shown at Test 176

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
169	12/14/2017	Spillway grade control beam backfill (Ref. sheet 14) STA -0+04 (South side of beam)	5131.5	23.3%	123.1	99.8	100%	95%	4
170	12/14/2017	Spillway grade control beam backfill (Ref. sheet 14) STA 0+04 (North side of beam)	5132.0	20.9%	122.4	101.2	100+%	95%	4
171	12/14/2017	Spillway grade control beam backfill (Ref. sheet 14) STA -0+05 (South side of beam)	5133.0	21.2%	121.4	100.2	100+%	95%	4
172	12/15/2017	Irrigation structure backfill (Ref. sheet 17) STA 0+55 (East side of pipe)	5134.5	20.3%	124.1	103.2	100+%	95%	4
173	12/15/2017	Irrigation structure backfill (Ref. sheet 17) STA 0+60 (West side of pipe)	5135.5	20.0%	123.5	102.9	100+%	95%	4
174	12/15/2017	Irrigation structure backfill (Ref. sheet 17) STA 0+65 (East side of pipe)	5136.0	21.6%	125.4	103.1	100+%	95%	4
175	12/18/2017	Outlet structure backfill (Ref. sheet 11) STA 0+30 (North side of pipe)	5122.0	16.7%	116.6	99.9	94%	95%	2
176	12/18/2017	Outlet structure backfill (Ref. sheet 11) STA 0+30 (North side of pipe) **Retest of Test 175**	5122.0	18.3%	121.3	102.5	96%	95%	2
177	12/18/2017	Outlet structure backfill (Ref. sheet 11) STA 0+50 (North side of pipe)	5123.5	16.8%	123.6	105.8	99%	95%	2
178	12/18/2017	Outlet structure backfill (Ref. sheet 11) STA 0+55 (South side of pipe)	5122.7	16.6%	126.7	108.7	100+%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
1	105.6	16.4%
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: Tyler Davis

NOTES: Approximate embankment STA 9+00 outlet pipe stationing noted for tests

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
189	12/20/2017	Outlet structure backfill, STA 0+50 (Ref. sheet 11) North of outlet structure	5134.5	18.4%	127.3	107.5	100+%	95%	2
190	12/20/2017	Outlet structure backfill, STA 0+45 (Ref. sheet 11) South of outlet structure	5134.5	19.7%	127.1	106.2	100%	95%	2
191	12/20/2017	Outlet structure backfill, STA 0+30 (Ref. sheet 11) At outlet structure	5134.5	18.4%	125.7	106.2	100%	95%	2
192	12/20/2017	Outlet structure backfill, STA 0+40 (Ref. sheet 11) South of outlet structure	5135.3	18.9%	127.1	106.9	100+%	95%	2
193	12/20/2017	Outlet structure backfill, STA 0+30 (Ref. sheet 11) At outlet structure	5135.3	19.5%	115.3	96.5	91%	95%	2
194	12/20/2017	Outlet structure backfill, STA 0+50 (Ref. sheet 11) North of outlet structure	5136.0	18.4%	128.6	108.6	102%	95%	2
195	12/20/2017	Outlet structure backfill, STA 0+30 (Ref. sheet 11) At outlet structure **Retest of 193**	5135.3	20.5%	122.1	101.3	95%	95%	2
196	12/20/2017	Outlet structure backfill, STA 0+50 (Ref. sheet 11) South of outlet structure	5136.0	20.4%	127.7	106.1	100%	95%	2

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
RD-1	110.8-113.4	

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: LCB

NOTES: Approximate embankment STA 9+00 outlet pipe stationing noted for tests

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
197	1/16/2018	MH-5 Toe drain	5120.5	10.7%	123.1	111.2	67%	65-75%	RD-1
198	1/17/2018	MH-5 Toe drain + 25'	5120.5	13.5%	125.8	110.8	65%	65-75%	RD-1

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
RD-1	110.8-113.4	

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES:	Approximate embankment STA 9+00 outlet pipe stationing noted for tests

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
199	1/25/2018	MH-2 Toe drain + 16' W	5124.3	9.9%	124.5	113.3	74%	65-75%	RD-1

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
RD-1	110.8-113.4	

PROJECT: Swede Lake
JOB NO: 110480

CLIENT: Boulder County
CONTRACTOR: CAP
ENGINEER: Engineering Analytics, Inc.
TESTED BY: EAH

NOTES:	Approximate embankment STA 9+00 outlet pipe stationing noted for tests

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
200	2/8/2018	Toe drain, 120' S of MH-7 between MH-7 and MH-8	5126.0	10.0%	124.1	112.8	75%	65-75%	RD-1

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES: Approximate embankment STA 9+00 outlet pipe stationing noted for tests

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
201	2/17/2018	Toe drain, STA 10+10 (Ref sheet 6)	5129.0	17.1%	125.2	106.9	100+%	95%	3
202	2/17/2018	Toe drain, STA 9+35 (Ref sheet 6)	5129.0	18.9%	127.2	107.0	100+%	95%	3
203	2/17/2018	Toe drain, STA 11+70 (Ref sheet 6)	5129.0	17.8%	124.3	105.5	99%	95%	3
204	2/17/2018	Toe drain, STA 13+20 (Ref sheet 6)	5130.0	16.8%	126.1	108.0	100+%	95%	3
205	2/17/2018	Toe drain, STA 14+60 (Ref sheet 6)	5131.0	17.0%	125.0	106.8	100+%	95%	3
206	2/17/2018	Toe drain, STA 10+15 (Ref sheet 6)	5130.0	18.6%	126.8	106.9	100+%	95%	3
207	2/17/2018	Toe drain, STA 9+50 (Ref sheet 6)	5130.0	17.9%	126.4	107.2	100+%	95%	3

FIELD DENSITY TEST REPORT

ASTM D 2922-Density
ASTM D3017-Moisture

MOISTURE-DENSITY RELATIONSHIPS

ASTM D 4253 & 4254

Curve No.	Maximum Dry Density (pcf)	Optimum Moisture (%)
2	106.4	18.6%
4	99.9	20.3%

PROJECT: Swede Lake

JOB NO: 110480

CLIENT: Boulder County

CONTRACTOR: CAP

ENGINEER: Engineering Analytics, Inc.

TESTED BY: EAH

NOTES: Approximate embankment STA 9+00 outlet pipe stationing noted for tests

Datum: _____

Test No.	Date	Location	Elevation	% Moist	Density (pcf)		% Compaction	Required Compaction	Curve No.
					Moist	Dry			
208	2/26/2018	Toe drain backfill, STA 7+50	5128.3	18.2%	123.5	104.5	98%	95%	2
209	2/26/2018	Toe drain backfill, STA 6+25	5128.5	17.4%	125.6	107.0	100+%	95%	2
210	2/26/2018	Toe drain backfill, STA 5+00	5128.7	20.5%	122.8	101.9	96%	95%	2
211	2/26/2018	Toe drain backfill, STA 4+00	5129.7	17.6%	126.1	107.2	100+%	95%	2
212	2/26/2018	Toe drain backfill, STA 3+00	5131.0	16.9%	122.0	104.4	98%	95%	2
213	2/26/2018	Toe drain backfill, STA 1+75	5131.0	16.7%	118.7	101.7	96%	95%	2

APPENDIX D
STRUCTURAL DESIGN LETTER

January 8, 2018
Project No. 110480

Mr. Tim Zych
Project Manager
Boulder County Parks and Open Space
5201 Saint Vrain Rd.
Longmont, CO, 80503

Subject: Swede Dam, Dam ID: 050304
Construction File No.: C-2064
Water Division 1, Water District 5
Evaluation of Structural Integrity of the Irrigation Tower

Dear Mr. Zych

During the construction of the irrigation tower, concrete tests and cylinders were taken per usual. The cylinders were low on the 28-day strength test. The two samples tested at 3,858 and 3,846 psi rather than the required 4,500 psi according to the Construction Specifications. The structural calculations on the irrigation tower were redone, and it was determined that the tower is structurally sound with a concrete strength of 3,846 psi. See the attached documents for structural calculations.

Sincerely,



Engineering Analytics, Inc.

DESIGN OF CONCRETE BEAMS

ACI 350-06

Page

PROJECT: Swede Lake

MEMBER I.D.:

Irrigation Outlet

INPUT VALUES

$f'_c =$ 3846 psi	$b =$ 12 in	Ult L.F. = 1.6001	Calculated
$f_y =$ 60000 psi	$D =$ 12 in	Env. Exp. None	Quadratic Coefficients
$E_s =$ 29000 ksi	$d_{cvr} =$ 2.65 in	One Way Member	a 45884.1883
$M_o =$ 3.07 k-ft	L.F. 1.60	$S_d = \phi f_y / \gamma f_s =$ 1.00	b -542250
$M_u =$ 4.91 k-ft	$d_{e\ cvr} =$ 0 in <----- (0 for slabs)		c 65520

CALCULATED VALUES

(see ACI 350-06 Section 10.5 for A_{smin})

$E_c =$ 3573 ksi	
$n =$ 8.1	
$d =$ 9.0375 in	
$B_1 =$ 0.85	
$\rho_{min(MOR)} =$ 0.0031	$A_{smin} =$ 0.36 in ² (max of 2 eqns)
$\rho_{min(ACI)} =$ 0.0033	
$\rho_{max} =$ 0.0174	$A_{smax} =$ 1.884 in ²
$\rho_{bal} =$ 0.0274	
$\rho_{req} =$ 0.0011	$A_{sreq} =$ 0.122 in ²
$=$ 0.04 ρ_{bal}	
$(1.33 * A_{sreq}) =$ 0.16 in ²	$A_{smin} =$ 0.16 in ² (min of A_{smin} or $1.33 * A_{sreq}$)

QTY	SIZE	Area	As pro
1	#4	0.20	0.20
1	#5	0.31	0.31
1	#6	0.44	0.44
1	#7	0.60	0.60
1	#8	0.79	0.79
1	#9	1.00	1.00
1	#10	1.27	1.27

As = 0.16 in²

-----> Minimum steel controls - Use A_{smin} or provide $1.33(A_{sreq})$ per ACI 10.5

REBAR SPACING

ACI 318-05 Crack Control Provisions (10.6.4)

INPUT---> Selected Bar Size **#5**
Qty of bars used = **1**

Calcd Values	Area of bar = 0.31 in ²	
	Clear Cover = 2.65 in	
	$A_{spro} =$ 0.31 in ²	OK
	$\rho =$ 0.3%	
	$M_o =$ 3.071 k-ft	
	$a =$ 0.47 in	
	$j =$ 0.97	
	$f_s = M_o / [A_s * (d - a/2)] =$ 13.5 ksi	
	s = 12.0 in	OK
	$s_{max} =$ 18.0 in	

#5@12 in 12 inch deep beam is: OK

ACI 350-06 REBAR SPACING

$s_{max} =$ 12.0 in **OK**

CRACK CONTROL

ACI 350-06 Crack Control Provisions

Reinforcement Stresses ACI 350 Section 10.6.4.1-3

$\beta = 1.35$ ACI 350 Section 10.6.4.4

Exposure	Allowable Bar Stress, f_s	
Normal	20.0 ksi	OK
Severe	17.0 ksi	OK

Actual Bar Stress = 13.5 ksi

Stress Ratio	Concrete Stress
Normal 0.68	$f_c =$ 736.0 psi
Severe 0.79	$f_{c,all} =$ 1731 psi

Given: Retained Wall Height, $H := 13.75$ ft

Construction Load Height, $H_{const} := 2$ ft

Unit Weight of Soil, $\gamma := 130$ lbs/ft³

Strength Reduction Factor, $\phi := 0.75$

Compressive Strength of Concrete, $f'_c := 3846$ psi

Construction Load, $L_{const} := 130$ lb/ft²

Earth Loading Factor of Safety, $FS_{Earth} := 1.6$

Width of Vault Gate $l := 6$ ft

Calculate the maximum Shear Load

Retained Wall Height at a, accounting for pipe and concrete encasement on east wall

$$H_a := H + H_{const} = 15.75 \text{ ft}$$

$$V_0 := 0.5 \cdot \gamma \cdot H \cdot \frac{l}{2} = 2.68 \cdot 10^3 \frac{\text{lbs}}{\text{ft}}$$

$$V_u := FS_{Earth} \cdot V_0 = 4.29 \cdot 10^3 \frac{\text{lbs}}{\text{ft}}$$

$$d := 12 - 2.625 = 9.375 \text{ inches}$$

$$\phi V_{na} := 2 \cdot \phi \cdot 12 \cdot d \cdot \sqrt{f'_c} = 1.05 \cdot 10^4 \frac{\text{lbs}}{\text{ft}}$$

Thus, wall thickness of (D) $D := 2.625 + d = 12$ in. will not require stirrups.