

HYDROLOGY REPORT
ENLARGEMENT OF OLD DILLON RESERVOIR
DAM ID 360117
WATER DIVISION No. 5
WATER DISTRICT No. 36

Prepared for:

Colorado River Water Conservation District
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1.0 INTRODUCTION

This report summarizes the hydrology evaluation of the Old Dillon Reservoir (ODR) enlargement project and presents the inflow design flood (IDF) for the determination of the required spillway capacity. The report also includes calculations and supporting data. The components of the project include the following:

- Replacing Dillon Ditch with a pipe and modifying its headgate on Salt Lick Gulch to serve the enlarged reservoir
- Increasing the size of the existing reservoir to 286 acre-feet
- Restoring the outlet from the existing reservoir to the south to the Blue River (now Dillon Reservoir)
- Rehabilitating the outlet to Salt Lick Gulch

Subsequent sections of this report present the design criteria established for storm flow criteria for the proposed improvements.

The purpose of the ODR improvements is to:

- Increase the capacity of the ODR
- Increase storage for the Towns of Dillon, Silverthorne and Summit County
- Provide more flexibility in management of water from Salt Lick Gulch

The dam is located in Water Division No. 5, Water District No. 36. It is also located in Section 13, Township 5 South, Range 78 West. The State DAM ID is 360117. The dam is currently classified as a Small, Low Hazard Dam. The proposed enlargement will change the Hazard Classification to a Small, High Hazard Dam.

The Colorado River Water Conservation District is the lead agency for design and implementation of the ODR improvements. A vicinity map is presented in Figure 1.

2.0 HISTORY AND EXISTING CONDITIONS

The ODR is located near the center of Summit County, approximately 70 miles west of Denver, Colorado (Figure 1). The reservoir was originally built in 1939 to supply water for the historic Town of Dillon. After the Town of Dillon was relocated for the construction of Denver Water's Dillon Reservoir, the Town no longer used the Old Dillon Reservoir for water supply and the reservoir no longer actively serviced Dillon.

The existing reservoir has a surface area of approximately 9 acres, and is impounded by two embankments approximately 5 to 7 feet high in a saddle on an east-west trending ridge providing storage of about 46 acre-feet. Under proposed conditions the embankments will be raised so the surface area of the reservoir will be increased to approximately 16 acres, providing storage for about 286 acre-feet. Water is supplied to the reservoir from Salt Lick Gulch. The Salt Lick Gulch drainage basin extends to the peak of Buffalo Mountain in the Gore Range. Salt Lick Gulch is tributary to the Blue River. Water from Salt Lick Gulch is diverted via a headgate into

the Dillon Ditch. Dillon Ditch continues east and passes under Interstate 70 through an inverted siphon and then continues east discharging into the Old Dillon Reservoir. The siphon was built in the 1970's with the construction of Interstate I-70. The siphon is a 24" diameter, reinforced concrete pipe. Flow then returns to Salt Lick Gulch approximately 0.9 miles downstream of the diversion via an outlet channel and culvert under Interstate 70. Drainage area tributary to the headgate on Salt Lick Gulch is 2.73 sq.mi. The drainage area directly tributary to the reservoir is relatively small at 0.051 sq.mi. (33 acres).

3.0 HYDROLOGY

This section presents the development of the inflow design flood and provides the hydrologic and hydraulic calculations for the proposed enlargement of Old Dillon Reservoir. Analyses of storm precipitation and runoff were performed to evaluate the capacity of proposed conveyance facilities for the Old Dillon Reservoir. The Probable Maximum Precipitation (PMP) Storms, used to determine the IDF, are discussed in this section. Both USBR and NRCS methods were used for hydrologic calculations.

3.1 Hydrologic Parameters

3.1.1 *Basin Geometry and Topographic Parameters*

The drainage basins that directly contribute to the Old Dillon Reservoir encompass a total of 0.051 square miles. The total watershed area and individual contributing hydrologic basins and centroid locations are presented in Figure 2. A summary of the physical parameters including area, elevations, and flow lengths are presented in Tables 1 and 2.

The hydraulic characteristics of each subbasin were represented by a K_n roughness value. The United States Bureau of Reclamation (USBR) publication, "Design of Small Dams", recommends K_n values that range from 0.050 to 0.339 for the Rocky Mountains. A K_n value was applied as a representative roughness for the study drainage basin based on previously accepted basin studies in comparable hydrologic and topographic settings. Separate K_n values for the frequency storms, the local PMP, and the general PMP were estimated. K_n values for each basin are summarized in Table 1.

For the NRCS method, soil maps were reviewed and it was determined that 'Type B' soils are present in the drainage areas directly tributary to ODR. A CN value of 86 was selected for the analysis. This value was selected because it represents bare soil which is the conservative condition. The TR-55 method was used to calculate time of concentration and lag times. Curve Number values and times of concentration used in the SCS method are summarized in Table 2.

3.1.2 *Unit Hydrographs*

The synthetic unit hydrographs for the contributing basins were determined using a Microsoft Excel spreadsheet developed by the Division One Office of the State Engineer. The hydrographs were calculated for each basin using the USBR Rocky Mountains data and are provided in

Appendix A. For the NRCS method unit hydrographs were created using a Type 2 storm distribution.

3.1.3 Reservoir Hydrograph

The peak runoff for rain falling directly on to the ODR reservoir was calculated using the following formula:

$$Q_p = 645.33 \left(\frac{A}{t} \right)$$

Where A = basin area in square miles

t = duration in hours, also the calculation interval from HEC-1

3.1.4 Inflow Design Flood

The Inflow Design Flood (IDF) requirements for determining the spillway capacity was developed using Hydrometeorological Report (HMR) 49.

3.1.5 Probable Maximum Precipitation (PMP)

The Inflow Design Flood requirement for a small, high hazard dam is 90% of the PMP per Rule 5.9.1.4, Table 5.2 of the Dam Safety Rules and Regulations (2007).

3.1.5.1 PMP Adjustments

Based on rule 5.9.1.5, Table 5.3, the PMP was not adjusted for elevation.

3.1.5.2 PMP General Storm

A general storm is a long-duration event associated with a frontal storm system. Determination of the 1-, 6-, 24-, and 72-hour general storm index PMP values were made using the HMR-49 10-mi² PMP index maps. Duration values for the general storm PMP were estimated for durations of 5-minutes, 15-minutes, 1-hour, 2-hours, 3-hours, 6-hours, 12-hours, 24-hours, 48-hours, and 72-hours. The recommended procedure by the Colorado Dam Safety Branch Hydrology Committee was used for depth duration values that were not determined by HMR-49. Calculations for PMP storms are presented in Appendix A.

3.1.5.3 PMP Local Storm

A local storm is short duration, high intensity event. Determination of the one-hour index PMP estimate was made using the 1-mi² PMP at elevation 5,000 feet index map in HMR-49. Calculations for PMP storms are presented in Appendix A.

Local storm precipitation data for the HEC-1 program requires depth duration values at 5-minute, 15-minute, 1-hour, 2-hour, 3-hour, and 6-hour durations. Depth duration values that were not readily available from HMR-49 were based upon the recommended procedure by the

Colorado Dam Safety Branch Hydrology Committee. Calculations for the PMP Local Storm are presented in Appendix A.

3.1.6 Snowmelt Runoff

Due to the very small size of the tributary drainage basin snowmelt runoff was not calculated in this study. A base flow of 10 cfs was assumed for the flow entering reservoir from the Salt Lick Gulch headgate based upon the in priority water rights.

3.2 Reservoir Elevation-Capacity Curve

The ODR Reservoir elevation-capacity curve used in the HEC-1 modeling was based on 1-foot contours based upon the proposed dam embankments. The elevation-area data was entered directly in to HEC-1 model which then computes, using the conic method, the reservoir volume.

The total storage within the reservoir at the proposed normal high water surface elevation (el. 9190.5) is approximately 286 ac-ft. The total storage at the maximum high water surface elevation (el. 9192.4) is approximately 314 ac-ft. A summary of elevation-capacity data and a chart of the curve is presented in Appendix A.

3.3 Hydrologic Modeling – Reservoir Inflow

The HEC-1 computer program (US Army Corps of Engineers, 1990) is used for the hydrologic modeling. The USBR and NRCS models were run using both the Local and General PMP events.

All models were produced using the parameters described in preceding sections. All of the basins modeled are directly tributary to the reservoir so channel routing was not necessary. Detailed input and output of the modeling effort is presented in Appendix B in the form of HEC-1 reports.

Table 3. Summary of HEC-1 Model Output Inflow to Reservoir

Model	Peak Discharge (cfs)
USBR – LOCAL PMP	258
USBR – GENERAL PMP	169
NRCS – LOCAL PMP	254
NRCS – GENERAL PMP	195

3.4 Proposed Old Dillon Dam Spillway

The proposed ODR spillway is a concrete structure located on the north end of the dam. It is a concrete box with rectangular weirs cut into the sides. One slot, on the front of the box, is 8' wide with a crest elevation set at 9190.5. Two additional slots, one on each side, are 6' wide with crest elevations set at 9191.5. A 40% obstruction due to screening was assumed for these openings so the widths were adjusted in the HEC-1 model in order to account for this factor.

The top elevation of the dam is approximately at elevation 9194. The spillway discharges into the existing channel that will return flows to Salt Lick Gulch.

A weir coefficient of 2.65 was used in the hydrologic model. This value was selected because it is a conservative value for the spillway. A sketch of the proposed spillway, and associated spillway rating curve and calculations are presented in Appendix A.

3.5 Hydrologic Modeling Results - Spillway

A table summarizing the results of the hydrologic models is presented below. Detailed HEC-1 reports, including input and output, are presented in Appendix A.

Table 4. Summary of HEC-1 Model Output, Outflow to Salt Lick Gulch

Model	Spillway Peak Discharge (cfs)	Maximum Elevation (ft. AMSL)
USBR – LOCAL PMP	37	9192.2
USBR – GENERAL PMP	37	9192.2
NRCS – LOCAL PMP	31	9192.0
NRCS – GENERAL PMP	37	9192.2

Three of the models summarized in the above table show that the peak discharge from the reservoir is not dependent on the type of storm analyzed. The peak discharge is approximately 37 cfs over the spillway with a maximum elevation of 9192.2. The proposed spillway is shown to be effective for this storm. The ODR system is able to store and release the IDF.

A summary of proposed reservoir area capacity data and curve is presented in Appendix A.

4.0 CONCLUSION

It is proposed to expand the size of the Old Dillon Reservoir to increase its storage capacity. The project includes construction of new dam embankments and a new spillway structure. The new spillway will discharge to Salt Lick Gulch, located on the north end of the project site.

The new dams will be classified as a small high hazard dams. The Inflow Design Flood for the new dam is 90% of the PMP.

Four HEC-1 models of the ODR and its tributary basins were prepared to model the local and general PMP storms using USBR and NRCS hydrographs. The results of the models show that the local PMP model with USBR hydrographs has the greatest peak discharge.

A spillway was encoded into each model to evaluate the storage capacity of the ODR. Results of the hydrologic modeling show that the proposed spillway has the same peak outflow rate independent of the inflow. This is due to the ratio of the reservoir volume to the tributary watershed area including the base inflow of 10 cfs from Dillon Ditch. The peak outflow for the

proposed ODR is approximately 37 cfs. The proposed system is capable of storing and discharging the Inflow Design Flood.

5.0 REFERENCES

Hydrologic Engineering Center, U.S. Army Corps of Engineers Flood Hydrograph Package, HEC-1, Version 4.1, June 1998.

Resource Engineering Inc., *Hydrology Specialist's Report Old Dillon Reservoir Enlargement Environmental Assessment*, August 2008.

State of Colorado, Department of Natural Resources, Division of Water Resources, Office of the State Engineer, *Rules and Regulations for Dam Safety and Dam Construction* January 1, 2007.

United States Department of Commerce, National Oceanic and Atmospheric Administration Hydrometeorological Reports (HMR No. 49, Probable Maximum Precipitation Estimates, Colorado River and Great Basin Drainages).

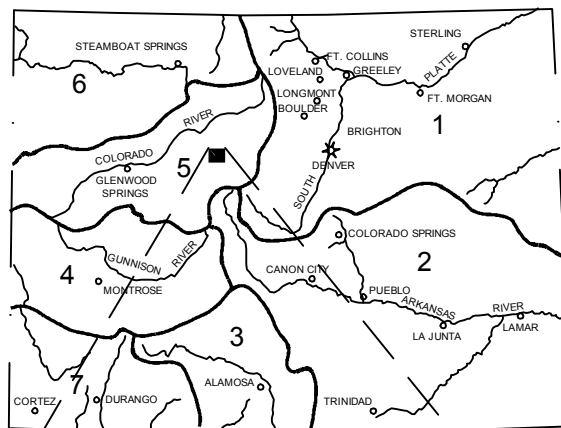
United State Department of the Interior, Bureau of Reclamation, *Design of Small Dam* Third Edition, United States Government Printing Office Denver, CO, 1987.

TABLES

TABLE 1																	
PROPOSED RESERVOIR BASIN CHARACTERISTICS - USBR Methodology																	
						Elevation	Flow	Flow	Centroidal	Centroidal						Basin	Lag
Basin	Area	Area				Change	Length, L	Length, L	Flow	Flow	Basin	Basin				Factor	Time
ID	(ft^2)	(acres)	(sq. miles)			(feet)	(feet)	(mile)	Length, Lca	Length, Lca	Slope	Slope	Kn1				(hours)
	sf			top	bot				(feet)	(mile)	(ft/ft)	(ft/mile)	100/500 YR	Local PMP	Gen. PMP		
SW	388960	8.93	0.014	9337	9190.5	146.5	1383	0.262	260	0.049	0.106	559.314	0.050	0.080	0.130	0.001	0.106
NE	334868	7.69	0.012	9349	9190.5	158.5	854	0.162	229	0.043	0.186	979.488	0.050	0.080	0.130	0.000	0.079
Lake	699116	16.05	0.025			0											
Total		32.67	0.051														
Notes:	1. An average drainage area Kn was applied to each sub-basin.																
TABLE 2																	
PROPOSED RESERVOIR BASIN CHARACTERISTICS - NRCS Methodology																	
						Elevation	Flow	Flow	Basin	Basin	Curve	Rainfall in inches				Lag	
Basin	Area	Area				Change	Length, L	Length, L	Slope	Slope	Number	Local	General			Time	
ID	(ft^2)	(acres)	(sq. miles)			(feet)	(feet)	(mile)	(ft/ft)	(ft/mile)						(hours)	
	sf			top	bot												
SW	388960	8.93	0.014	9337	9190.5	146.5	1383	0.262	0.106	559.314	86	10.920	21.500		0.117		
NE	334868	7.69	0.012	9349	9190.5	158.5	854	0.162	0.186	979.488	86	10.920	21.500		0.104		
Lake	699116	16.05	0.025			0					98	10.920	21.500				
Total		32.67	0.051														
Notes:	1. General Storm Rainfall totals were much higher than county averages due to the small size of the drainage area.																

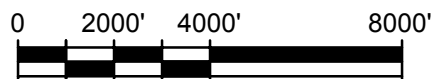
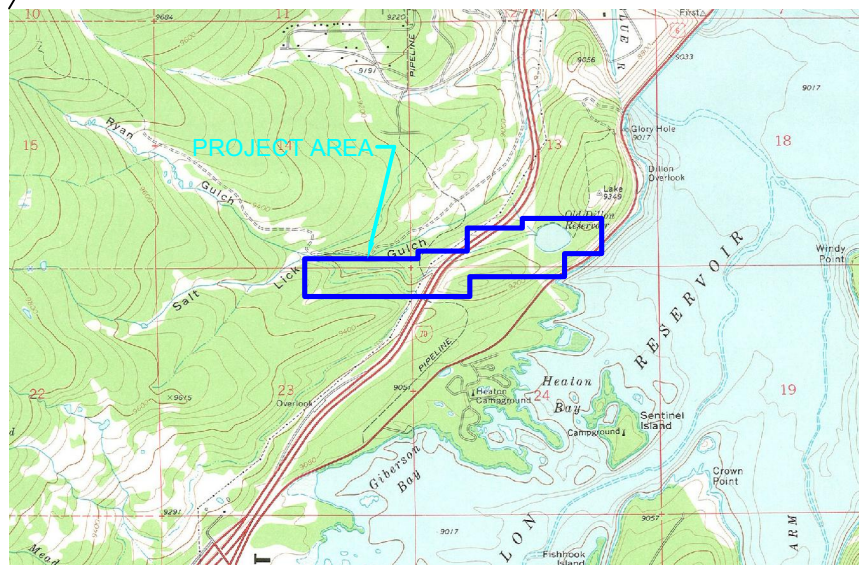
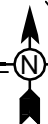
FIGURES

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STATE OF COLORADO
PROJECT LOCATION MAP

NOT TO SCALE



TETRA TECH

www.tetratech.com

1900 S. SUNSET STREET, SUITE I-F
LONGMONT, COLORADO 80501
PHONE: 303-772-5282 FAX: 303-772-7039

Drawing Description

PROJECT LOCATION
AND VICINITY MAP

Project No.: 133-1187-004-03

Date: 10-24-08

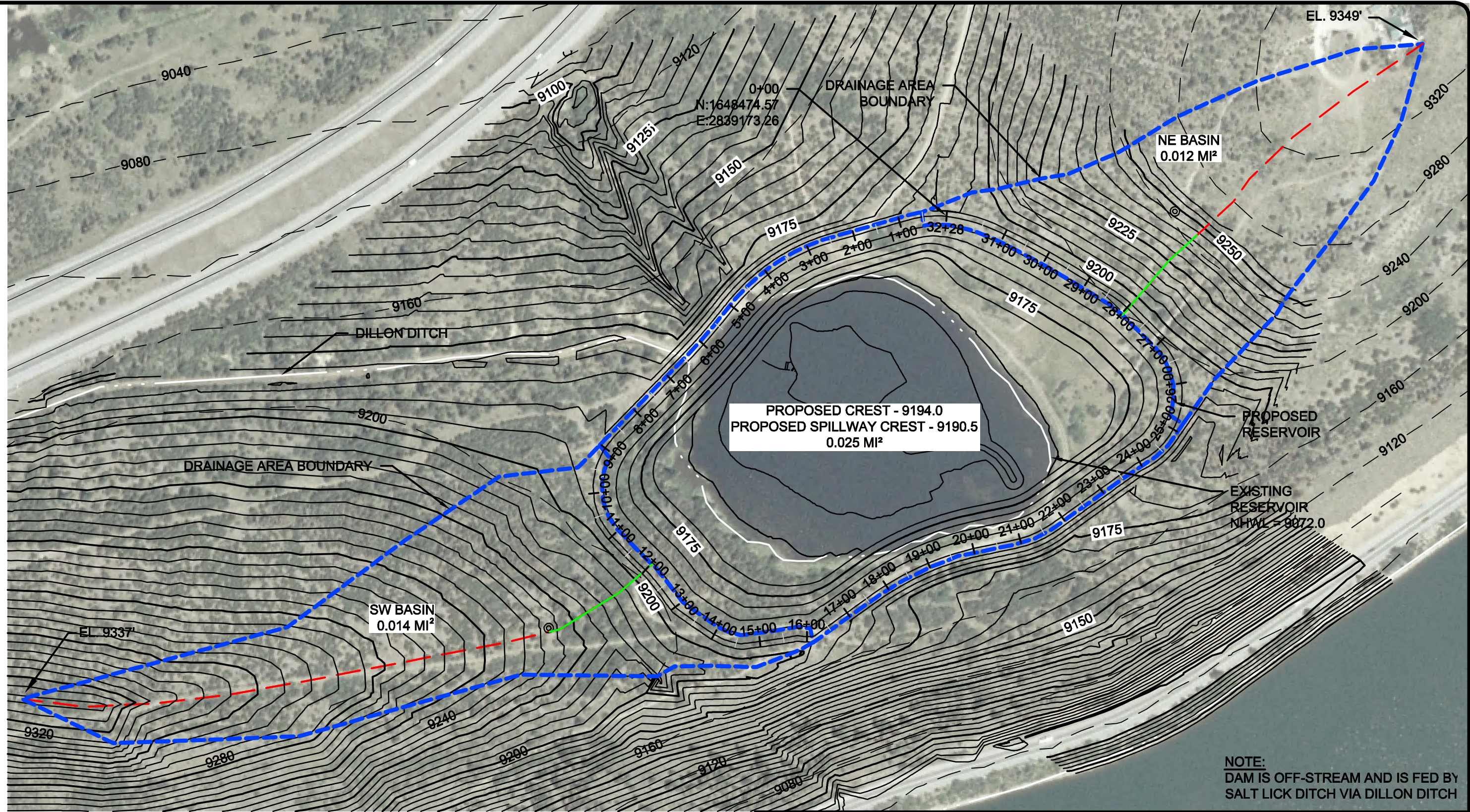
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Figure No.

1

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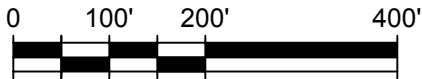
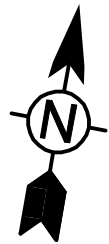
Monday, January 18, 2010 11:36:21 AM DRAWING: P:\133_1187_004_03_Old_Dillon_Res\CAD\RefFiles\ReportFigures\Figures1-2.DWG LAYOUT: FIG-2 USER NAME: MORISON, MIKE



NOTE:
DAM IS OFF-STREAM AND IS FED BY
SALT LICK DITCH VIA DILLON DITCH

LEGEND

- 5' C.I. TETRA TECH (EXISTING/PROPOSED)
- 40' C.I. USGS CONTOURS
- DRAINAGE BOUNDARY
- L
- LC
- CENTROID



TETRA TECH

www.tetratech.com

1900 S. SUNSET STREET, SUITE I-F
LONGMONT, COLORADO
PHONE: 303-772-5282 FAX: 303-772-7039

Drawing Description
**OLD DILLON RESERVOIR
WATERSHED MAP**

Project No.: 133-1187-004-03
Date: 10-24-08
Designed By: AT

Figure No.
2

APPENDIX A

CALCULATIONS

USBR UNIT HYDROGRAPHS



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: USBR HYDROGRAPH FOR RAINFALLING DIRECTLY ON A RESERVOIR

Total Number of Pages (including cover sheet): 1

Total Number of Computer Runs: —

Prepared by: AST Date: OCT 16, 2008

Checked by: _____ Date: _____

Description and Purpose:

UNIT HYDROGRAPH FOR RAINFALL DIRECTLY ON A RESERVOIR

$$Q_p = 645.33 \left(\frac{A}{t} \right)$$

A = basin area in square miles

t = duration in hours

$$Q_p = A^{3/5}$$

Design Basis/References/Assumptions:

$$A = 16.05 \text{ ACRES} \\ = 0.025 \text{ mi}^2$$

$$t = 1 \text{ minute} = 0.0167 \\ 3 \text{ minute} = 0.05$$

1 minute
interval

$$Q_p = 968 \text{ cfs}$$

3 minute
interval

$$Q_p = 323 \text{ cfs}$$

Remarks/Conclusions/Results:

FOR INPUT IN HEC-1

Calculation Approved by:

Project Manager

10/24/08

Date

Revision No.:

Description of Revision:

Approved by:

Project Manager/Date

Unit Hydrograph for Rainfall Directly on a Reservoir

$$Q_p = 645.33 \cdot (A/t)$$

for: A = Basin Area in square miles
t = Duration in hours

$$A = 0.3 \text{ Square Miles}$$

$$t = 0.083 \text{ Hours}$$

5.0 Minutes (Time step from HEC-1)

$$Q_p = 2323 \text{ cfs}$$

$$\frac{.013}{1}$$

$$t_{\min} = .0167$$

$$Q_p = 503 \text{ cfs}$$

$$A = .025 \text{ mi}^2$$

$$t = 1 \text{ min}$$

$$Q_p = 968.$$

$$t = 5 \text{ min}$$

$$Q_p = 194$$

$$\text{Area}_{\text{res}} = .025$$

$$t = 3 \text{ min}$$

$$Q_{\text{peak}} = 322.7$$
$$= 323.0$$



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: USBR LOCAL STORM HYDROGRAPH

Total Number of Pages (including cover sheet): 5

Total Number of Computer Runs: —

Prepared by: AJT Date: OCT 16, 2008

Checked by: _____ Date: _____

Description and Purpose:

USBR LOCAL STORM (PMP) HYDROGRAPH

Design Basis/References/Assumptions:

SPREAD SHEET FROM SEO

Remarks/Conclusions/Results:

FOR INPUT INTO HEL-1

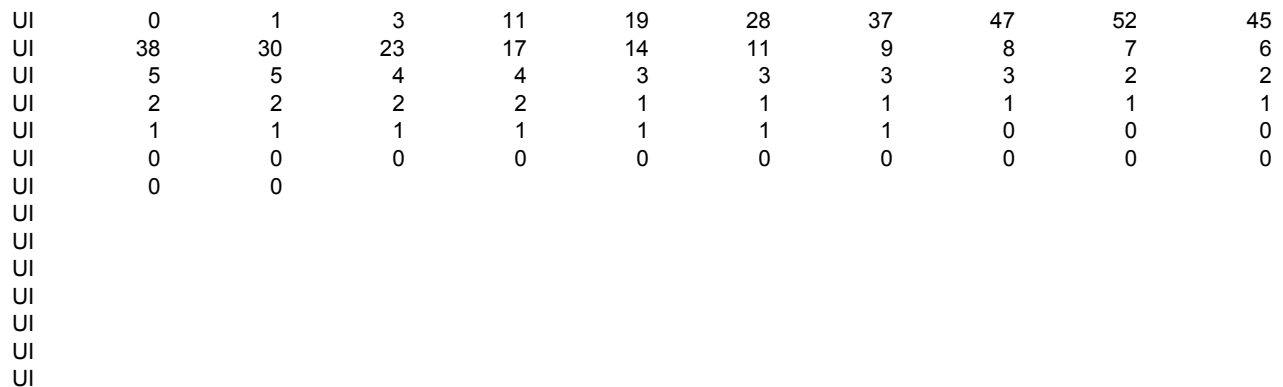
Calculation Approved by: _____
Project Manager Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____

Project Manager/Date

Lg+D/2 =	0.17	Hours
Basin Factor =	0.06	
V' =	0.32	cfs/Day
Qs =	1.9	* q, cfs

Data to be used in Analysis Unit Duration, D = 5 minutes, round down to nearest of 5, 10, 15, 30, 60, 120, 180, or 360
Selected Timestep = 1 minutes, integer value evenly divisible into 60



UI
UI
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USBR calculated unitgraph peak = 53

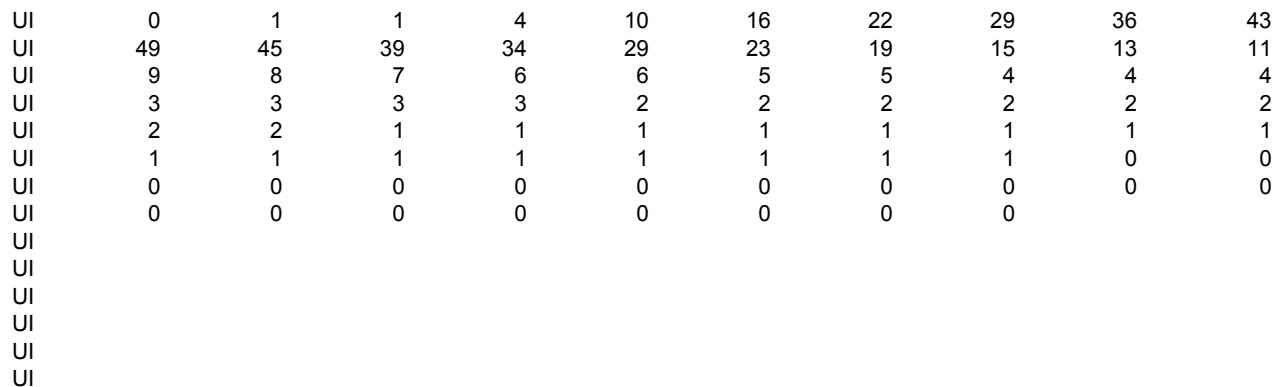
Interpolated Peak = 52

Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs	Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs
5.0	0.01	0.5	0.14	0	305.0	0.52	31.3	1.05	2
10.0	0.02	1.0	0.21	0	310.0	0.53	31.9	1.00	2
15.0	0.03	1.5	0.33	1	315.0	0.54	32.4	0.96	2
20.0	0.03	2.1	0.51	1	320.0	0.55	32.9	0.92	2
25.0	0.04	2.6	0.84	2	325.0	0.56	33.4	0.88	2
30.0	0.05	3.1	1.62	3	330.0	0.57	33.9	0.84	2
35.0	0.06	3.6	3.74	7	335.0	0.57	34.4	0.81	2
40.0	0.07	4.1	6.38	12	340.0	0.58	34.9	0.77	1
45.0	0.08	4.6	8.61	16	345.0	0.59	35.5	0.74	1
50.0	0.09	5.1	10.94	21	350.0	0.60	36.0	0.71	1
55.0	0.09	5.7	13.26	25	355.0	0.61	36.5	0.68	1
60.0	0.10	6.2	15.70	30	360.0	0.62	37.0	0.65	1
65.0	0.11	6.7	18.23	34	365.0	0.63	37.5	0.62	1
70.0	0.12	7.2	20.76	39	370.0	0.63	38.0	0.59	1
75.0	0.13	7.7	23.30	44	375.0	0.64	38.5	0.57	1
80.0	0.14	8.2	25.83	49	380.0	0.65	39.1	0.55	1
85.0	0.15	8.7	28.36	53	385.0	0.66	39.6	0.52	1
90.0	0.15	9.3	26.53	50	390.0	0.67	40.1	0.50	1
95.0	0.16	9.8	24.71	47	395.0	0.68	40.6	0.48	1
100.0	0.17	10.3	22.68	43	400.0	0.69	41.1	0.46	1
105.0	0.18	10.8	20.76	39	405.0	0.69	41.6	0.43	1
110.0	0.19	11.3	18.84	35	410.0	0.70	42.1	0.42	1
115.0	0.20	11.8	16.81	32	415.0	0.71	42.7	0.40	1
120.0	0.21	12.3	14.99	28	420.0	0.72	43.2	0.38	1
125.0	0.21	12.8	12.86	24	425.0	0.73	43.7	0.36	1
130.0	0.22	13.4	11.04	21	430.0	0.74	44.2	0.35	1
135.0	0.23	13.9	9.52	18	435.0	0.75	44.7	0.33	1
140.0	0.24	14.4	8.41	16	440.0	0.75	45.2	0.32	1
145.0	0.25	14.9	7.50	14	445.0	0.76	45.7	0.31	1
150.0	0.26	15.4	6.69	13	450.0	0.77	46.3	0.29	1
155.0	0.27	15.9	5.98	11	455.0	0.78	46.8	0.28	1
160.0	0.27	16.4	5.47	10	460.0	0.79	47.3	0.27	1
165.0	0.28	17.0	4.97	9	465.0	0.80	47.8	0.26	0
170.0	0.29	17.5	4.55	9	470.0	0.81	48.3	0.25	0
175.0	0.30	18.0	4.25	8	475.0	0.81	48.8	0.24	0
180.0	0.31	18.5	3.89	7	480.0	0.82	49.3	0.23	0
185.0	0.32	19.0	3.59	7	485.0	0.83	49.8	0.22	0
190.0	0.33	19.5	3.34	6	490.0	0.84	50.4	0.21	0
195.0	0.33	20.0	3.13	6	495.0	0.85	50.9	0.20	0
200.0	0.34	20.6	2.93	6	500.0	0.86	51.4	0.19	0
205.0	0.35	21.1	2.75	5	505.0	0.87	51.9	0.18	0
210.0	0.36	21.6	2.61	5	510.0	0.87	52.4	0.17	0
215.0	0.37	22.1	2.44	5	515.0	0.88	52.9	0.17	0
220.0	0.38	22.6	2.31	4	520.0	0.89	53.4	0.16	0
225.0	0.39	23.1	2.17	4	525.0	0.90	54.0	0.16	0
230.0	0.39	23.6	2.04	4	530.0	0.91	54.5	0.15	0
235.0	0.40	24.2	1.95	4	535.0	0.92	55.0	0.15	0
240.0	0.41	24.7	1.84	3	540.0	0.93	55.5	0.14	0
245.0	0.42	25.2	1.76	3	545.0	0.93	56.0	0.14	0
250.0	0.43	25.7	1.69	3	550.0	0.94	56.5	0.13	0
255.0	0.44	26.2	1.62	3	555.0	0.95	57.0	0.13	0
260.0	0.45	26.7	1.55	3	560.0	0.96	57.6	0.12	0
265.0	0.45	27.2	1.49	3	565.0	0.97	58.1	0.12	0
270.0	0.46	27.8	1.42	3	570.0	0.98	58.6	0.11	0
275.0	0.47	28.3	1.36	3	575.0	0.99	59.1	0.11	0
280.0	0.48	28.8	1.30	2	580.0	0.99	59.6	0.10	0
285.0	0.49	29.3	1.24	2	585.0	1.00	60.1	0.10	0
290.0	0.50	29.8	1.19	2	590.0	1.01	60.6	0.09	0
295.0	0.51	30.3	1.14	2	595.0	1.02	61.2	0.09	0
300.0	0.51	30.8	1.09	2	600.0	1.03	61.7	0.08	0

NOTES : 1. Methodology used Dimensionless Unit Hydrograph.
2. For values of q use Table 4-11 from Flood Hydrology Manual

Lg+D/2 =	0.22	Hours
Basin Factor =	0.08	
V' =	0.38	cfs/Day
Qs =	1.7	* q, cfs

Data to be used in Analysis Unit Duration, D = 5 minutes, round down to nearest of 5, 10, 15, 30, 60, 120, 180, or 360
Selected Timestep = 1 minutes, integer value evenly divisible into 60



UI
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UI

USBR calculated unitgraph peak = 50

Interpolated Peak = 49

Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs	Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs
5.0	0.01	0.6	0.14	0	305.0	0.66	39.5	1.05	2
10.0	0.02	1.3	0.21	0	310.0	0.67	40.1	1.00	2
15.0	0.03	1.9	0.33	1	315.0	0.68	40.8	0.96	2
20.0	0.04	2.6	0.51	1	320.0	0.69	41.4	0.92	2
25.0	0.05	3.2	0.84	1	325.0	0.70	42.1	0.88	2
30.0	0.06	3.9	1.62	3	330.0	0.71	42.7	0.84	1
35.0	0.08	4.5	3.74	7	335.0	0.72	43.3	0.81	1
40.0	0.09	5.2	6.38	11	340.0	0.73	44.0	0.77	1
45.0	0.10	5.8	8.61	15	345.0	0.74	44.6	0.74	1
50.0	0.11	6.5	10.94	19	350.0	0.75	45.3	0.71	1
55.0	0.12	7.1	13.26	23	355.0	0.77	45.9	0.68	1
60.0	0.13	7.8	15.70	27	360.0	0.78	46.6	0.65	1
65.0	0.14	8.4	18.23	32	365.0	0.79	47.2	0.62	1
70.0	0.15	9.1	20.76	36	370.0	0.80	47.9	0.59	1
75.0	0.16	9.7	23.30	41	375.0	0.81	48.5	0.57	1
80.0	0.17	10.4	25.83	45	380.0	0.82	49.2	0.55	1
85.0	0.18	11.0	28.36	50	385.0	0.83	49.8	0.52	1
90.0	0.19	11.6	26.53	46	390.0	0.84	50.5	0.50	1
95.0	0.20	12.3	24.71	43	395.0	0.85	51.1	0.48	1
100.0	0.22	12.9	22.68	40	400.0	0.86	51.8	0.46	1
105.0	0.23	13.6	20.76	36	405.0	0.87	52.4	0.43	1
110.0	0.24	14.2	18.84	33	410.0	0.88	53.0	0.42	1
115.0	0.25	14.9	16.81	29	415.0	0.89	53.7	0.40	1
120.0	0.26	15.5	14.99	26	420.0	0.91	54.3	0.38	1
125.0	0.27	16.2	12.86	22	425.0	0.92	55.0	0.36	1
130.0	0.28	16.8	11.04	19	430.0	0.93	55.6	0.35	1
135.0	0.29	17.5	9.52	17	435.0	0.94	56.3	0.33	1
140.0	0.30	18.1	8.41	15	440.0	0.95	56.9	0.32	1
145.0	0.31	18.8	7.50	13	445.0	0.96	57.6	0.31	1
150.0	0.32	19.4	6.69	12	450.0	0.97	58.2	0.29	1
155.0	0.33	20.1	5.98	10	455.0	0.98	58.9	0.28	0
160.0	0.35	20.7	5.47	10	460.0	0.99	59.5	0.27	0
165.0	0.36	21.3	4.97	9	465.0	1.00	60.2	0.26	0
170.0	0.37	22.0	4.55	8	470.0	1.01	60.8	0.25	0
175.0	0.38	22.6	4.25	7	475.0	1.02	61.5	0.24	0
180.0	0.39	23.3	3.89	7	480.0	1.04	62.1	0.23	0
185.0	0.40	23.9	3.59	6	485.0	1.05	62.8	0.22	0
190.0	0.41	24.6	3.34	6	490.0	1.06	63.4	0.21	0
195.0	0.42	25.2	3.13	5	495.0	1.07	64.0	0.20	0
200.0	0.43	25.9	2.93	5	500.0	1.08	64.7	0.19	0
205.0	0.44	26.5	2.75	5	505.0	1.09	65.3	0.18	0
210.0	0.45	27.2	2.61	5	510.0	1.10	66.0	0.17	0
215.0	0.46	27.8	2.44	4	515.0	1.11	66.6	0.17	0
220.0	0.47	28.5	2.31	4	520.0	1.12	67.3	0.16	0
225.0	0.49	29.1	2.17	4	525.0	1.13	67.9	0.16	0
230.0	0.50	29.8	2.04	4	530.0	1.14	68.6	0.15	0
235.0	0.51	30.4	1.95	3	535.0	1.15	69.2	0.15	0
240.0	0.52	31.1	1.84	3	540.0	1.16	69.9	0.14	0
245.0	0.53	31.7	1.76	3	545.0	1.18	70.5	0.14	0
250.0	0.54	32.3	1.69	3	550.0	1.19	71.2	0.13	0
255.0	0.55	33.0	1.62	3	555.0	1.20	71.8	0.13	0
260.0	0.56	33.6	1.55	3	560.0	1.21	72.5	0.12	0
265.0	0.57	34.3	1.49	3	565.0	1.22	73.1	0.12	0
270.0	0.58	34.9	1.42	2	570.0	1.23	73.8	0.11	0
275.0	0.59	35.6	1.36	2	575.0	1.24	74.4	0.11	0
280.0	0.60	36.2	1.30	2	580.0	1.25	75.0	0.10	0
285.0	0.61	36.9	1.24	2	585.0	1.26	75.7	0.10	0
290.0	0.63	37.5	1.19	2	590.0	1.27	76.3	0.09	0
295.0	0.64	38.2	1.14	2	595.0	1.28	77.0	0.09	0
300.0	0.65	38.8	1.09	2	600.0	1.29	77.6	0.08	0

NOTES : 1. Methodology used Dimensionless Unit Hydrograph.
2. For values of q use Table 4-11 from Flood Hydrology Manual



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: USBR GENERAL STORM HYDROGRAPH

Total Number of Pages (including cover sheet): 5

Total Number of Computer Runs: —

Prepared by: ADT Date: OCT 16, 2008

Checked by: _____ Date: _____

Description and Purpose:

USBR GENERAL STORM (PMP) HYDROGRAPH

Design Basis/References/Assumptions:

SPREAD SHEET FROM SEO

Remarks/Conclusions/Results:

FOR INPUT INTO HEC-1

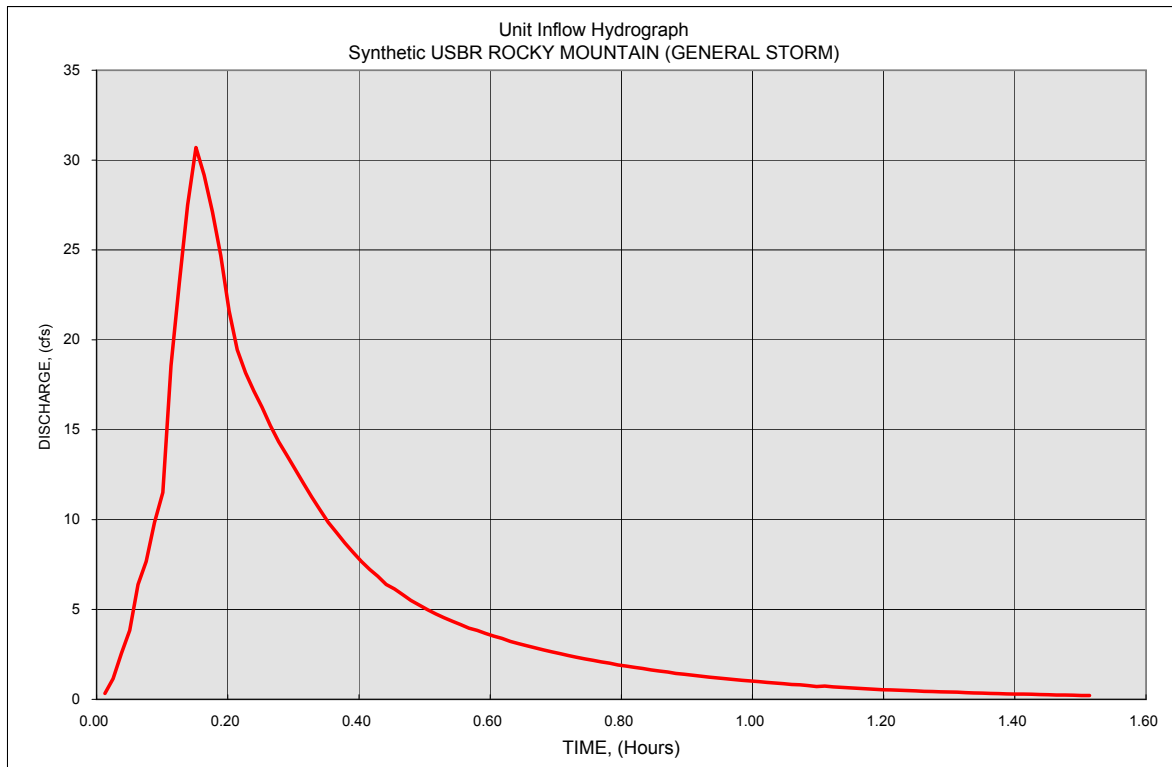
Calculation Approved by: _____
Project Manager Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____

Project Manager/Date

Lg+D/2 =	0.25	Hours
Basin Factor =	0.06	
V' =	0.32	cfs/Day
Qs =	1.3	* q, cfs

Data to be used in Analysis Unit Duration, D = 5 minutes, round down to nearest of 5, 10, 15, 30, 60, 120, 180, or 360
Selected Timestep = 3 minutes, integer value evenly divisible into 60



3 minute interval

[illegible]

UI
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USBR calculated unitgraph peak = 31

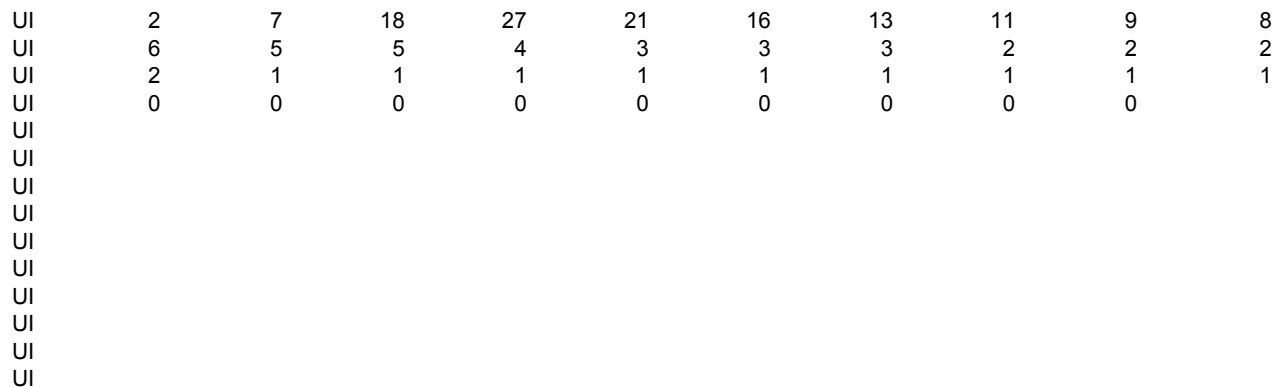
Interpolated Peak = 30

Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs	Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs
5.0	0.01	0.8	0.26	0	305.0	0.77	46.2	1.63	2
10.0	0.03	1.5	0.90	1	310.0	0.78	46.9	1.57	2
15.0	0.04	2.3	2.00	3	315.0	0.79	47.7	1.50	2
20.0	0.05	3.0	3.00	4	320.0	0.81	48.4	1.45	2
25.0	0.06	3.8	5.00	6	325.0	0.82	49.2	1.39	2
30.0	0.08	4.5	6.00	8	330.0	0.83	50.0	1.34	2
35.0	0.09	5.3	7.70	10	335.0	0.85	50.7	1.28	2
40.0	0.10	6.1	9.00	12	340.0	0.86	51.5	1.23	2
45.0	0.11	6.8	14.51	19	345.0	0.87	52.2	1.19	2
50.0	0.13	7.6	18.11	23	350.0	0.88	53.0	1.13	1
55.0	0.14	8.3	21.51	28	355.0	0.90	53.7	1.09	1
60.0	0.15	9.1	24.01	31	360.0	0.91	54.5	1.05	1
65.0	0.16	9.8	22.81	29	365.0	0.92	55.3	1.01	1
70.0	0.18	10.6	21.21	27	370.0	0.93	56.0	0.97	1
75.0	0.19	11.4	19.31	25	375.0	0.95	56.8	0.93	1
80.0	0.20	12.1	16.91	22	380.0	0.96	57.5	0.90	1
85.0	0.21	12.9	15.21	19	385.0	0.97	58.3	0.86	1
90.0	0.23	13.6	14.21	18	390.0	0.98	59.0	0.83	1
95.0	0.24	14.4	13.41	17	395.0	1.00	59.8	0.80	1
100.0	0.25	15.1	12.71	16	400.0	1.01	60.6	0.77	1
105.0	0.26	15.9	11.91	15	405.0	1.02	61.3	0.74	1
110.0	0.28	16.7	11.21	14	410.0	1.03	62.1	0.71	1
115.0	0.29	17.4	10.61	14	415.0	1.05	62.8	0.68	1
120.0	0.30	18.2	10.01	13	420.0	1.06	63.6	0.65	1
125.0	0.32	18.9	9.40	12	425.0	1.07	64.3	0.63	1
130.0	0.33	19.7	8.80	11	430.0	1.09	65.1	0.60	1
135.0	0.34	20.4	8.25	11	435.0	1.10	65.9	0.56	1
140.0	0.35	21.2	7.70	10	440.0	1.11	66.6	0.58	1
145.0	0.37	22.0	7.25	9	445.0	1.12	67.4	0.54	1
150.0	0.38	22.7	6.80	9	450.0	1.14	68.1	0.52	1
155.0	0.39	23.5	6.40	8	455.0	1.15	68.9	0.50	1
160.0	0.40	24.2	6.00	8	460.0	1.16	69.6	0.48	1
165.0	0.42	25.0	5.65	7	465.0	1.17	70.4	0.46	1
170.0	0.43	25.7	5.35	7	470.0	1.19	71.2	0.44	1
175.0	0.44	26.5	5.00	6	475.0	1.20	71.9	0.42	1
180.0	0.45	27.3	4.80	6	480.0	1.21	72.7	0.41	1
185.0	0.47	28.0	4.55	6	485.0	1.22	73.4	0.40	1
190.0	0.48	28.8	4.30	5	490.0	1.24	74.2	0.38	0
195.0	0.49	29.5	4.10	5	495.0	1.25	74.9	0.37	0
200.0	0.50	30.3	3.90	5	500.0	1.26	75.7	0.35	0
205.0	0.52	31.0	3.72	5	505.0	1.27	76.5	0.34	0
210.0	0.53	31.8	3.55	5	510.0	1.29	77.2	0.33	0
215.0	0.54	32.6	3.40	4	515.0	1.30	78.0	0.32	0
220.0	0.56	33.3	3.25	4	520.0	1.31	78.7	0.31	0
225.0	0.57	34.1	3.10	4	525.0	1.32	79.5	0.29	0
230.0	0.58	34.8	3.00	4	530.0	1.34	80.2	0.28	0
235.0	0.59	35.6	2.87	4	535.0	1.35	81.0	0.27	0
240.0	0.61	36.3	2.75	4	540.0	1.36	81.8	0.26	0
245.0	0.62	37.1	2.65	3	545.0	1.38	82.5	0.25	0
250.0	0.63	37.8	2.52	3	550.0	1.39	83.3	0.24	0
255.0	0.64	38.6	2.42	3	555.0	1.40	84.0	0.23	0
260.0	0.66	39.4	2.33	3	560.0	1.41	84.8	0.23	0
265.0	0.67	40.1	2.24	3	565.0	1.43	85.5	0.22	0
270.0	0.68	40.9	2.15	3	570.0	1.44	86.3	0.21	0
275.0	0.69	41.6	2.07	3	575.0	1.45	87.1	0.20	0
280.0	0.71	42.4	1.99	3	580.0	1.46	87.8	0.19	0
285.0	0.72	43.1	1.91	2	585.0	1.48	88.6	0.19	0
290.0	0.73	43.9	1.83	2	590.0	1.49	89.3	0.18	0
295.0	0.74	44.7	1.76	2	595.0	1.50	90.1	0.17	0
300.0	0.76	45.4	1.70	2	600.0	1.51	90.8	0.17	0

NOTES : 1. Methodology used Dimensionless Unit Hydrograph.
2. For values of q use Table 4-9 from Flood Hydrology Manual

Lg+D/2 =	0.32	Hours
Basin Factor =	0.08	
V' =	0.38	cfs/Day
Qs =	1.2	* q, cfs

Data to be used in Analysis Unit Duration, D = 5 minutes, round down to nearest of 5, 10, 15, 30, 60, 120, 180, or 360
Selected Timestep = 3 minutes, integer value evenly divisible into 60



UI
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USBR calculated unitgraph peak = 28

Interpolated Peak = 27

Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs	Time t, % of Lg+D/2	Hours	Min.	q	Qs cfs
5.0	0.02	1.0	0.26	0	305.0	0.99	59.4	1.63	2
10.0	0.03	1.9	0.90	1	310.0	1.01	60.3	1.57	2
15.0	0.05	2.9	2.00	2	315.0	1.02	61.3	1.50	2
20.0	0.06	3.9	3.00	3	320.0	1.04	62.3	1.45	2
25.0	0.08	4.9	5.00	6	325.0	1.05	63.3	1.39	2
30.0	0.10	5.8	6.00	7	330.0	1.07	64.2	1.34	2
35.0	0.11	6.8	7.70	9	335.0	1.09	65.2	1.28	1
40.0	0.13	7.8	9.00	10	340.0	1.10	66.2	1.23	1
45.0	0.15	8.8	14.51	17	345.0	1.12	67.1	1.19	1
50.0	0.16	9.7	18.11	21	350.0	1.14	68.1	1.13	1
55.0	0.18	10.7	21.51	25	355.0	1.15	69.1	1.09	1
60.0	0.19	11.7	24.01	28	360.0	1.17	70.1	1.05	1
65.0	0.21	12.7	22.81	26	365.0	1.18	71.0	1.01	1
70.0	0.23	13.6	21.21	25	370.0	1.20	72.0	0.97	1
75.0	0.24	14.6	19.31	22	375.0	1.22	73.0	0.93	1
80.0	0.26	15.6	16.91	20	380.0	1.23	74.0	0.90	1
85.0	0.28	16.5	15.21	18	385.0	1.25	74.9	0.86	1
90.0	0.29	17.5	14.21	16	390.0	1.27	75.9	0.83	1
95.0	0.31	18.5	13.41	16	395.0	1.28	76.9	0.80	1
100.0	0.32	19.5	12.71	15	400.0	1.30	77.9	0.77	1
105.0	0.34	20.4	11.91	14	405.0	1.31	78.8	0.74	1
110.0	0.36	21.4	11.21	13	410.0	1.33	79.8	0.71	1
115.0	0.37	22.4	10.61	12	415.0	1.35	80.8	0.68	1
120.0	0.39	23.4	10.01	12	420.0	1.36	81.7	0.65	1
125.0	0.41	24.3	9.40	11	425.0	1.38	82.7	0.63	1
130.0	0.42	25.3	8.80	10	430.0	1.39	83.7	0.60	1
135.0	0.44	26.3	8.25	10	435.0	1.41	84.7	0.56	1
140.0	0.45	27.2	7.70	9	440.0	1.43	85.6	0.58	1
145.0	0.47	28.2	7.25	8	445.0	1.44	86.6	0.54	1
150.0	0.49	29.2	6.80	8	450.0	1.46	87.6	0.52	1
155.0	0.50	30.2	6.40	7	455.0	1.48	88.6	0.50	1
160.0	0.52	31.1	6.00	7	460.0	1.49	89.5	0.48	1
165.0	0.54	32.1	5.65	7	465.0	1.51	90.5	0.46	1
170.0	0.55	33.1	5.35	6	470.0	1.52	91.5	0.44	1
175.0	0.57	34.1	5.00	6	475.0	1.54	92.5	0.42	0
180.0	0.58	35.0	4.80	6	480.0	1.56	93.4	0.41	0
185.0	0.60	36.0	4.55	5	485.0	1.57	94.4	0.40	0
190.0	0.62	37.0	4.30	5	490.0	1.59	95.4	0.38	0
195.0	0.63	38.0	4.10	5	495.0	1.61	96.3	0.37	0
200.0	0.65	38.9	3.90	5	500.0	1.62	97.3	0.35	0
205.0	0.66	39.9	3.72	4	505.0	1.64	98.3	0.34	0
210.0	0.68	40.9	3.55	4	510.0	1.65	99.3	0.33	0
215.0	0.70	41.8	3.40	4	515.0	1.67	100.2	0.32	0
220.0	0.71	42.8	3.25	4	520.0	1.69	101.2	0.31	0
225.0	0.73	43.8	3.10	4	525.0	1.70	102.2	0.29	0
230.0	0.75	44.8	3.00	3	530.0	1.72	103.2	0.28	0
235.0	0.76	45.7	2.87	3	535.0	1.74	104.1	0.27	0
240.0	0.78	46.7	2.75	3	540.0	1.75	105.1	0.26	0
245.0	0.79	47.7	2.65	3	545.0	1.77	106.1	0.25	0
250.0	0.81	48.7	2.52	3	550.0	1.78	107.0	0.24	0
255.0	0.83	49.6	2.42	3	555.0	1.80	108.0	0.23	0
260.0	0.84	50.6	2.33	3	560.0	1.82	109.0	0.23	0
265.0	0.86	51.6	2.24	3	565.0	1.83	110.0	0.22	0
270.0	0.88	52.6	2.15	2	570.0	1.85	110.9	0.21	0
275.0	0.89	53.5	2.07	2	575.0	1.87	111.9	0.20	0
280.0	0.91	54.5	1.99	2	580.0	1.88	112.9	0.19	0
285.0	0.92	55.5	1.91	2	585.0	1.90	113.9	0.19	0
290.0	0.94	56.4	1.83	2	590.0	1.91	114.8	0.18	0
295.0	0.96	57.4	1.76	2	595.0	1.93	115.8	0.17	0
300.0	0.97	58.4	1.70	2	600.0	1.95	116.8	0.17	0

NOTES : 1. Methodology used Dimensionless Unit Hydrograph.
2. For values of q use Table 4-9 from Flood Hydrology Manual

NRCS DOCUMENTATION



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: NRCS SOIL GROUP FOR O.D.R. WATERSHED

Total Number of Pages (including cover sheet): 5

Total Number of Computer Runs: —

Prepared by: AJT Date: OCT 16, 2008

Checked by: — Date: —

Description and Purpose:

DETERMINE SOIL GROUP FOR O.D.R. WATERSHED

Design Basis/References/Assumptions:

USING website: <http://websurvey.nrcs.usda.gov/app/>

Remarks/Conclusions/Results:

SOIL GROUP FOR ENTIRE WATERSHED

= TYPE B

Calculation Approved by:  Date: 10/24/08
Project Manager

Revision No.: _____ Description of Revision: _____ Approved by: _____

Project Manager/Date

This map displays the Salt Lick River watershed, with the proposed 5F and 7D units highlighted in purple. The watershed boundary is delineated by a blue line. The map includes a coordinate grid with UTM coordinates (407200 to 408600 Easting, 4384400 to 4385800 Northing) and a scale bar in both meters (0 to 900) and feet (0 to 3,000). A north arrow is located in the bottom left corner. Key roads shown include Silverheels Dr, Salt Lick Cir, Ryan Gulch Ct, Ryan Gulch Rd, Cord 1260B, and Dam Rd. The Salt Lick River and Ryan Gulch are labeled. A small area labeled 'W' is also visible within the watershed.

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Units

Soil Ratings

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Political Features

Municipalities

	Cities
	Urban Areas

Water Features

	Oceans
	Streams and Canals

Transportation

	Rails
---	-------

Roads

	Interstate Highways
	US Routes
	State Highways

Local Roads

 Local Roads

 Other Roads

MAP INFORMATION

Original soil survey map sheets were prepared at publication scale. Viewing scale and printing scale, however, may vary from the original. Please rely on the bar scale on each map sheet for proper map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
Coordinate System: UTM Zone 13N

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Summit County Area, Colorado
Survey Area Data: Version 4, Jan 30, 2008
Date(s) aerial images were photographed: 1999

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — Summit County Area, Colorado				
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
5F	Frisco-Peeler complex, 25 to 65 percent slopes	B	207.9	95.3%
7D	Grenadier gravelly loam, 6 to 15 percent slopes	B	3.0	1.4%
W	Water		7.3	3.3%
Totals for Area of Interest (AOI)			218.2	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Lower



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: NRCS CURVE NUMBER

Total Number of Pages (including cover sheet): 2

Total Number of Computer Runs: —

Prepared by: AST Date: OCT 16, 2008

Checked by: — Date: —

Description and Purpose:

CURVE NUMBER EQUIVALENT FOR ODR WATERSHED

Design Basis/References/Assumptions:

- TYPE B SOIL GROUP
- ASSUME ALL TREE'S IN WATERSHED REMOVED
 - DUE TO PINE BEETLE OR FIRE
- CHOOSE HIGHEST CN FOR TYPE B SOILS

Remarks/Conclusions/Results:

- USE CN OF 86 FOR MOST CONSERVATIVE CASE

Calculation Approved by: _____
Project Manager Date

Revision No.: _____ Description of Revision: _____ Approved by: _____

Project Manager/Date

Table 2-2b Runoff curve numbers for cultivated agricultural lands ^{1/}

Cover description			Curve numbers for hydrologic soil group			
Cover type	Treatment ^{2/}	Hydrologic condition ^{3/}	A	B	C	D
Fallow	Bare soil	—	77	86	91	94
	Crop residue cover (CR)	Poor	76	85	90	93
		Good	74	83	88	90
Row crops	Straight row (SR)	Poor	72	81	88	91
		Good	67	78	85	89
	SR + CR	Poor	71	80	87	90
		Good	64	75	82	85
	Contoured (C)	Poor	70	79	84	88
		Good	65	75	82	86
	C + CR	Poor	69	78	83	87
		Good	64	74	81	85
	Contoured & terraced (C&T)	Poor	66	74	80	82
		Good	62	71	78	81
	C&T+ CR	Poor	65	73	79	81
		Good	61	70	77	80
Small grain	SR	Poor	65	76	84	88
		Good	63	75	83	87
	SR + CR	Poor	64	75	83	86
		Good	60	72	80	84
	C	Poor	63	74	82	85
		Good	61	73	81	84
	C + CR	Poor	62	73	81	84
		Good	60	72	80	83
	C&T	Poor	61	72	79	82
		Good	59	70	78	81
Close-seeded or broadcast legumes or rotation meadow	SR	Poor	66	77	85	89
		Good	58	72	81	85
	C	Poor	64	75	83	85
		Good	55	69	78	83
	C&T	Poor	63	73	80	83
		Good	51	67	76	80

¹ Average runoff condition, and $I_a=0.2s$ ² Crop residue cover applies only if residue is on at least 5% of the surface throughout the year.³ Hydraulic condition is based on combination factors that affect infiltration and runoff, including (a) density and canopy of vegetative areas, (b) amount of year-round cover, (c) amount of grass or close-seeded legumes, (d) percent of residue cover on the land surface (good $\geq 20\%$), and (e) degree of surface roughness.

Poor: Factors impair infiltration and tend to increase runoff.

Good: Factors encourage average and better than average infiltration and tend to decrease runoff.



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: NRC5 TIME OF CONCENTRATION

Total Number of Pages (including cover sheet): 3

Total Number of Computer Runs: —

Prepared by: AJT Date: OCT 16, 2008

Checked by: — Date: —

Description and Purpose:

DETERMINE TIME OF CONCENTRATION (T_c) FOR THE TWO O.D.R. SUBBASINS

Design Basis/References/Assumptions:

Remarks/Conclusions/Results:

- ASSUME $T_c = 5$ minutes for Reservoir

Calculation Approved by: _____
Project Manager Date

Revision No.: _____ Description of Revision: _____ Approved by: _____

Project Manager/Date

BASIN NE	
Sheet Flow (Applicable to Tc only) Segment ID	
1. Surface description (Table 3-1)	Fallow (no residue)
2. Manning's roughness coeff., n (Table 3-1)	0.05
3. Flow length, L (total L < 100 ft) ft	300
4. Two-year 24-hour rainfall, P2..... in	1.16
5. Land slope, s ft/ft	0.08
top elevation	9,349
bottom elevation	9,324
6. Compute Tt hr	0.15
Shallow Concentrated Flow	
7. Surface description (paved or unpaved)	unpaved
8. Flow length, L ft	554
9. Watercourse slope, s ft/ft	0.24
top elevation	9,324
bottom elevation	9,191
10. Average velocity, V (Figure 3-1) ft/s	7.92
11. Compute Tt hr	0.019
Tc	0.173
No channelized flow	
SCS lag time (tc x 0.6)	0.104

BASIN SW	
Sheet Flow (Applicable to Tc only) Segment ID	
1. Surface description (Table 3-1)	Fallow (no residue)
2. Manning's roughness coeff., n (Table 3-1)	0.05
3. Flow length, L (total L < 100 ft) ft	300
4. Two-year 24-hour rainfall, P2..... in	1.16
5. Land slope, s ft/ft	0.12
top elevation	9,337
bottom elevation	9,300
6. Compute Tt hr	0.13
Shallow Concentrated Flow	
7. Surface description (paved or unpaved)	unpaved
8. Flow length, L ft	1148
9. Watercourse slope, s ft/ft	0.10
top elevation	9,300
bottom elevation	9,191
10. Average velocity, V (Figure 3-1) ft/s	4.98
11. Compute Tt hr	0.064
Tc	0.195
No channelized flow	
SCS lag time (tc x 0.6)	0.117

HMR-49
PMP STORM DETERMINATION



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: LOCAL STORM PMP COMPUTATION

Total Number of Pages (including cover sheet): 7

Total Number of Computer Runs: N/A

Prepared by: AJT Date: OCT 6, 2008

Checked by: _____ Date: _____

Description and Purpose:

DETERMINE LOCAL PMP

Design Basis/References/Assumptions:

HMR-49, PMP ESTIMATES, COLORADO RIVER

Remarks/Conclusions/Results:

ONE HOUR INCREMENTS

0.25 0.58 8.4 ^{1.18} 1.18 0.34 0.17

(FOR INPUT INTO HEC-1 / HEC-HMS)

Calculation Approved by:  Date: 10/24/08

Project Manager

Date

Revision No.:

Description of Revision:

Approved by:

Project Manager/Date

Table 6.3A.--Local-storm PMP computation, Colorado River, Great Basin and California drainages. For drainage average depth PMP. Go to table 6.3B if areal variation is required.

Drainage OLD DILLON RESERVOIR Area 0.05 mi² (km²)
 Latitude 39° 36' 40.14" Longitude 106° 04' 17.53" Minimum Elevation 9200 ft (m)

39.611235° 106.07127°

Steps correspond to those in sec. 6.3A.

1. Average 1-hr 1-mi² (2.6-km²) PMP for 10.5 in. (mm)

2. a. Reduction for elevation. [No adjustment for elevations up to 5,000 feet (1,524 m): 5% decrease per 1,000 feet (305 m) above 5,000 feet (1,524 m)]. 8.0 %

b. Multiply step 1 by step 2a. 8.4 in. (mm)

3. Average 6/1-hr ratio for drainage [fig. 4.7]. 1.27

	Duration (hr)									
	1/4	1/2	3/4	1	2	3	4	5	6	
4. Durational variation for 6/1-hr ratio of step 3 [table 4.4].	<u>74</u>	<u>89</u>	<u>95</u>	<u>100</u>	<u>114</u>	<u>121</u>	<u>125</u>	<u>128</u>	<u>130</u>	%

5. 1-mi ² (2.6-km ²) PMP for indicated durations [step 2b X step 4].	<u>6.22</u>	<u>7.48</u>	<u>7.98</u>	<u>8.4</u>	<u>9.58</u>	<u>10.16</u>	<u>10.5</u>	<u>10.75</u>	<u>10.92</u>	in. (mm)
---	-------------	-------------	-------------	------------	-------------	--------------	-------------	--------------	--------------	----------

6. Areal reduction [fig. 4.9].					<u>100%</u>				%
--------------------------------	--	--	--	--	-------------	--	--	--	---

7. Areal reduced PMP [steps 5 X 6].	<u>6.22</u>	<u>7.48</u>	<u>7.98</u>	<u>8.40</u>	<u>9.58</u>	<u>10.16</u>	<u>10.50</u>	<u>10.75</u>	<u>10.92</u>	in. (mm)
-------------------------------------	-------------	-------------	-------------	-------------	-------------	--------------	--------------	--------------	--------------	----------

8. Incremental PMP [successive subtraction in step 7].

				<u>8.4</u>	<u>1.18</u>	<u>0.58</u>	<u>0.34</u>	<u>0.25</u>	<u>0.17</u>	in. (mm)
--	--	--	--	------------	-------------	-------------	-------------	-------------	-------------	----------

6.22 1.26 0.5 0.42 } 15-min. increments

9. Time sequence of incremental PMP according to:

Hourly increments [table 4.7].

0.25 0.58 8.4 1.18 0.34 0.17 in. (mm)

Four largest 15-min. increments [table 4.8].

6.22 1.26 0.5 0.42 in. (mm)

10.92" total

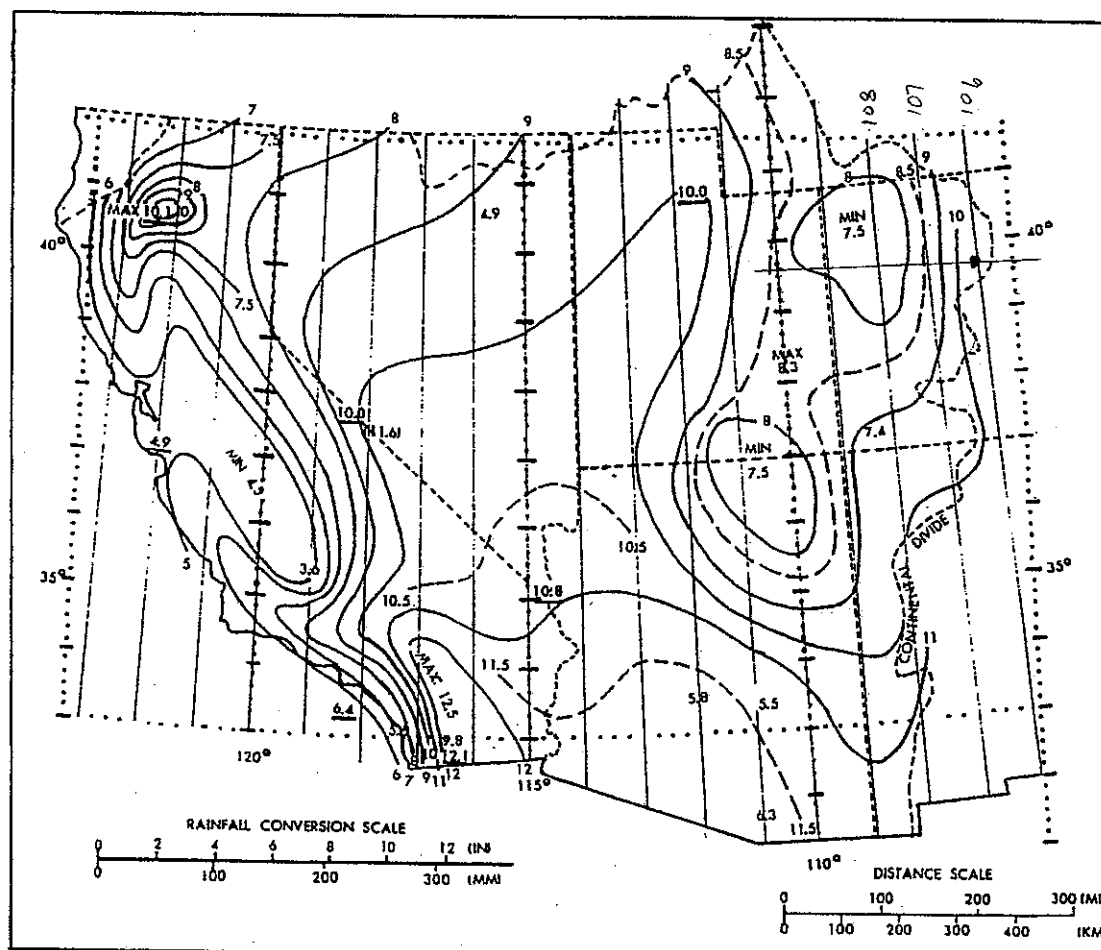


Figure 4.5--Local-storm PMP for 1 mi^2 (2.6 km^2) 1 hr. Directly applicable for locations between sea level and 5000 ft (1524 m). Elevation adjustment must be applied for locations above 5000 ft.

events. In contrast to figure 4.4, figure 4.5 maintains a maximum between these two locations. There is no known meteorological basis for a different solution. The analysis suggests that in the northern portion of the region maximum PMP occurs between the Sierra Nevada on the west and the Wasatch range on the east.

A discrete maximum (> 10 inches, 254 mm) occurs at the north end of the Sacramento Valley in northern California because the northward-flowing moist air is increasingly channeled and forced upslope. Support for this PMP center comes from the Newton, Kennett, and Red Bluff storms (fig. 4.1). Although the analysis in this region appears to be an extension of the broad maximum through the center of the Southwestern Region, it does not indicate the direction of moist inflow. The pattern has evolved primarily as a result of attempts to tie plotted maxima into a reasonable picture while considering inflow directions, terrain effects, and moisture potential.

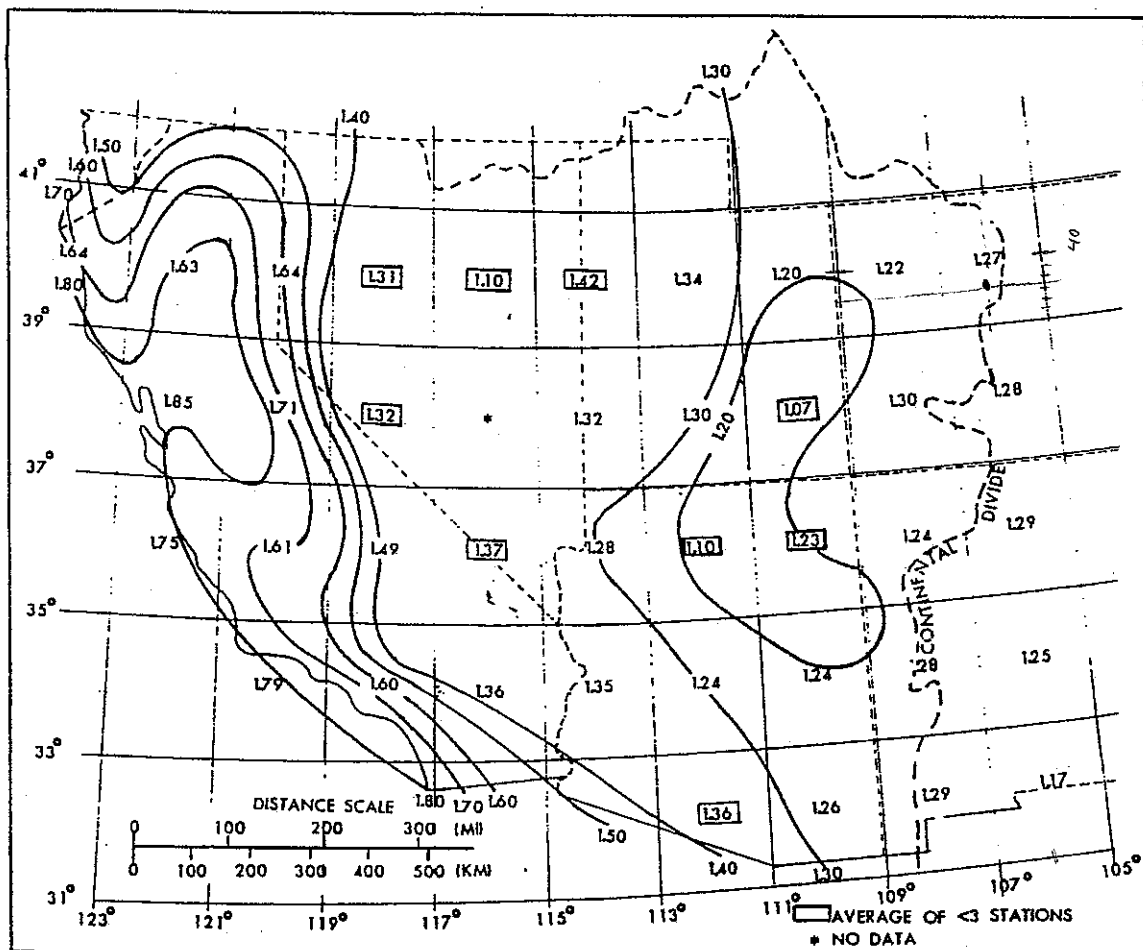
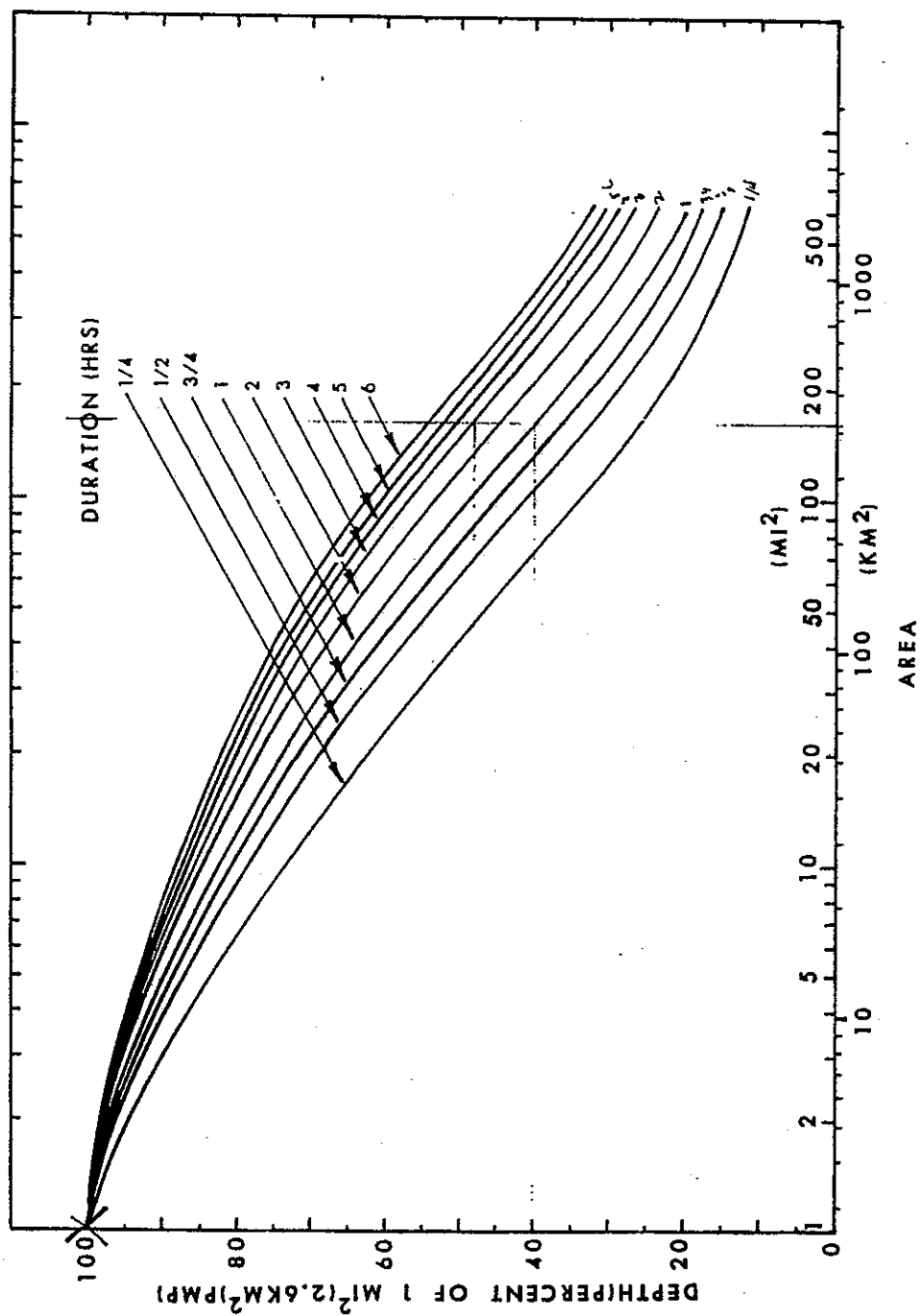


Figure 4.7.--Analysis of 6/1-hr ratios of averaged maximum station data (plotted at midpoints of a 2° latitude-longitude grid).

establish the basic depth-duration curve, then structure a variable set of depth-duration curves to cover the range of 6/1-hr ratios that are needed.

Three sets of data were considered for obtaining a base relation (see table 4.3 for depth-duration data).

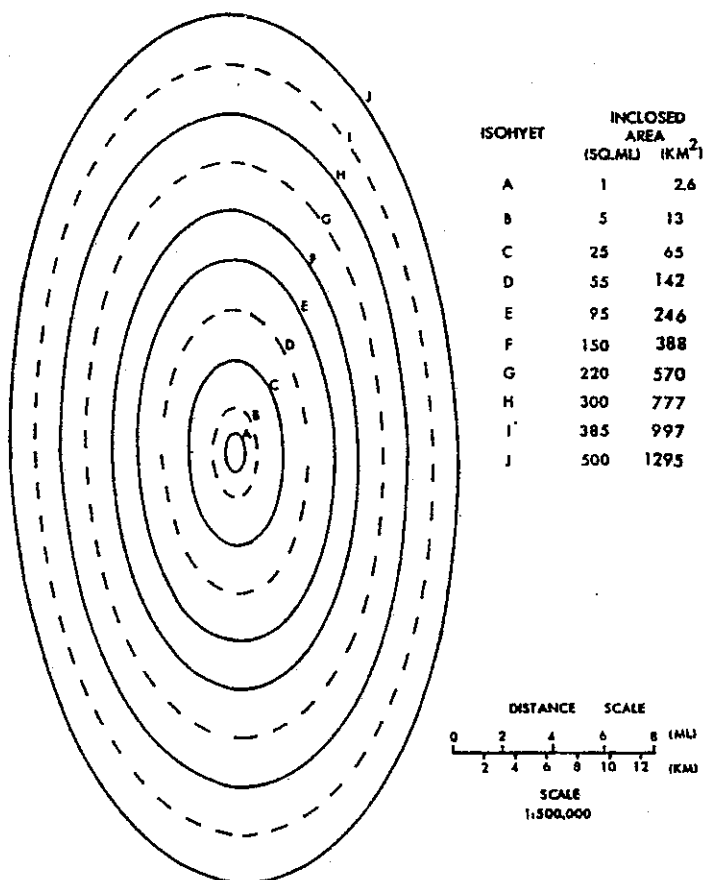
- a. An average of depth-duration relations from each of 17 greatest 3-hr rains from summer storms (1940-49) in Utah (U. S. Weather Bureau 1951b) and in unpublished tabulations for Nevada and Arizona (1940-63). The 3-hr amounts ranged from 1 to 3 inches (25 to 76 mm) in these events.
- b. An average depth-duration relation from 14 of the most extreme short-duration storms listed in Storm Rainfall (U. S. Army, Corps of Engineers 1945-). These storms come from Eastern and Central States and have 3-hr amounts of 5 to 22 inches (127 to 559 mm).



$$AREA = 0.05 \text{ mi}^2$$

Figure 4.9: --Adopted depth-area relations for local-storm PMP.

Figure 4.10.--Idealized
local-storm isohyetal
pattern.



storm period. The sequence of hourly incremental PMP for the Southwest 6-hr thunderstorm in accord with this study is presented in column 2 of table 4.7. A small variation from this sequence is given in Engineering Manual 1110-2-1411 (U. S. Army, Corps of Engineers 1965). The latter, listed in column 3 of table 4.7, places greater incremental amounts somewhat more toward the end of the 6-hr storm period. In application, the choice of either of these distributions is left to the user since one may prove to be more critical in a specific case than the other.

Table 4.7.--Time sequence for hourly incremental PMP in 6-hr storm

Increment	HMR No. 5 ¹	EM1110-2-1411 ²
	Sequence Position	
Largest hourly amount	Third	Fourth
2nd largest	Fourth	Third
3rd largest	Second	Fifth
4th largest	Fifth	Second
5th largest	First	Last
least	Last	First

¹U. S. Weather Bureau 1947.

²U. S. Corps of Engineers 1952.

Also of importance is the sequence of the four 15-min incremental PMP values. We recommend a time distribution, table 4.8, giving the greatest intensity in the first 15-min interval (U.S. Weather Bureau 1947). This is based on data from a broad geographical region. Additional support for this time distribution is found in the reports of specific storms by Keppell (1963) and Osborn and Renard (1969).

Table 4.8.--Time sequence for 15-min incremental PMP within 1 hr.

Increment	Sequence Position
Largest 15-min amount	First
2nd largest	Second
3rd largest	Third
least	Last

4.8 Seasonal Distribution

The time of the year when local-storm PMP is most likely is of interest. Guidance was obtained from analysis of the distribution of maximum 1-hr thunderstorm events through the warm season at the recording stations in Utah, Arizona, and in southern California (south of 37°N and east of the Sierra Nevada ridgeline). The period of record used was for 1940-72 with an average record length for the stations considered of 27 years. The month with the one greatest thunderstorm rainfall for the period of record at each station was noted. The totals of these events for each month, by States, are shown in table 4.9.

Table 4.9.--Seasonal distribution of thunderstorm rainfalls.

(The maximum event at each of 108 stations, period of record 1940-72.)

	Month						No. of Cases
	M	J	J	A	S	O	
Utah	1	5	9	14	5		34
Arizona		4	16	19	4		43
S. Calif.*		14	10	7			31
No. of cases/mo.	1	23	35	40	9	0	

*South of 37°N and east of Sierra Nevada ridgeline.



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: GENERAL STORM PMP CALCULATION

Total Number of Pages (including cover sheet): _____

Total Number of Computer Runs: _____

Prepared by: AJT Date: OCT 6, 2008

Checked by: _____ Date: _____

Description and Purpose:

DETERMINE GENERAL STORM PMP FOR
JULY, AUGUST, SEPTEMBER; OCTOBER

Design Basis/References/Assumptions:

HMR-49

Remarks/Conclusions/Results:

DETERMINED 6, 12, 18, 24, 48, 72 hr RAINFALL AMOUNTS

- USED CURVE FIT TO DETERMINE 5min 30min, 1hr, 2hr, 3hr

- FOR INPUT INTO HEC-1/HEC-HMS

Calculation Approved by: [Signature] Date: 10/24/08
Project Manager Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____

Project Manager/Date

Table 6.1.—General-storm PMP computations for the Colorado River and Great basin

Drainage OLD DILLON RES Area 0.05 mi² (km²)
 Latitude 39°36", Longitude 106°04' of basin center

Month JULY

Step	Duration (hrs)					
	6	12	18	24	48	72

A. Convergence PMP

- Drainage average value from one of figures 2.5 to 2.16 15 in. (mm)
- Reduction for barrier-elevation [fig. 2.18] 30 %
- Barrier-elevation reduced PMP [step 1 X step 2] 4.5 in. (mm)
- Durational variation [figs. 2.25 to 2.27 and table 2.7].

69	86	94	100	115	121	%
----	----	----	-----	-----	-----	---
- Convergence PMP for indicated durations [steps 3 X 4]

3.1	3.9	4.2	4.5	5.2	5.4	in. (mm)
-----	-----	-----	-----	-----	-----	----------
- Incremental 10 mi² (26 km²) PMP [successive subtraction in step 5]

3.1	0.8	0.3	0.3	0.7	0.2	in. (mm)
-----	-----	-----	-----	-----	-----	----------
- Areal reduction [select from figs. 2.28 and 2.29]

100	100	100	100	100	100	%
-----	-----	-----	-----	-----	-----	---
- Areally reduced PMP [step 6 X step 7]

3.1	0.8	0.3	0.3	0.7	0.2	in. (mm)
-----	-----	-----	-----	-----	-----	----------
- Drainage average PMP [accumulated values of step 8]

3.1	3.9	4.2	4.5	5.2	5.4	in. (mm)
-----	-----	-----	-----	-----	-----	----------

B. Orographic PMP

- Drainage average orographic index from figure 3.11a to d. 8.5 in. (mm)
- Areal reduction [figure 3.20] 100 %
- Adjustment for month [one of figs. 3.12 to 3.17] 107 %
- Areally and seasonally adjusted PMP [steps 1 X 2 X 3] 8.67 in. (mm)
- Durational variation [table 3.6]

6	12	18	24	48	72
30	57	80	100	158	186
3.67	3.9				
- Orographic PMP for given durations [steps 4 X 5]

2.6	4.9	6.9	8.7	13.7	16.1	in. (mm)
-----	-----	-----	-----	------	------	----------

C. Total PMP

- Add steps A9 and B6

5.7	8.8	11.1	13.2	18.9	21.5	in. (mm)
-----	-----	------	------	------	------	----------
- PMP for other durations from smooth curve fitted to plot of computed data.
- Comparison with local-storm PMP (see sec. 6.3).

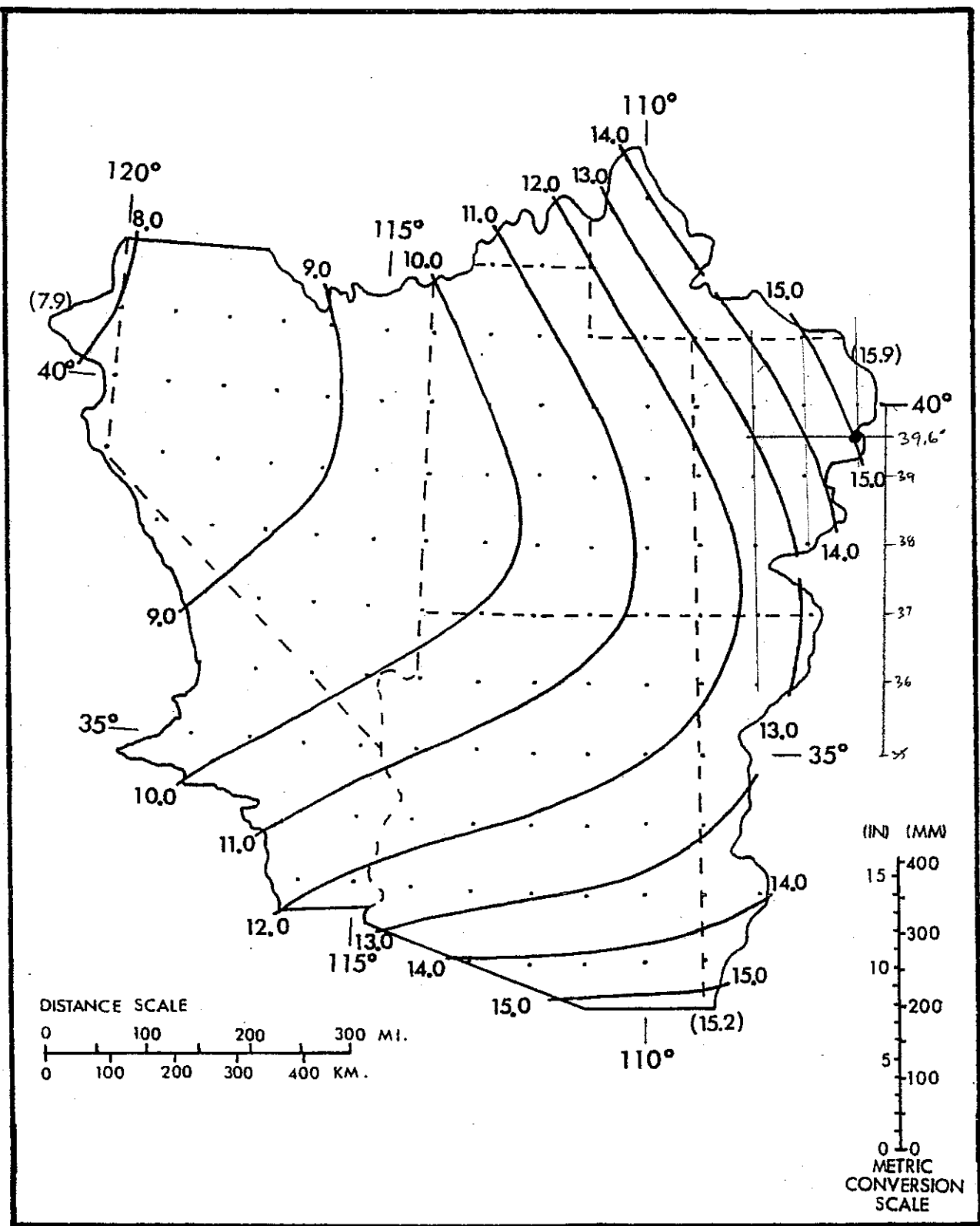


Figure 2.11.--1000-mb (100-kPa) 24-hr convergence PMP (inches) for 10 mi² (26 km²) for July. Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

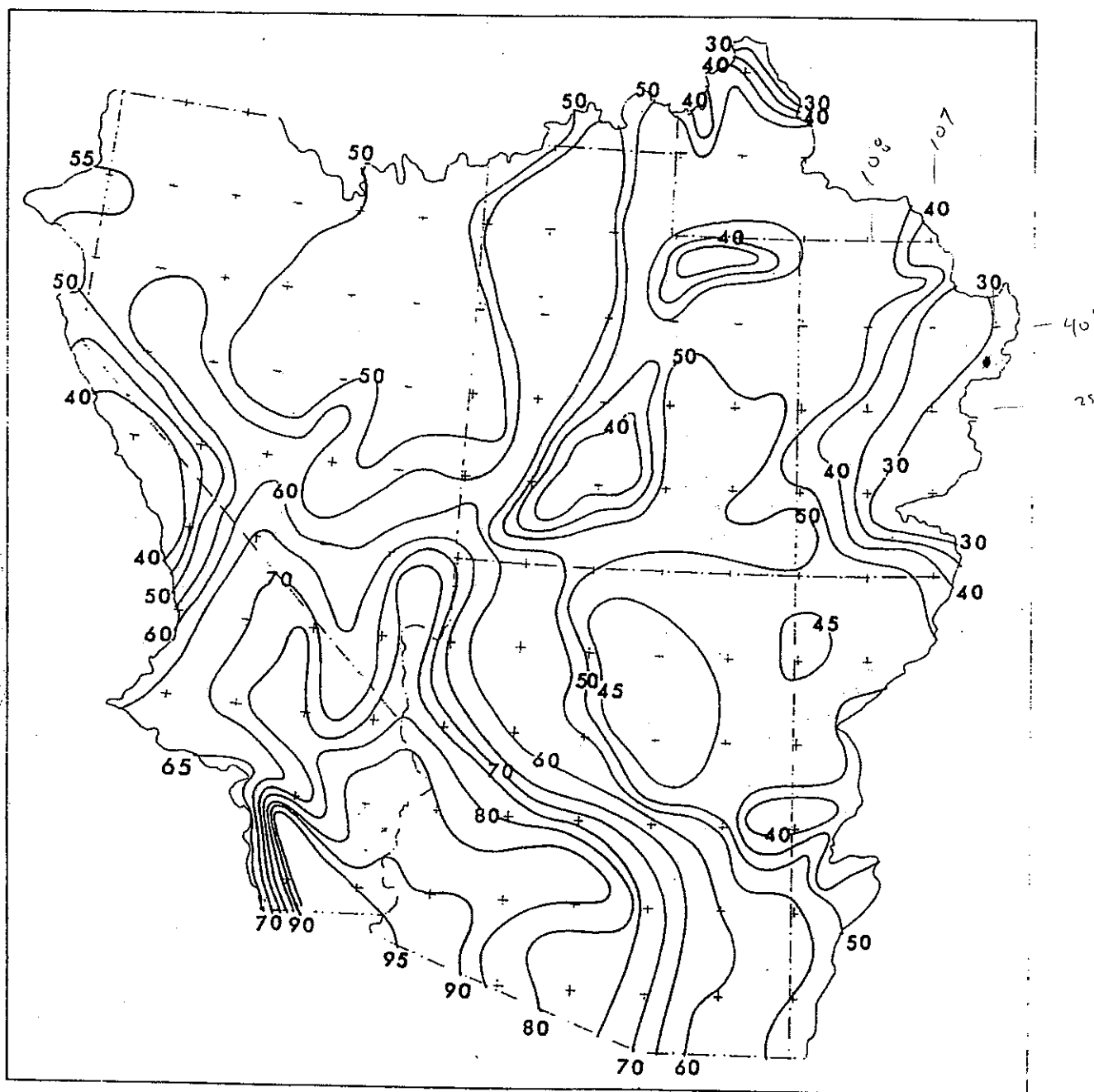
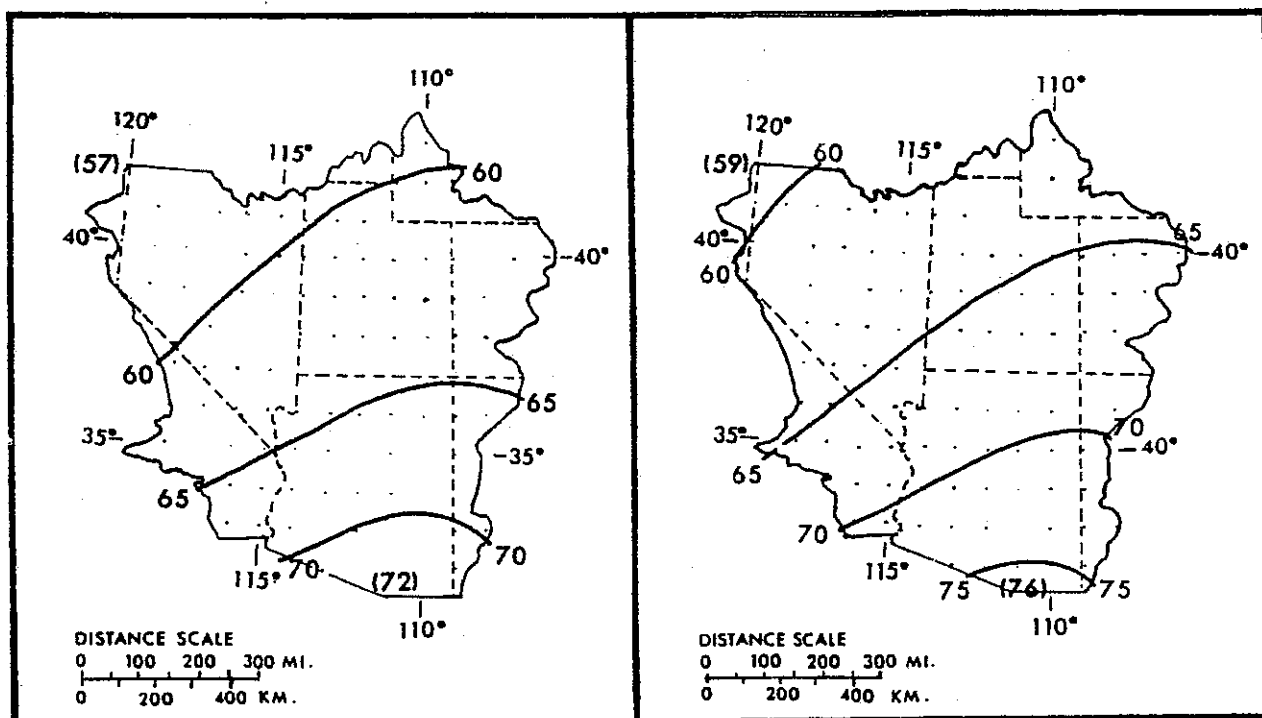
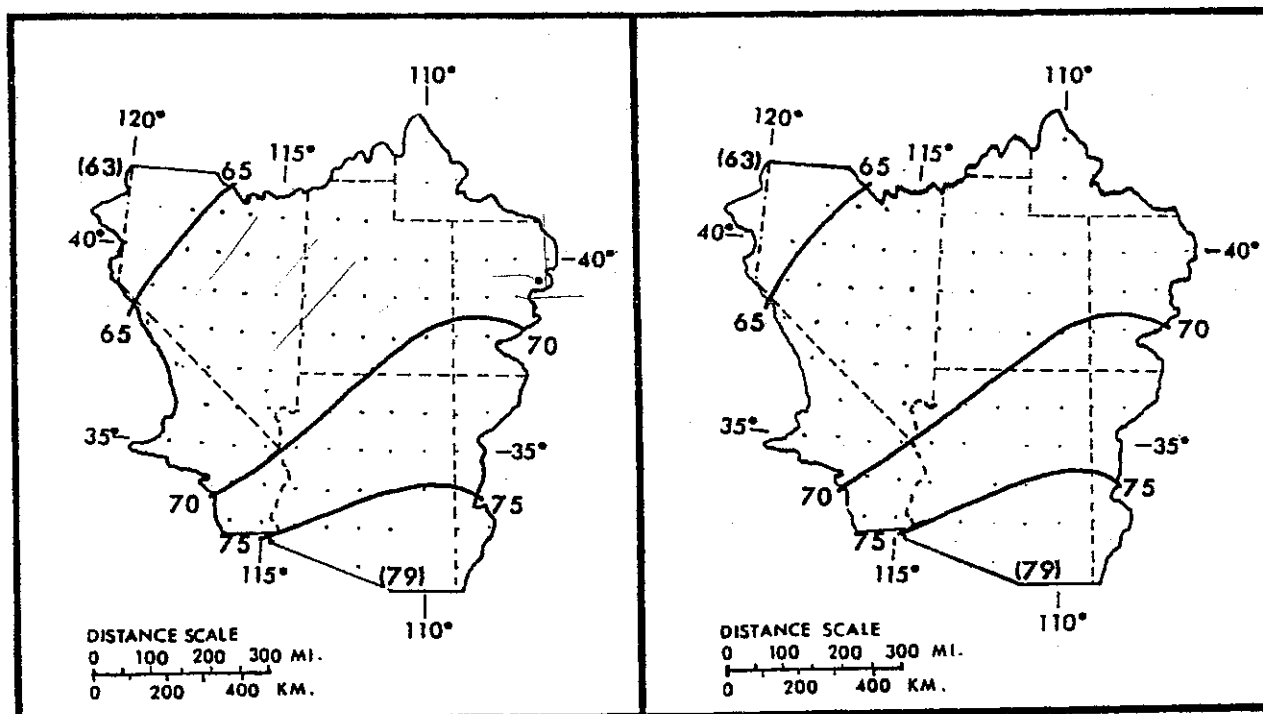


Figure 2.18.--Percent of 1000-mb (100-kPa) convergence PMP resulting from effective elevation and barrier considerations. Isolines drawn for every five percent.



May

June



July

August

Figure 2.26.--Regional variation of 6/24-hr ratios by month (percent). Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

For the range of 6/24-hr ratios included in figures 2.25 to 2.27, depth-duration values in percent of 24-hr amounts are found in table 2.7. The regional ratio maps, and the depth-duration curves presented in figure 2.20 were used in adjusting the major storm data to 24-hr amounts listed in table 2.1.

Table 2.7.—Durational variation of convergence PMP (in percent of 24-hr amount).

Duration (Hrs)						Duration (Hrs)					
6	12	18	24	48	72	6	12	18	24	48	72
50	76	90	100	129	150	66	84	93	100	116	124
51	77	90	100	128	148	67	85	94	100	116	123
52	77	90	100	127	146	68	85	94	100	115	122
53	77	91	100	127	144	69	86	94	100	115	121
54	78	91	100	126	142						
55	78	91	100	125	140	70	87	94	100	114	120
56	79	91	100	124	138	71	87	95	100	114	119
57	79	92	100	123	137	72	88	95	100	113	118
58	80	92	100	122	135	73	88	95	100	113	118
59	80	92	100	121	134	74	89	95	100	112	117
						75	89	96	100	112	116
60	81	92	100	120	132	76	90	96	100	111	115
61	81	92	100	120	131	77	90	96	100	110	114
62	82	93	100	119	129	78	91	96	100	110	114
63	82	93	100	118	128	79	92	97	100	109	113
64	83	93	100	117	126						
65	84	93	100	117	125	80	92	97	100	109	113

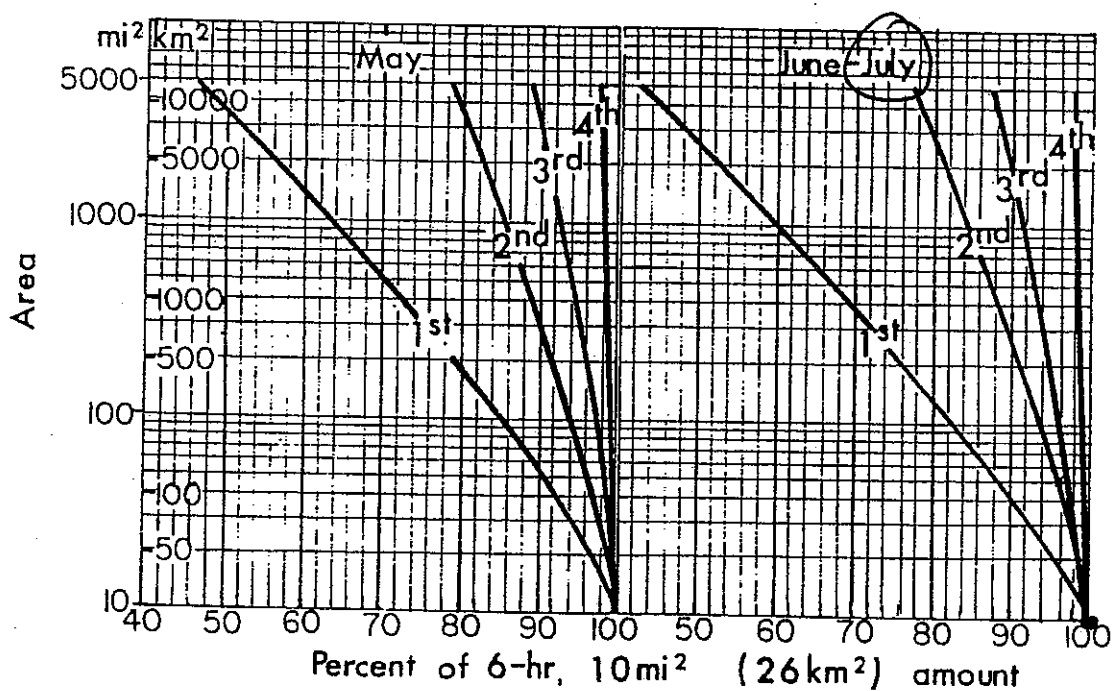
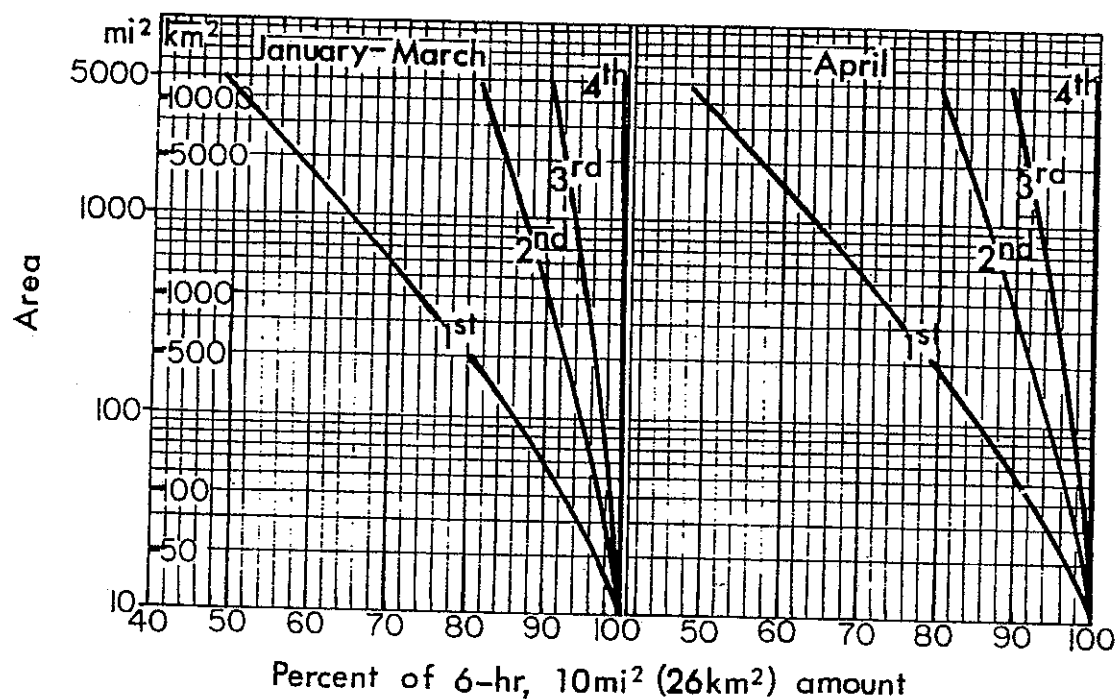
Note: For use, enter first column (6 hr) with 6/24-hr ratio from figures 2.25 to 2.27.

2.5 Areal Reduction for Basin Size

For operational use, basin average values of convergence PMP are needed rather than 10-mi² (26-km²) values. Preferably, the method for reducing 10-mi² (26-km²) values to basin average rainfalls should be derived from depth-area relations of storms in the region. However, all general storms in the region include large proportions of orographic precipitation.

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Figures 2.28 and 2.29 give depth-area relations that reduce 10-mi² (26-km²) convergence PMP for basin sizes up to 5,000 mi² (12,950 km²) for each month. Areal variations are given for the 4 greatest (1st to 4th) 6-hr PMP increments. After the 4th increment no reduction for basin size is required. Application of these figures will become clear through consideration of an example of PMP computation in chapter 6.



BASIN AREA = 0.05mi^2

Figure 2.28 --Depth-area variation for convergence PMP for first to fourth 6-hr increments.

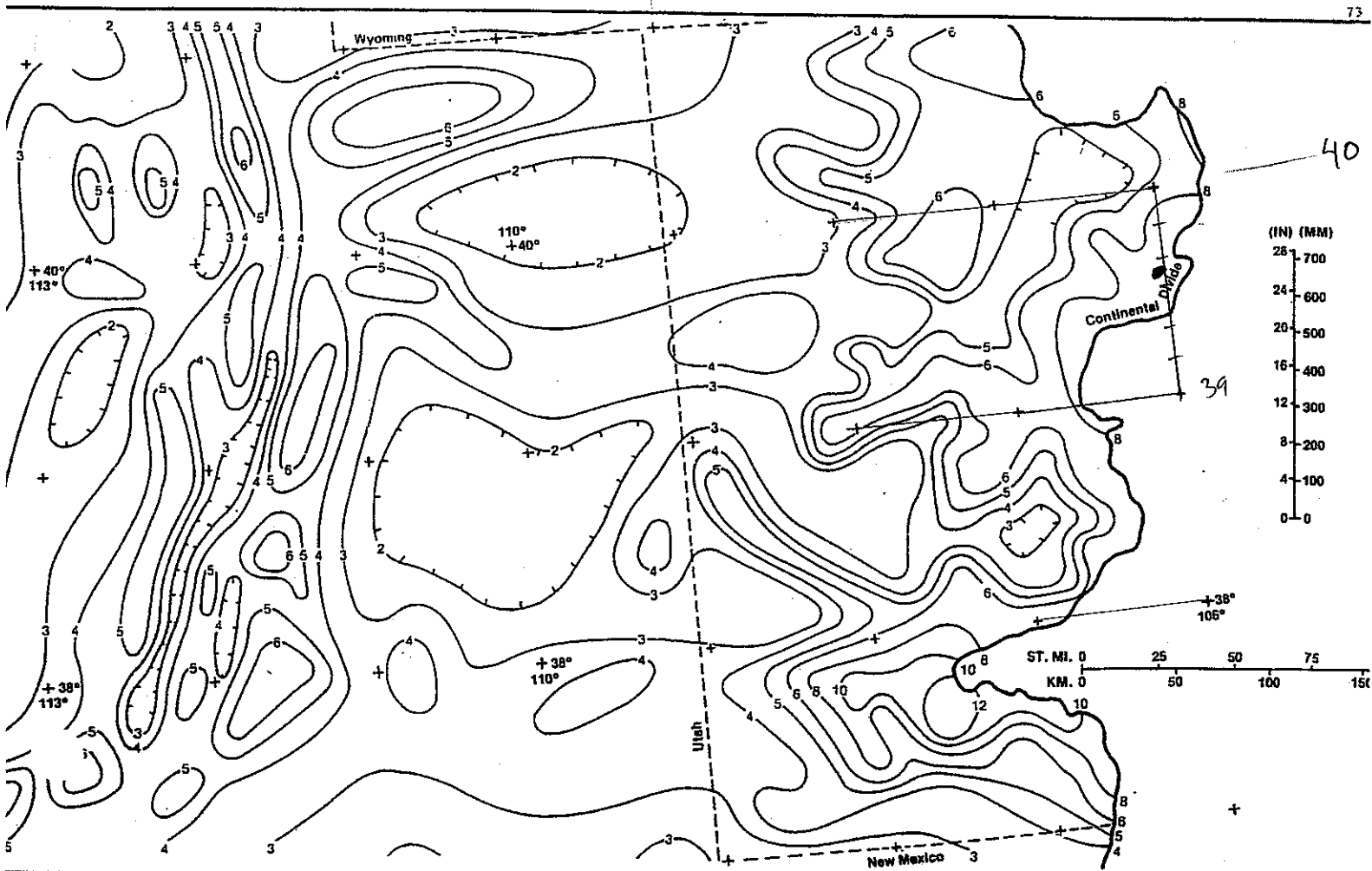


FIGURE 3.11b (Revised) — 10-mi² (26-km²) 24-hr orographic PMP index map (inches), north-central section.

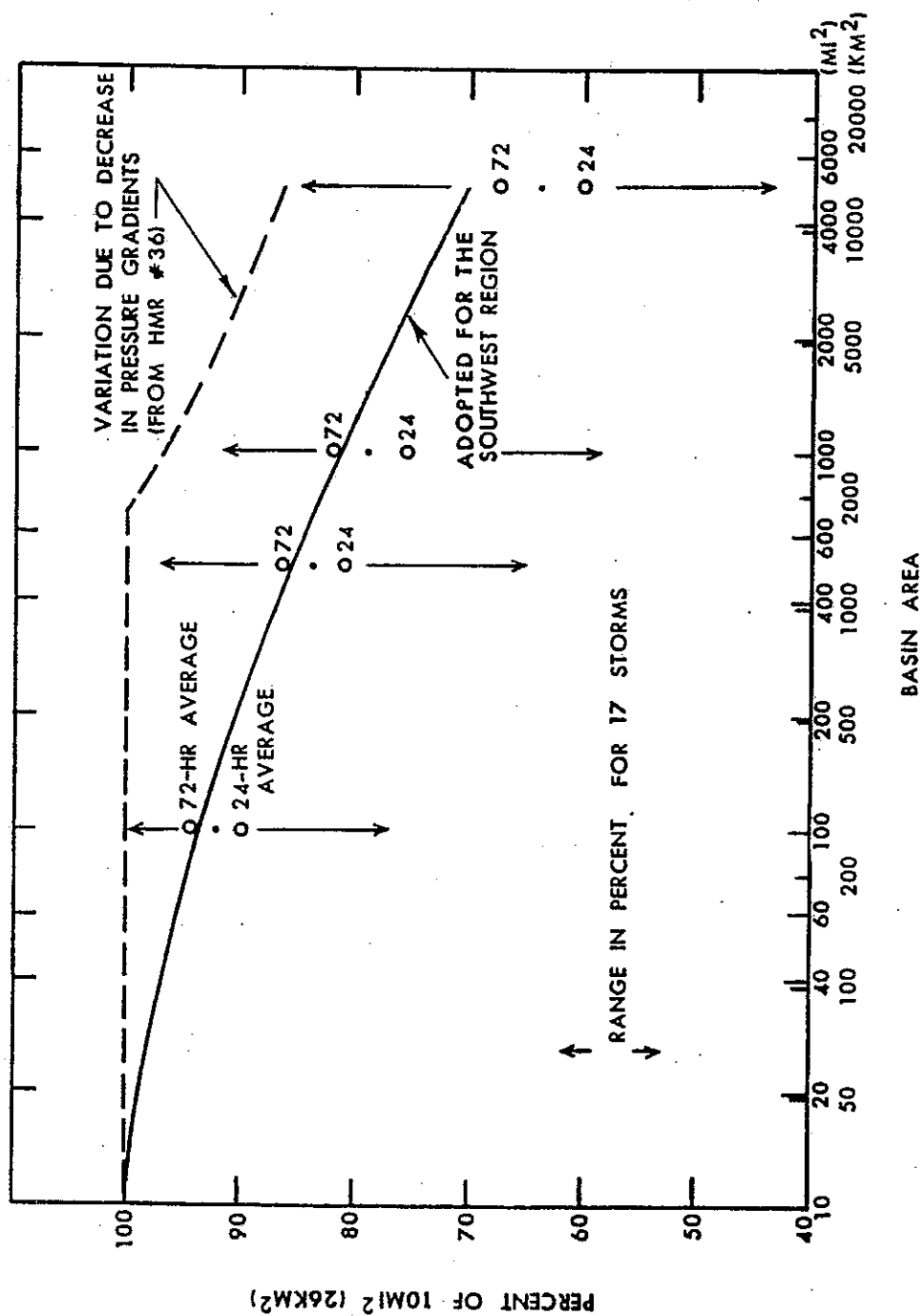
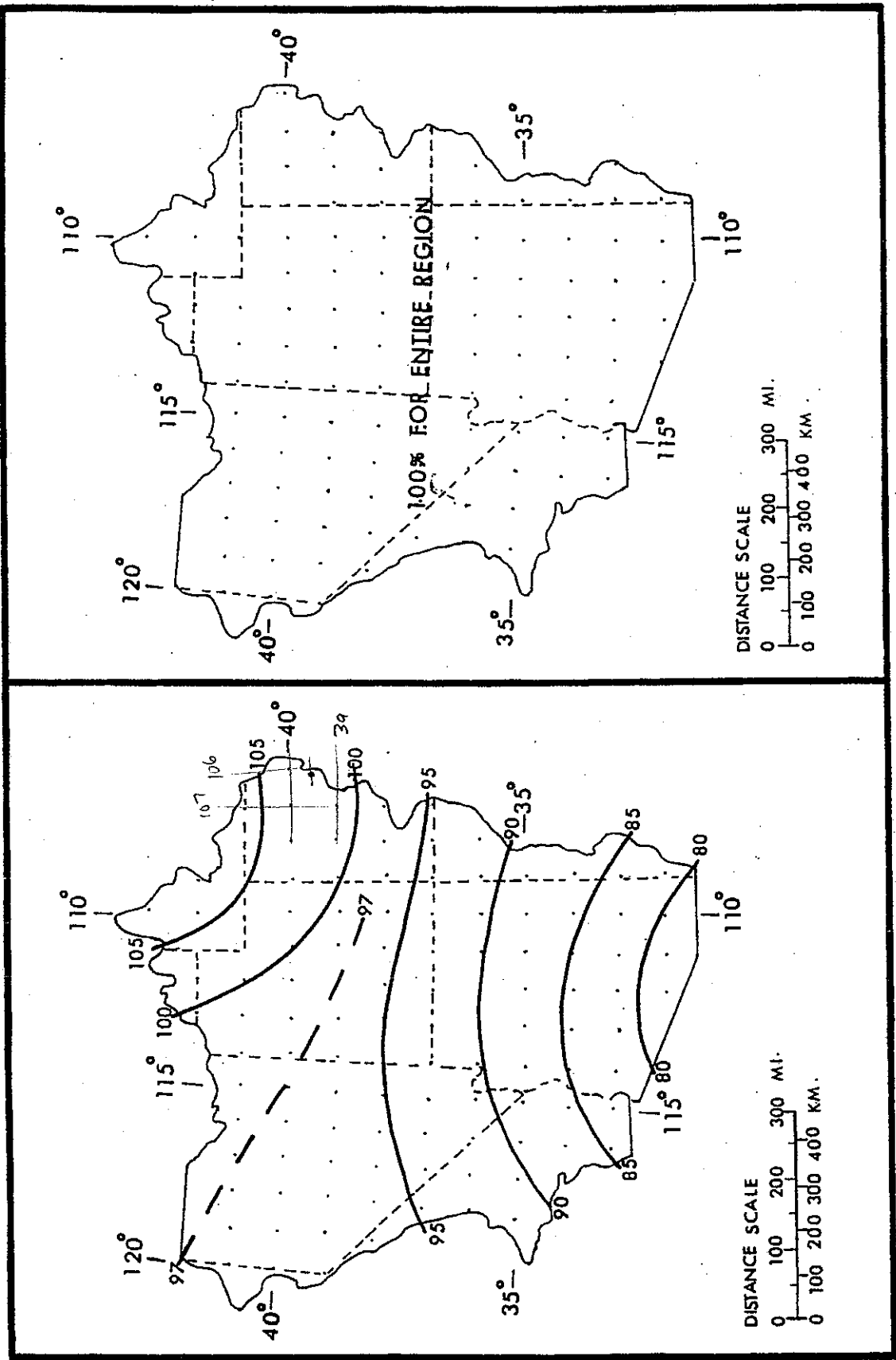


Figure 3.20.---Variation of orographic PMP with basin size.



July

August

Figure 3.15. ---Seasonal variation in 10-mi^2 (26-km^2) 24-hr orographic PMP for the study region (in percent of values in figure 3.11).

Table 3.9.--Durational variation of orographic PMP

Latitude °N	Percent of 24-hr value					
	6 hr	12	18	24	48	72
42	28	55	79	100	161	190
41	29	56	79	100	160	189
39.6° — 40	30	57	80	100	159	187
39	30	57	80	100	157	185
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37	32	59	81	100	152	177
36	33	60	82	100	149	172
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33	36	63	84	100	139	157
32	37	64	84	100	135	152
31	39	66	85	100	132	146

4. LOCAL-STORM PMP FOR THE SOUTHWESTERN REGION AND CALIFORNIA

4.1 Introduction

This chapter provides generalized estimates of local or thunderstorm probable maximum precipitation. By "generalized" is meant that mapped values are given from which estimates of PMP may be determined for any selected drainage.

4.1.1 Region of Interest

Local-storm PMP was not included in the "Interim Report, Probable Maximum Precipitation in California" (HMR No. 36). During the formulation of the present study, we decided that the local-storm part of the study should include California west of the Sierra Nevada. It was also noted that PMP for summer thunderstorms was not considered west of the Cascade Divide in the Northwestern Region (HMR No. 43). As stated in the latter report, "No summer thunderstorms have been reported there (west of the Divide) of an intensity of those to the east, for which the moisture source is often the Gulf of Mexico or Gulf of California. The Cascade Divide offers an additional barrier to such moisture inflows to coastal areas where, in addition, the Pacific Ocean to the west has a stabilizing influence on the air to hinder the occurrence of intense summer local storms." Therefore, it was necessary to establish some continuation of the Cascade Divide into California so that the local-storm PMP definition would have continuity between the two regions.

The stabilizing influence of the Pacific air is at times interrupted by the warm moist tropical air from the south pushing into California, although it is difficult to determine where the limit of southerly flow occurs. General storms having the tropical characteristic of excessive thunderstorm rains are observed as far north as the northern end of the Sacramento Valley. Thus, a northern boundary has been selected for this study, excluding that portion of

Chart Title

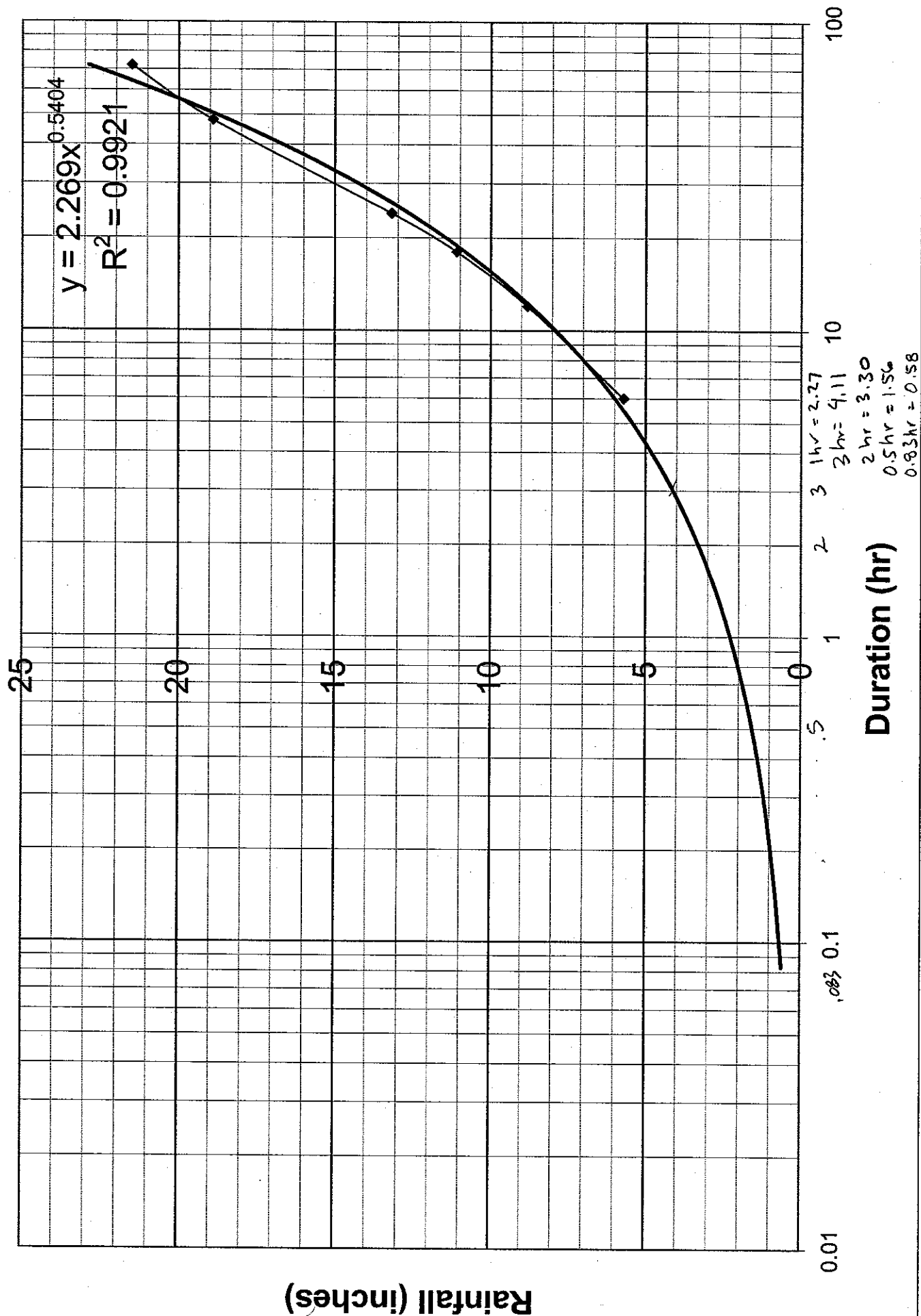


Table 6.1.--General-storm PMP computations for the Colorado River and Great basin

Drainage OLD DILLON RES Area 0.05 mi² (km²)
 Latitude 39°36', Longitude 106°04' of basin center
 Month AUGUST

Step	Duration (hrs)					
	6	12	18	24	48	72

A. Convergence PMP

- Drainage average value from one of figures 2.5 to 2.16 15.3 in. (mm)
- Reduction for barrier-elevation [fig. 2.18] 30%
- Barrier-elevation reduced PMP [step 1 X step 2] 4.6 in. (mm)
- Durational variation [figs. 2.25 to 2.27 and table 2.7].

69	86	94	100	115	121
----	----	----	-----	-----	-----
- Convergence PMP for indicated durations [steps 3 X 4]

3.2	4.0	4.3	4.6	5.3	5.6
-----	-----	-----	-----	-----	-----

in. (mm)
- Incremental 10 mi² (26 km²) PMP [successive subtraction in step 5]

3.2	0.8	0.3	0.3	0.7	0.3
-----	-----	-----	-----	-----	-----

in. (mm)
- Areal reduction [select from figs. 2.28 and 2.29]

100	100	100	100	100	100
-----	-----	-----	-----	-----	-----
- Areally reduced PMP [step 6 X step 7]

3.2	0.8	0.3	0.3	0.7	0.3
-----	-----	-----	-----	-----	-----

in. (mm)
- Drainage average PMP [accumulated values of step 8]

3.2	4.0	4.3	4.6	5.3	5.6
-----	-----	-----	-----	-----	-----

in. (mm)

B. Orographic PMP

- Drainage average orographic index from figure 3.11a to d. 8.5 in. (mm)
- Areal reduction [figure 3.20] 100%
- Adjustment for month [one of figs. 3.12 to 3.17] 100%
- Areally and seasonally adjusted PMP [steps 1 X 2 X 3] 8.5 in. (mm)
- Durational variation [table 3.6] 30 57 80 100 158 186%
- Orographic PMP for given durations [steps 4 X 5]

2.6	4.8	6.8	8.5	13.4	15.8
-----	-----	-----	-----	------	------

in. (mm)

C. Total PMP

- Add steps A9 and B6

5.8	8.8	11.1	13.1	18.7	21.4
-----	-----	------	------	------	------

in. (mm)
- PMP for other durations from smooth curve fitted to plot of computed data.
- Comparison with local-storm PMP (see sec. 6.3).

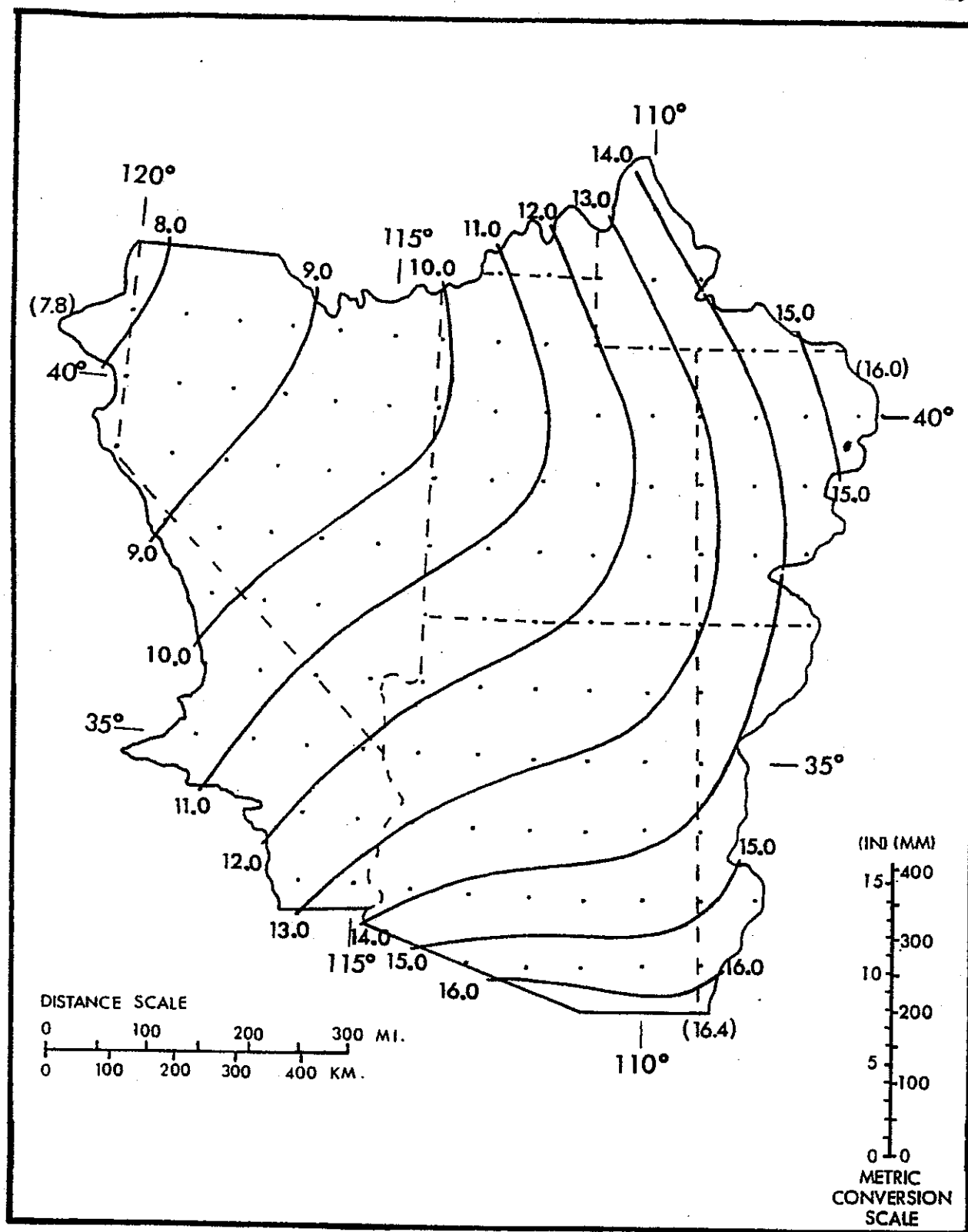


Figure 2.12.--1000-mb (100-kPa) 24-hr convergence PMP (inches) for 10 mi² (26 km²) for August. Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

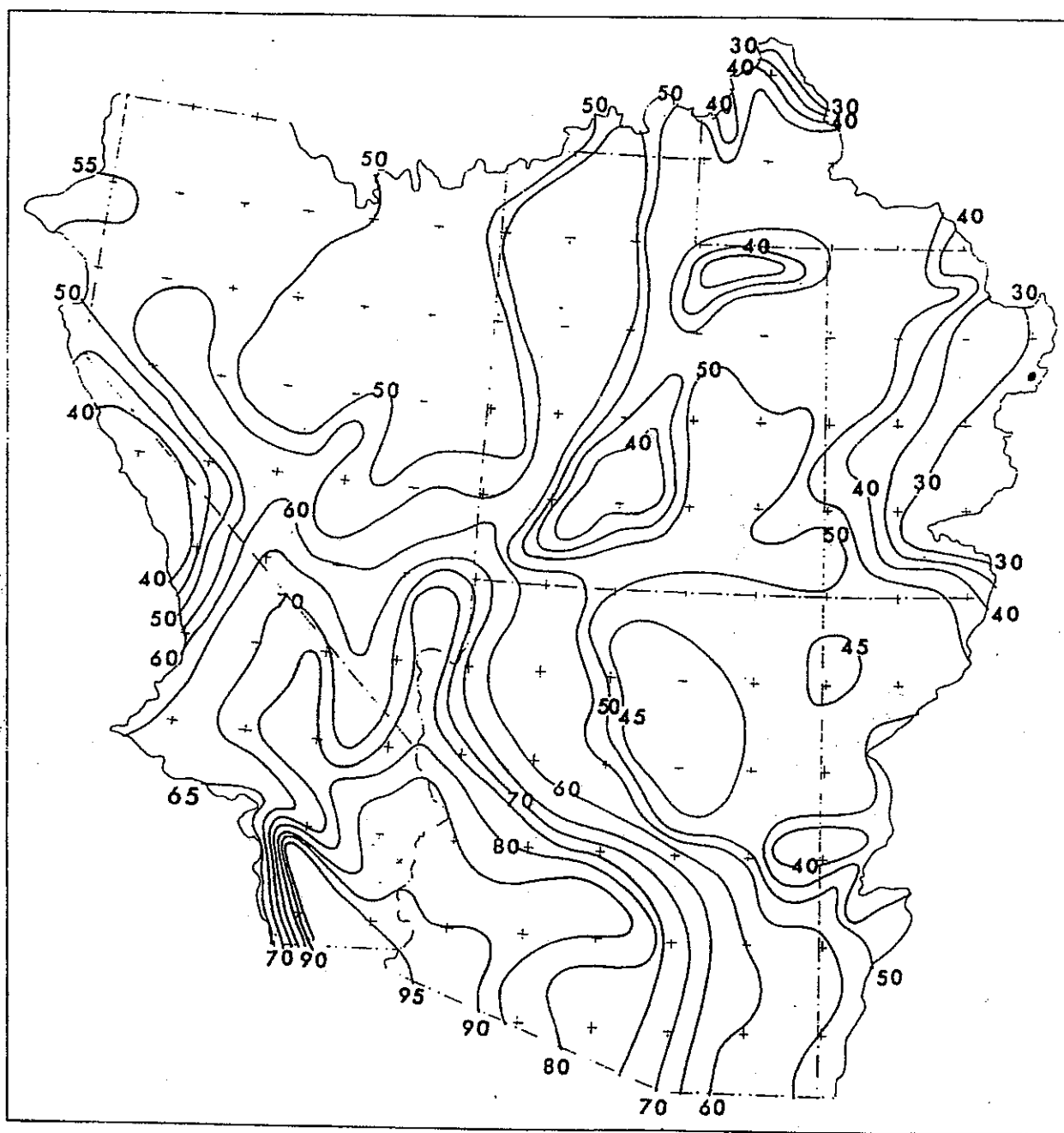
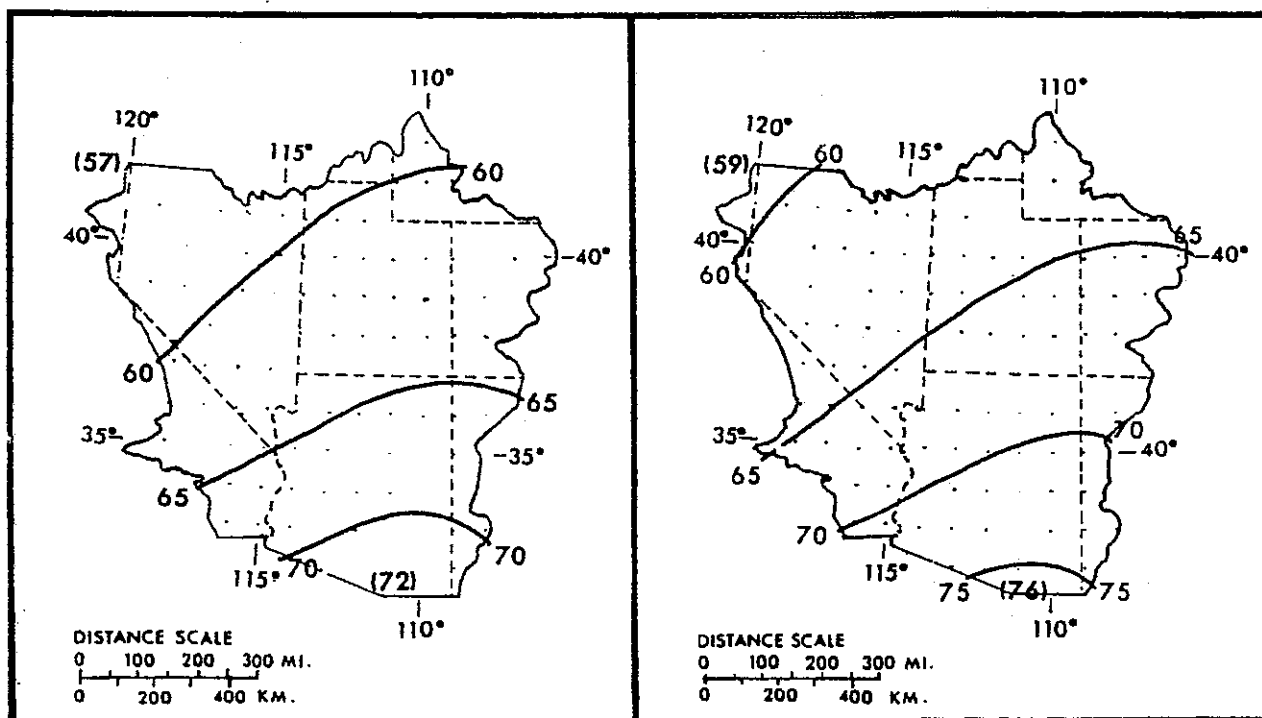
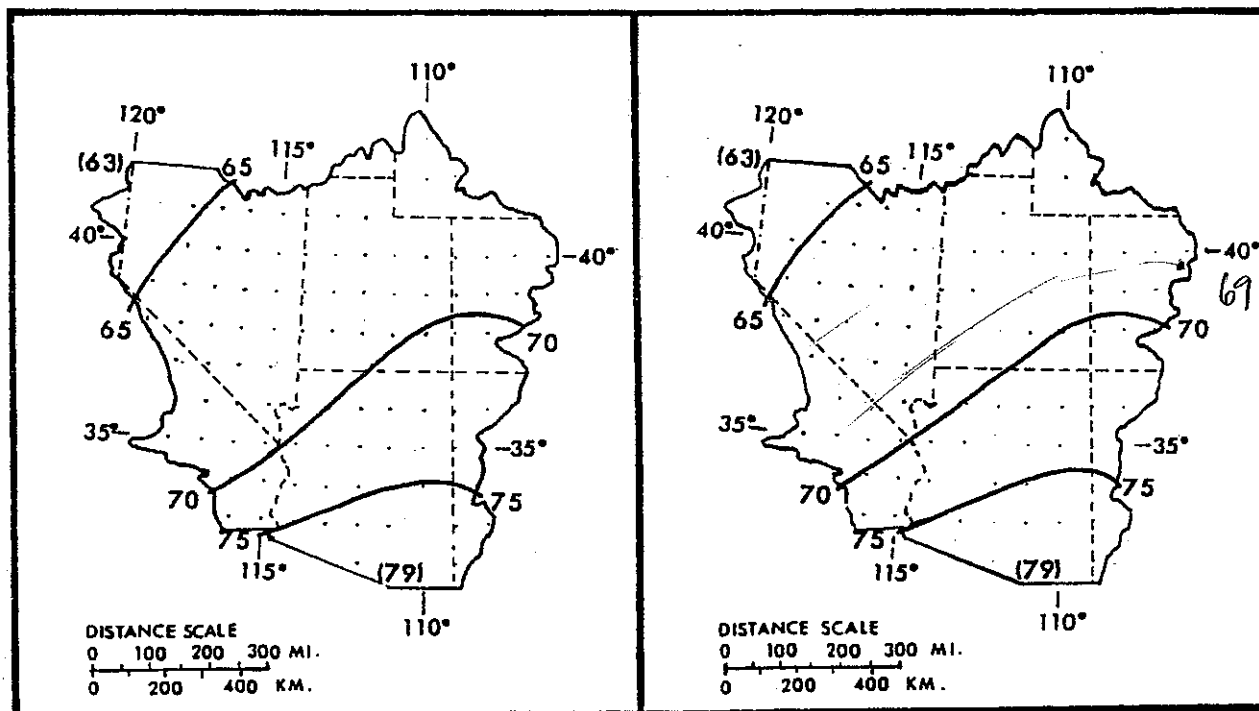


Figure 2.18.--Percent of 1000-mb (100-kPa) convergence PMP resulting from effective elevation and barrier considerations. Isolines drawn for every five percent.



May

June



July

August

Figure 2.26.--Regional variation of 6/24-hr ratios by month (percent). Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

For the range of 6/24-hr ratios included in figures 2.25 to 2.27, depth-duration values in percent of 24-hr amounts are found in table 2.7. The regional ratio maps, and the depth-duration curves presented in figure 2.20 were used in adjusting the major storm data to 24-hr amounts listed in table 2.1.

Table 2.7.--Durational variation of convergence PMP (in percent of 24-hr amount).

Duration (Hrs)						Duration (Hrs)					
6	12	18	24	48	72	6	12	18	24	48	72
50	76	90	100	129	150	66	84	93	100	116	124
51	77	90	100	128	148	67	85	94	100	116	123
52	77	90	100	127	146	68	85	94	100	115	122
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55	78	91	100	125	140	70	87	94	100	114	120
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59	80	92	100	121	134	74	89	95	100	112	117
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63	82	93	100	118	128	79	92	97	100	109	113
64	83	93	100	117	126						
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Note: For use, enter first column (6 hr) with 6/24-hr ratio from figures 2.25 to 2.27.

2.5 Areal Reduction for Basin Size

For operational use, basin average values of convergence PMP are needed rather than 10-mi² (26-km²) values. Preferably, the method for reducing 10-mi² (26-km²) values to basin average rainfalls should be derived from depth-area relations of storms in the region. However, all general storms in the region include large proportions of orographic precipitation.

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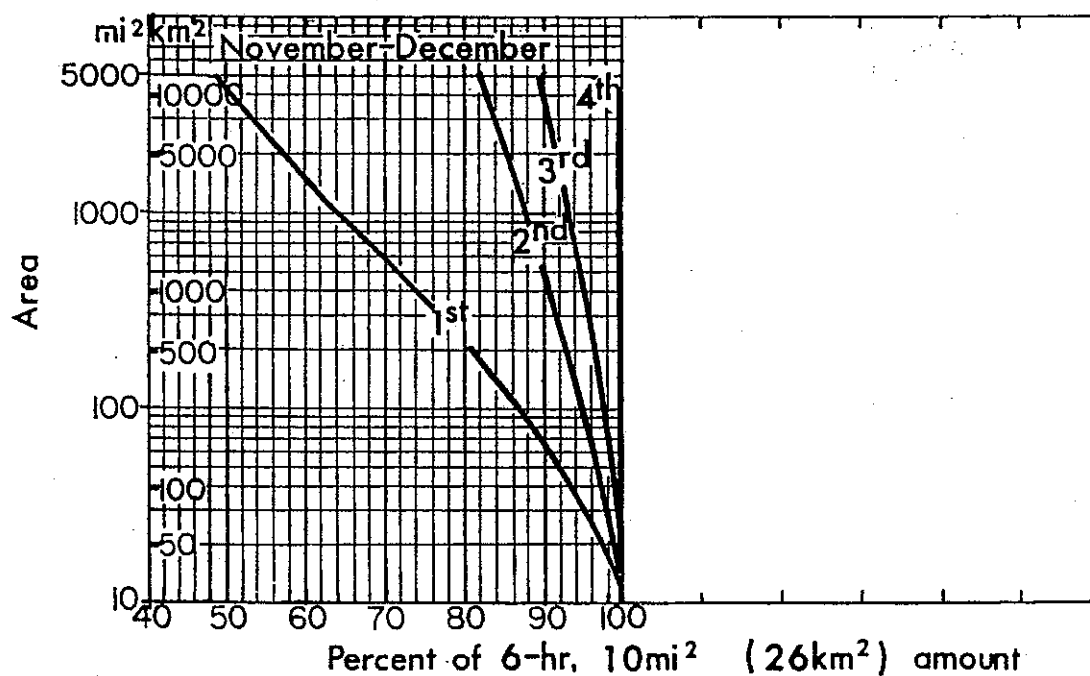
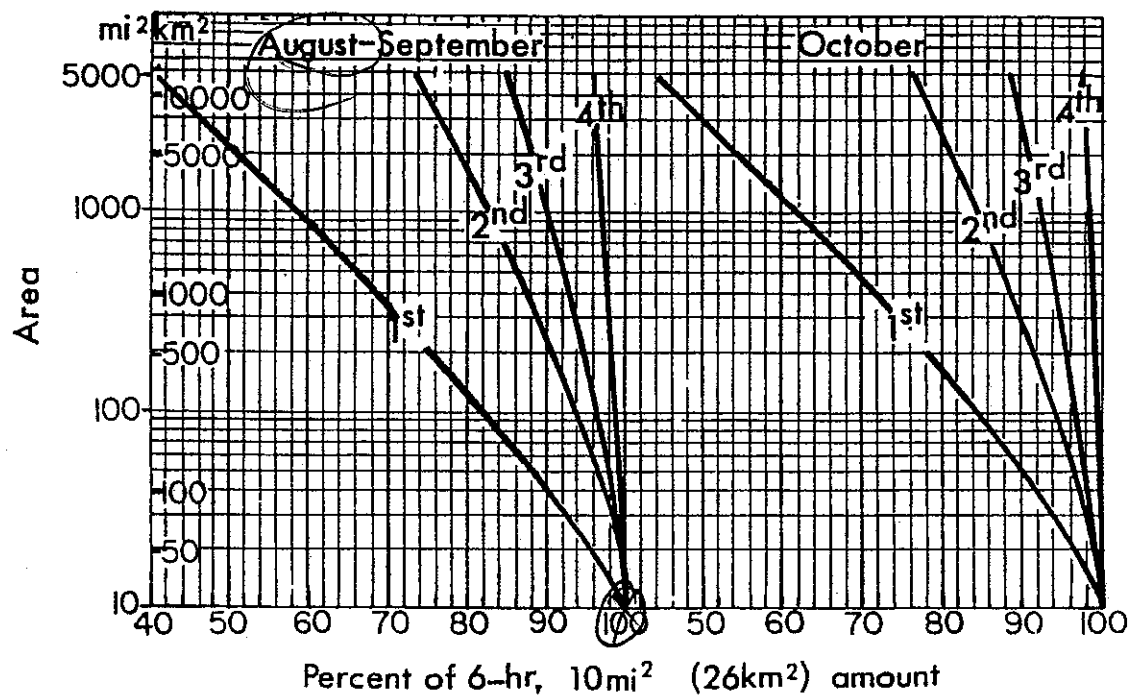


Figure 2.29.--Depth-area variation for convergence PMP for first to fourth 6-hr increments.

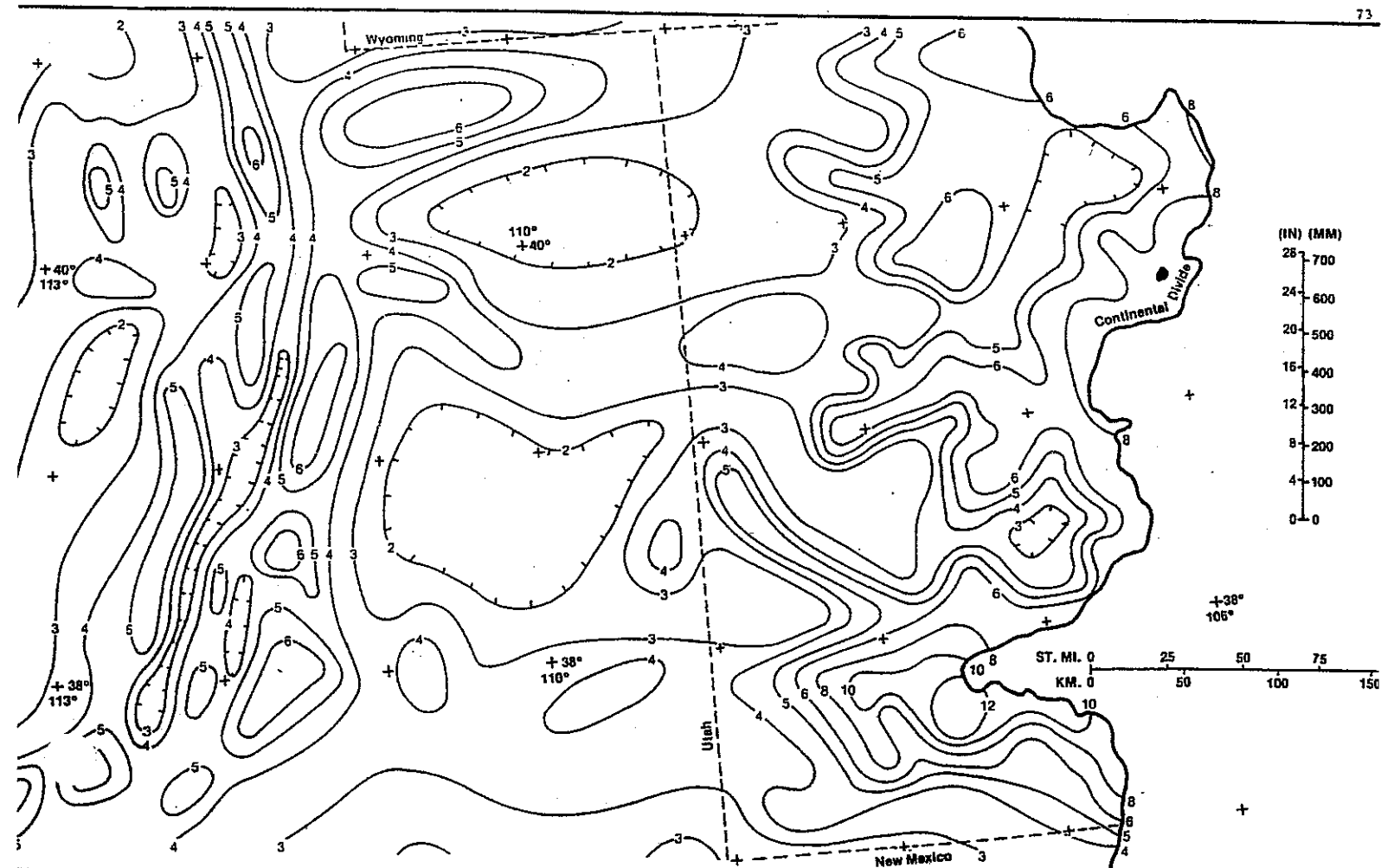


FIGURE 3.11b (Revised) — 10-mi² (26-km²) 24-hr orographic PMP index map (inches), north-central section.

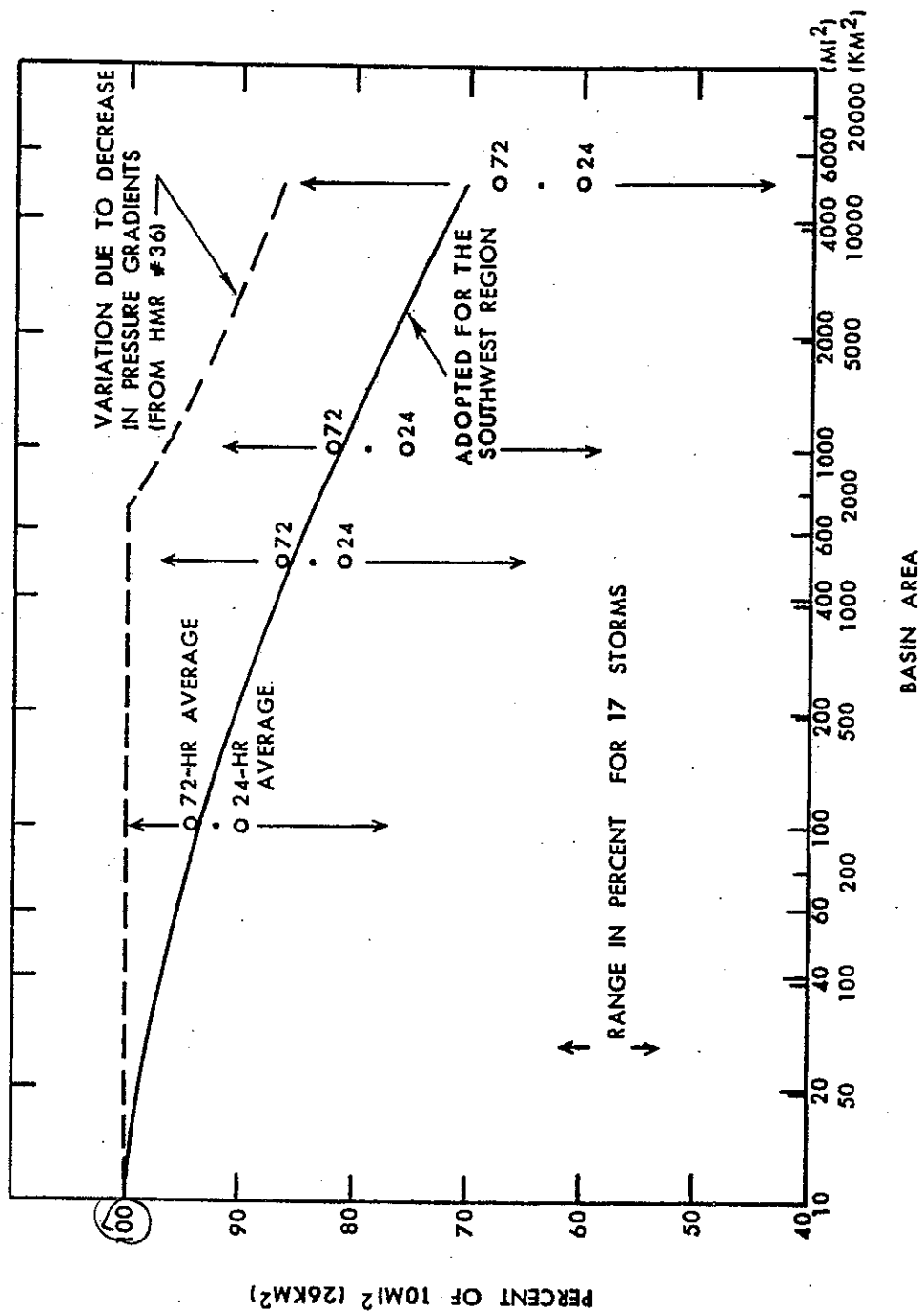
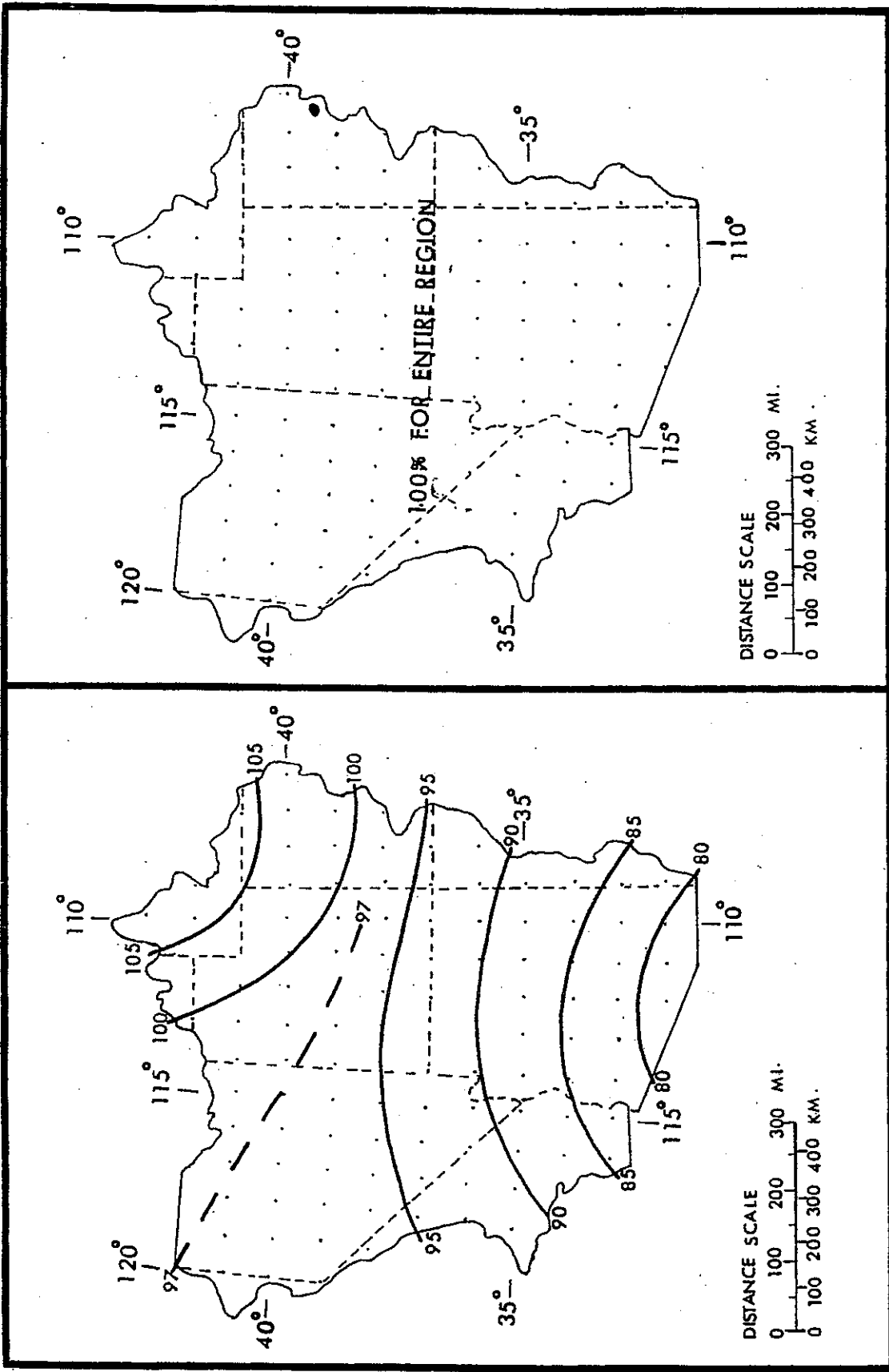


Figure 3.20.---Variation of orographic PMP with basin size.



July

August

Figure 3.15. ---Seasonal variation in 10-mi² (26-km²) 24-hr orographic PMP for the study region (in percent of values in figure 3.11).

Table 3.9.--Durational variation of orographic PMP

Latitude °N	Percent of 24-hr value					
	6 hr	12	18	24	48	72
42	28	55	79	100	161	190
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39.6° 40	30	57	80	100	159	187
39	30	57	80	100	157	185
38	31	58	81	100	155	182
37	32	59	81	100	152	177
36	33	60	82	100	149	172
35	34	61	82	100	146	167
34	35	62	83	100	143	162
33	36	63	84	100	139	157
32	37	64	84	100	135	152
31	39	66	85	100	132	146

4. LOCAL-STORM PMP FOR THE SOUTHWESTERN REGION AND CALIFORNIA

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August

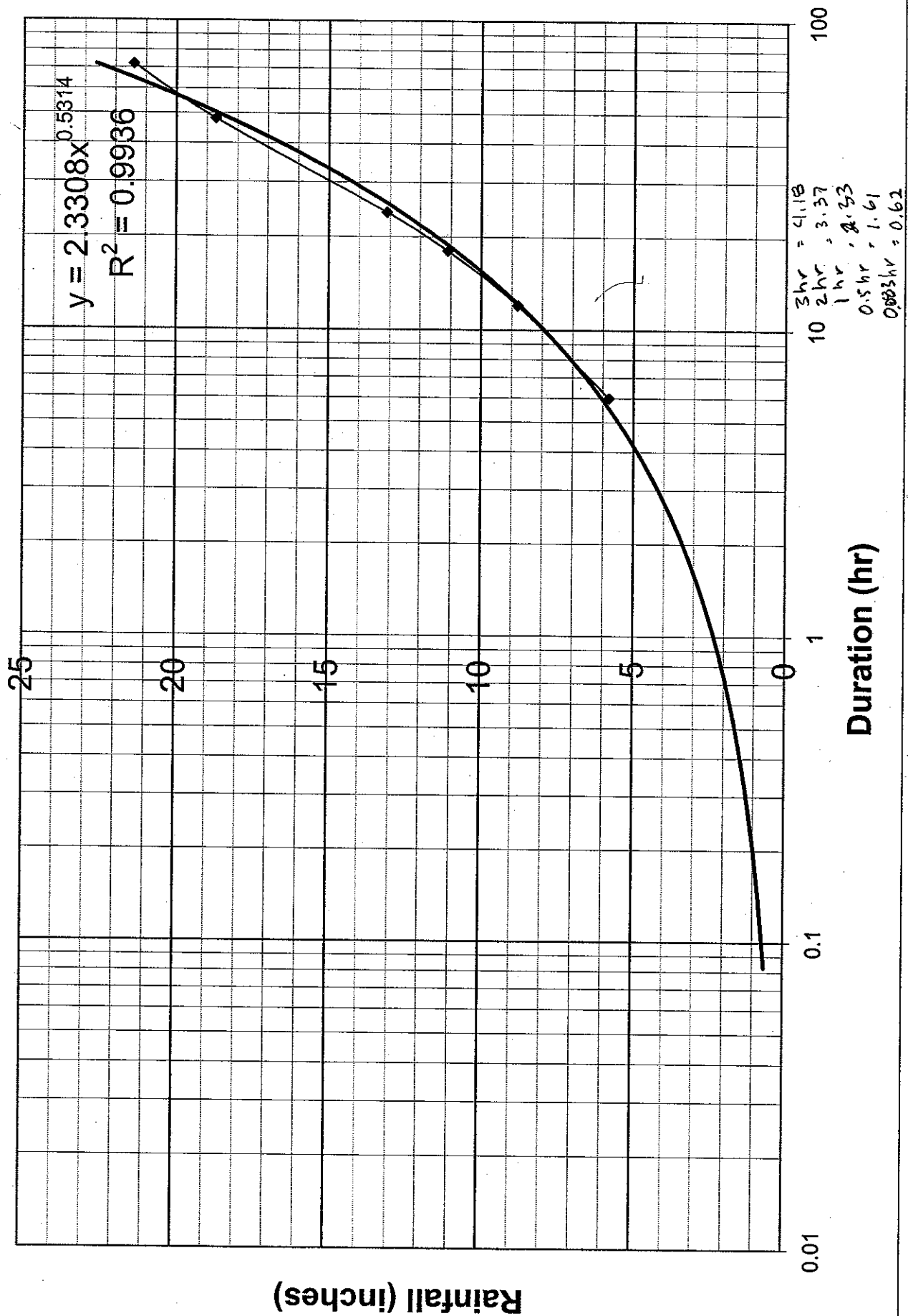


Table 6.1.--General-storm PMP computations for the Colorado River and Great basin

Drainage OLD DILLON RES Area 0.05 mi² (km²)
 Latitude 39°36", Longitude 106°04" of basin center

Month SEPTEMBER

Step	Duration (hrs)					
	6	12	18	24	48	72

A. Convergence PMP

- Drainage average value from one of figures 2.5 to 2.16 15.7 in. (mm)
- Reduction for barrier-elevation [fig. 2.18] 30 %
- Barrier-elevation reduced PMP [step 1 X step 2] 4.7 in. (mm)
- Durational variation [figs. 2.25 to 2.27 and table 2.7].
69 86 94 100 115 121 %
- Convergence PMP for indicated durations [steps 3 X 4] 3.2 4.0 4.4 4.7 5.4 5.7 in. (mm)
- Incremental 10 mi² (26 km²) PMP [successive subtraction in step 5] 3.2 0.8 0.4 0.3 0.7 0.3 in. (mm)
- Areal reduction [select from figs. 2.28 and 2.29] 100 100 100 100 100 100 %
- Areally reduced PMP [step 6 X step 7] 3.2 0.8 0.4 0.3 0.7 0.3 in. (mm)
- Drainage average PMP [accumulated values of step 8] 3.2 4.0 4.4 4.7 5.4 5.7 in. (mm)

B. Orographic PMP

- Drainage average orographic index from figure 3.11a to d. 8.5 in. (mm)
- Areal reduction [figure 3.20] 100 %
- Adjustment for month [one of figs. 3.12 to 3.17] 100 %
- Areally and seasonally adjusted PMP [steps 1 X 2 X 3] 8.5 in. (mm)
- Durational variation [table 3.6] 30 57 80 100 158 186 %
- Orographic PMP for given durations [steps 4 X 5] 2.6 4.8 6.8 8.5 13.4 15.8 in. (mm)

C. Total PMP

- Add steps A9 and B6 5.8 8.8 11.2 13.2 18.4 21.5 in. (mm)
- PMP for other durations from smooth curve fitted to plot of computed data.
- Comparison with local-storm PMP (see sec. 6.3).

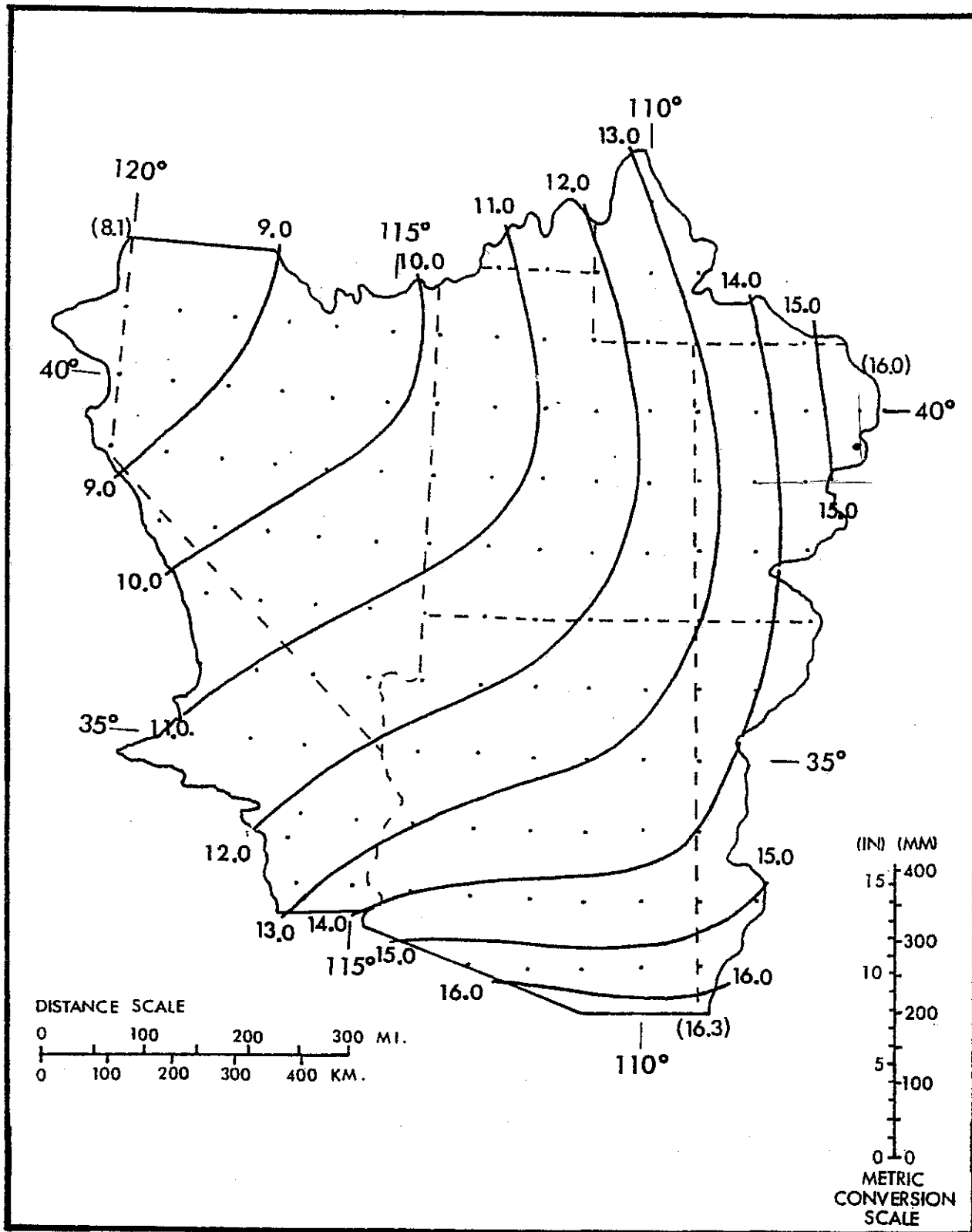


Figure 2.13.--1000-mb (100-kPa) 24-hr convergence PMP (inches) for 10 mi² (26 km²) for September. Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

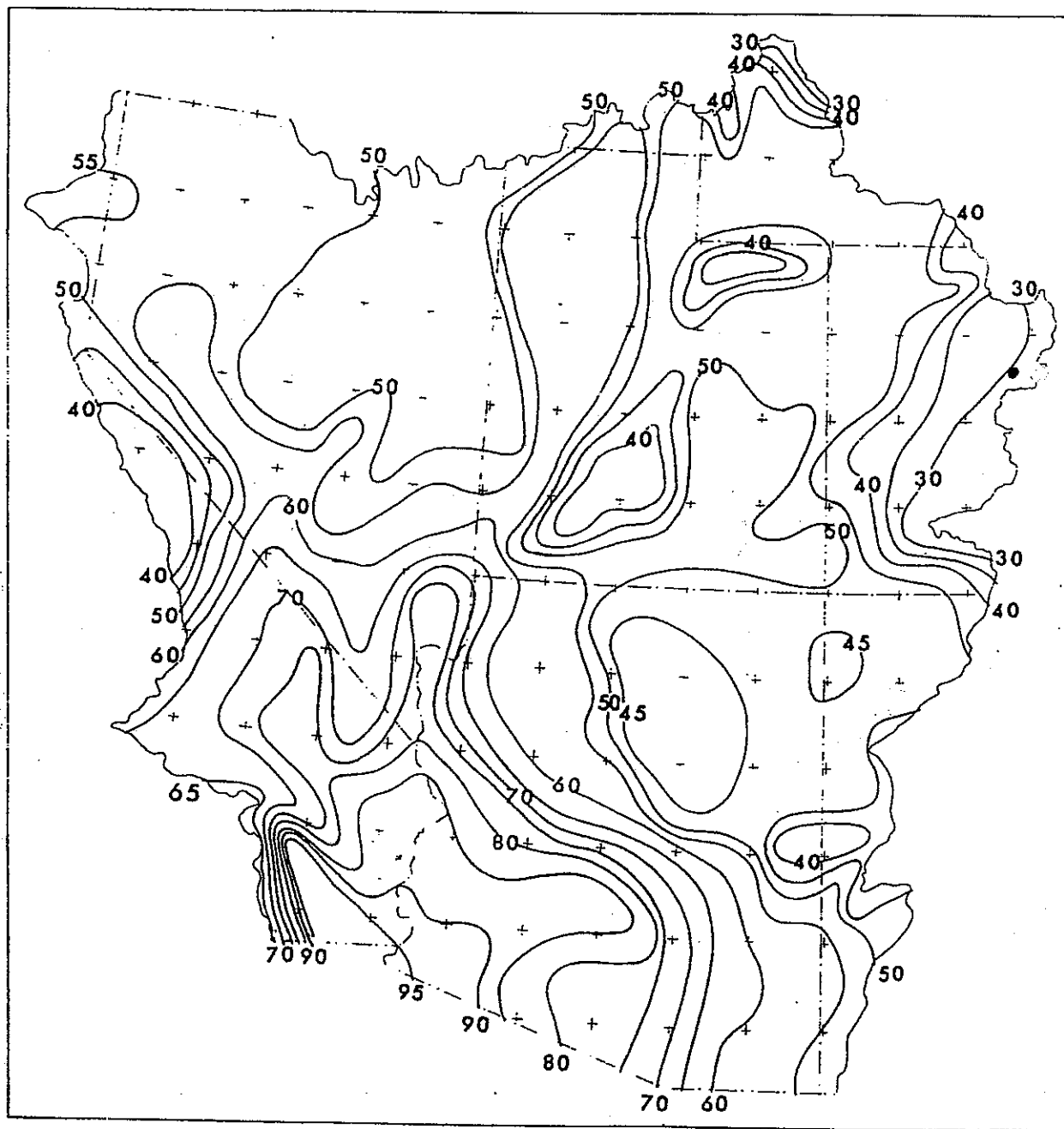


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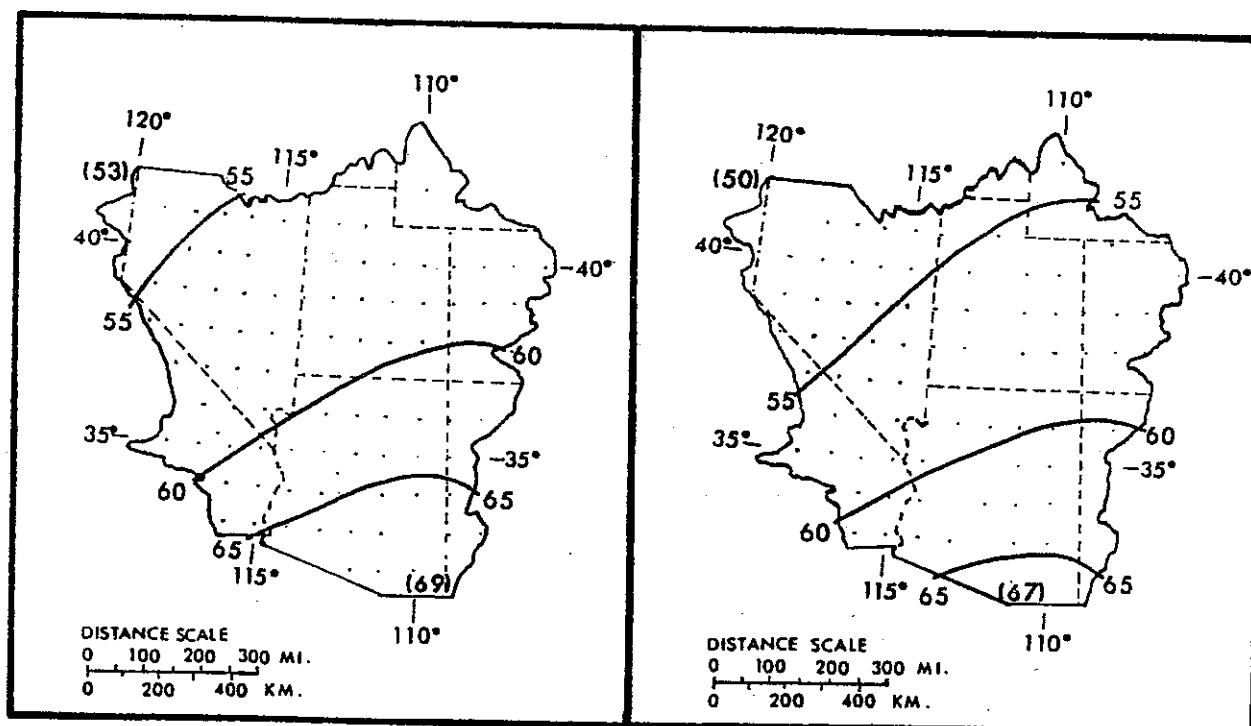
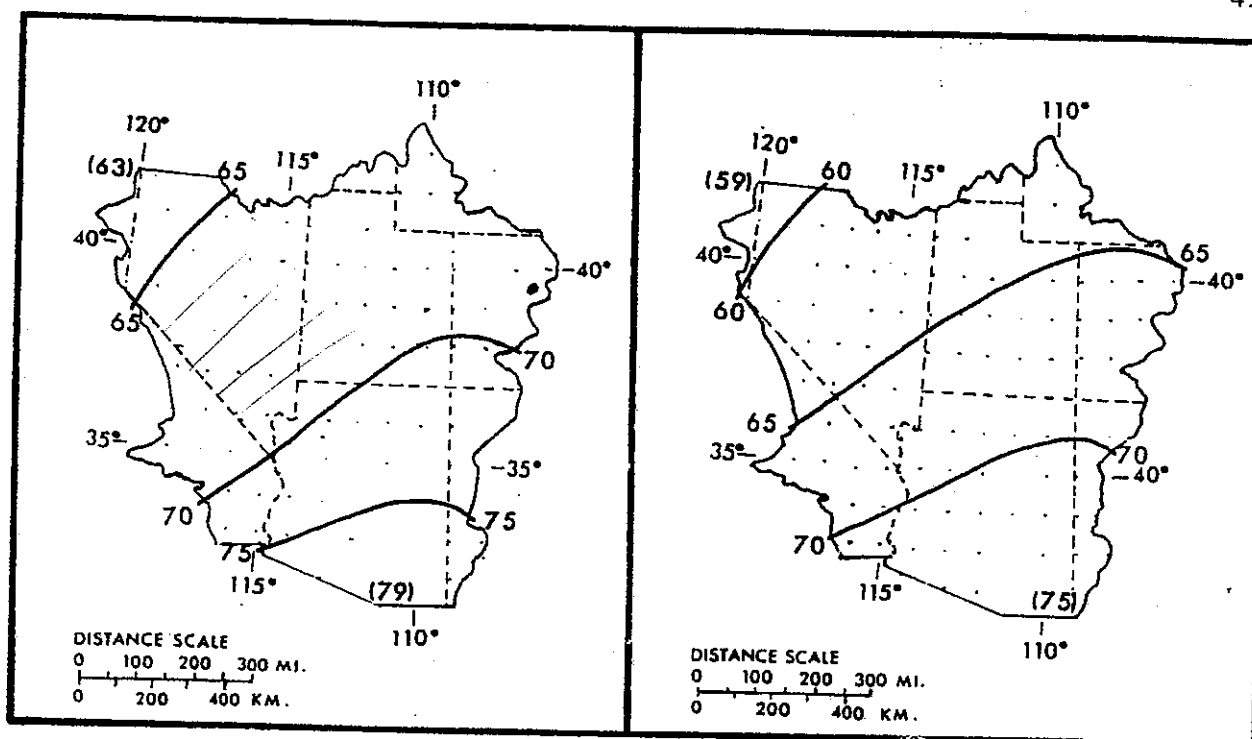


Figure 2.27.--Regional variation of 6/24-hr ratios by month (percent). Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

For the range of 6/24-hr ratios included in figures 2.25 to 2.27, depth-duration values in percent of 24-hr amounts are found in table 2.7. The regional ratio maps, and the depth-duration curves presented in figure 2.20 were used in adjusting the major storm data to 24-hr amounts listed in table 2.1.

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63	82	93	100	118	128	79	92	97	100	109	113
64	83	93	100	117	126						
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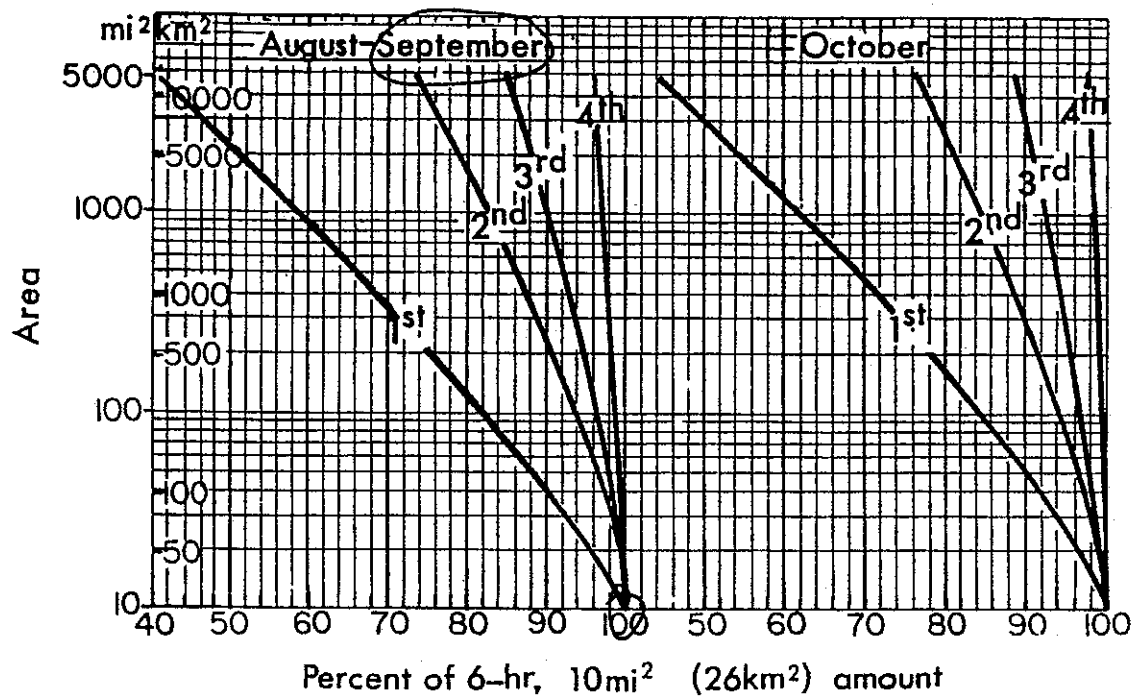


Figure 2.29.--Depth-area variation for convergence PMP for first to fourth 6-hr increments.

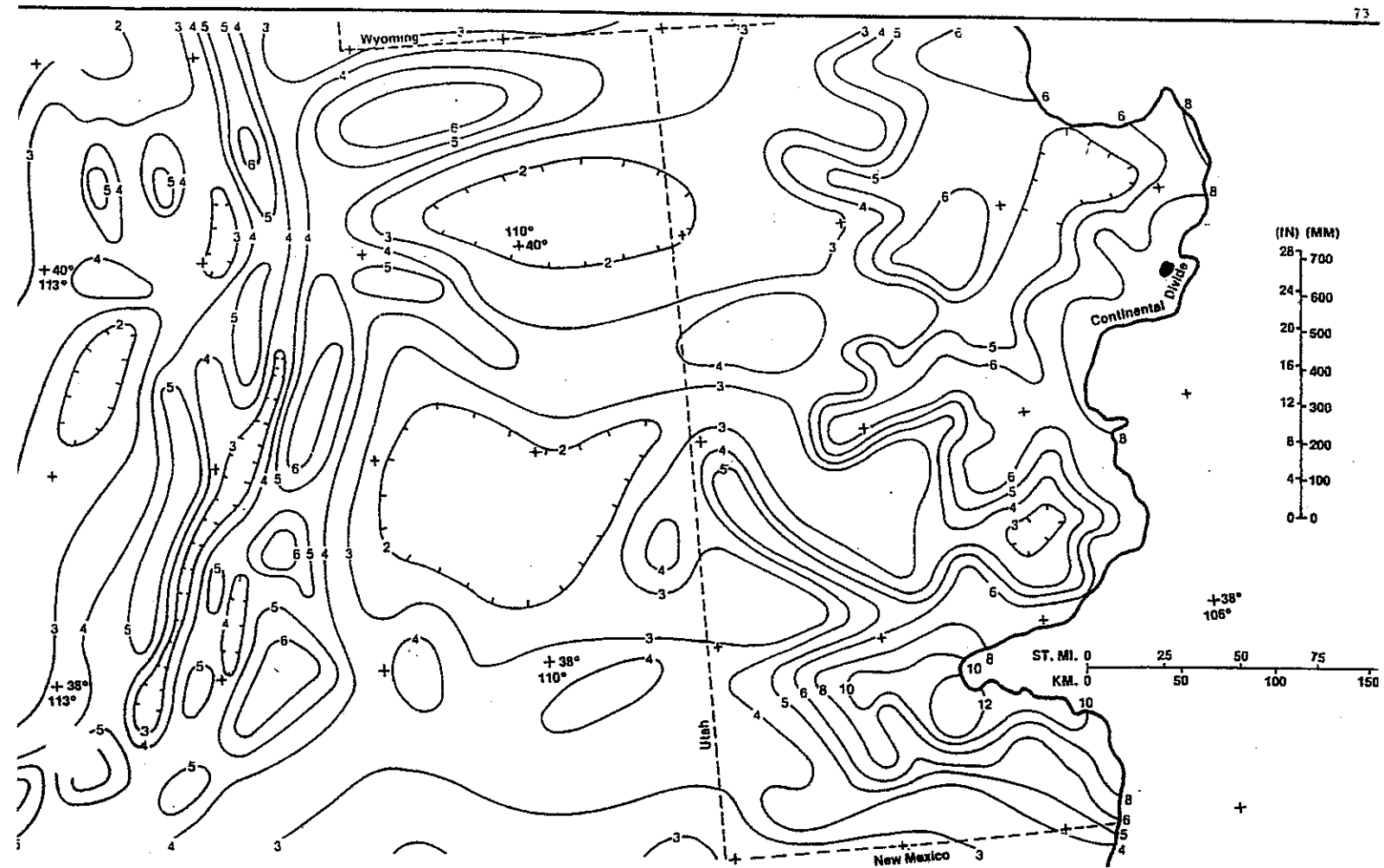


FIGURE 3.11b (Revised) — 10-mi² (26-km²) 24-hr orographic PMP index map (inches), north-central section.

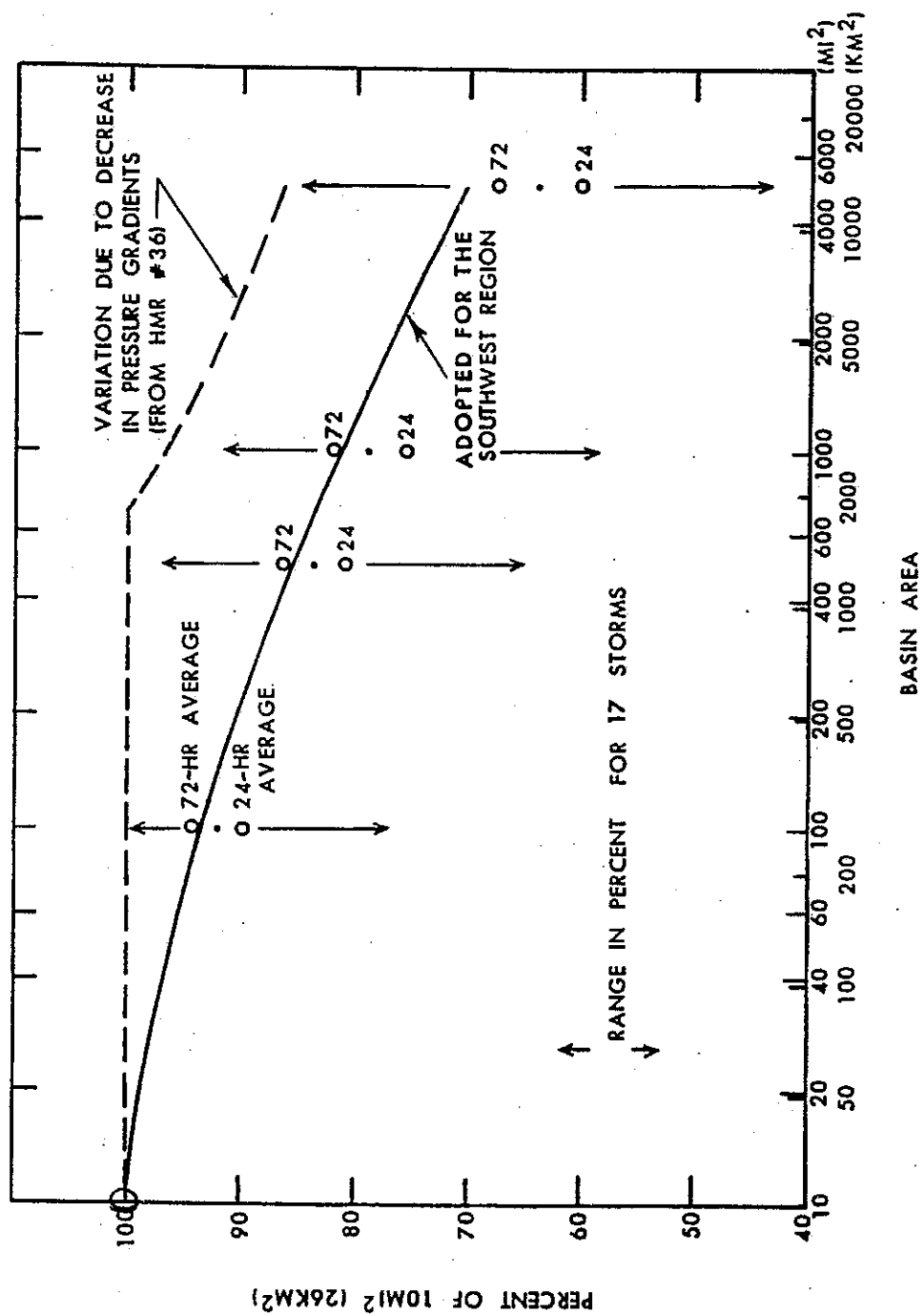


Figure 3.20.--Variation of orographic PMP with basin size.

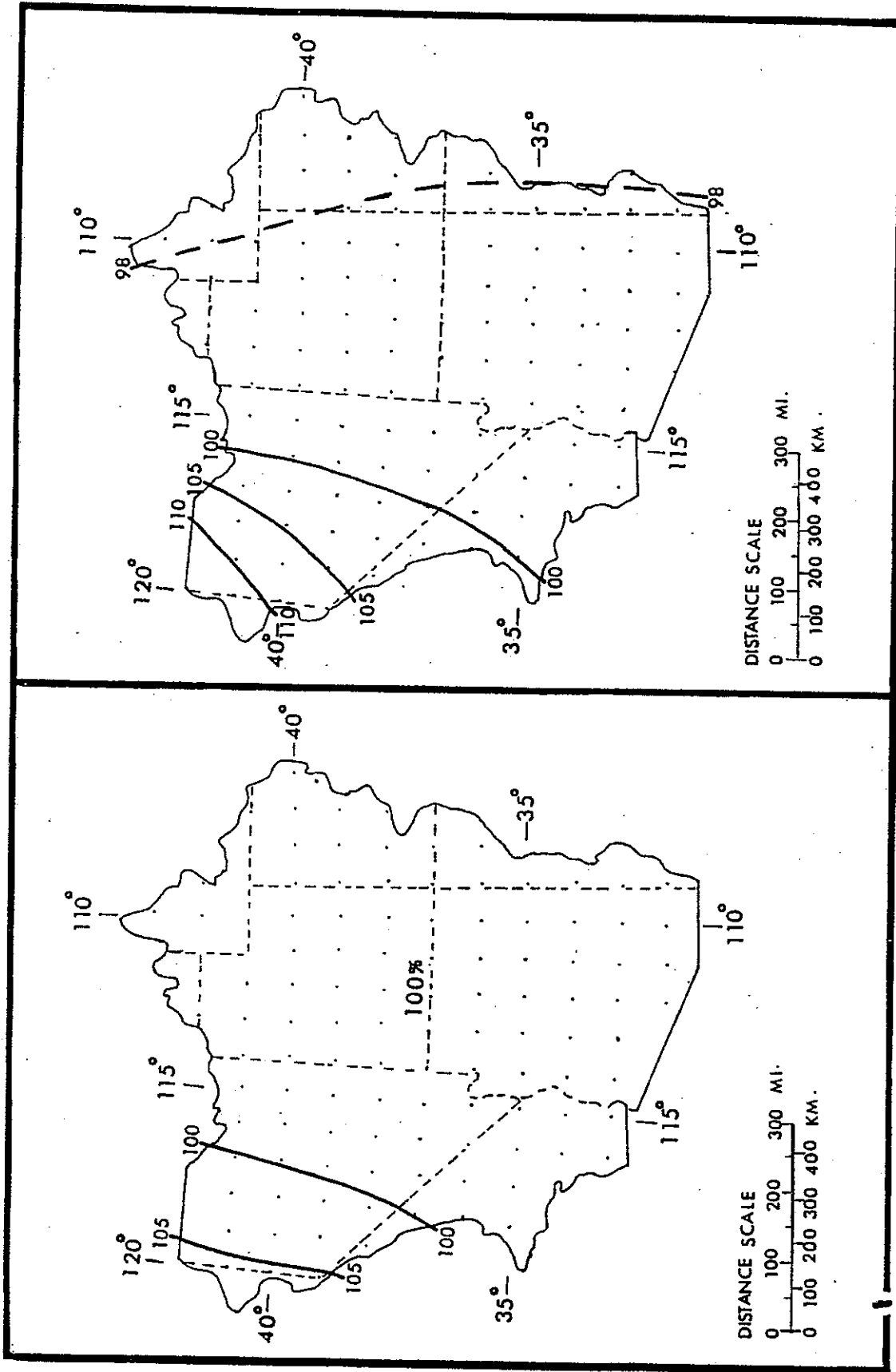


Figure 3.16. --Seasonal variation in 10-mi.² (26-km²) 24-hr orographic PMF for the study region (in percent of values in figure 3.11).

Table 3.9.--Durational variation of orographic PMP

Latitude °N	Percent of 24-hr value					
	6 hr	12	18	24	48	72
42	28	55	79	100	161	190
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39	30	57	80	100	157	185
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31	39	66	85	100	132	146

4. LOCAL-STORM PMP FOR THE SOUTHWESTERN REGION AND CALIFORNIA

4.1 Introduction

This chapter provides generalized estimates of local or thunderstorm probable maximum precipitation. By "generalized" is meant that mapped values are given from which estimates of PMP may be determined for any selected drainage.

4.1.1 Region of Interest

Local-storm PMP was not included in the "Interim Report, Probable Maximum Precipitation in California" (HMR No. 36). During the formulation of the present study, we decided that the local-storm part of the study should include California west of the Sierra Nevada. It was also noted that PMP for summer thunderstorms was not considered west of the Cascade Divide in the Northwestern Region (HMR No. 43). As stated in the latter report, "No summer thunderstorms have been reported there (west of the Divide) of an intensity of those to the east, for which the moisture source is often the Gulf of Mexico or Gulf of California. The Cascade Divide offers an additional barrier to such moisture inflows to coastal areas where, in addition, the Pacific Ocean to the west has a stabilizing influence on the air to hinder the occurrence of intense summer local storms." Therefore, it was necessary to establish some continuation of the Cascade Divide into California so that the local-storm PMP definition would have continuity between the two regions.

The stabilizing influence of the Pacific air is at times interrupted by the warm moist tropical air from the south pushing into California, although it is difficult to determine where the limit of southerly flow occurs. General storms having the tropical characteristic of excessive thunderstorm rains are observed as far north as the northern end of the Sacramento Valley. Thus, a northern boundary has been selected for this study, excluding that portion of

SEPTEMBER

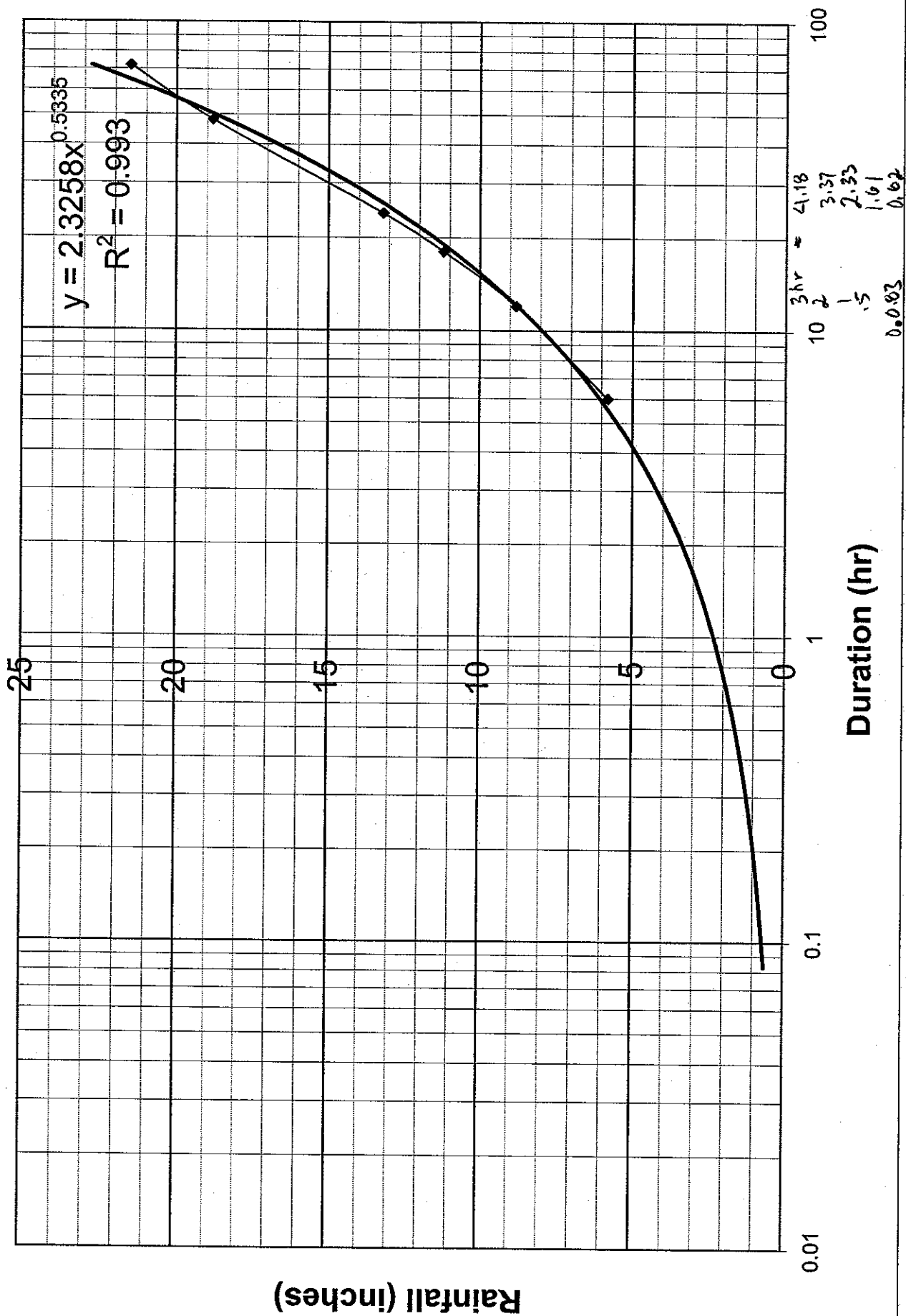


Table 6.1.--General-storm PMP computations for the Colorado River and Great basin

Drainage OLD DELLON RES Area 0.05 mi² (km²)
 Latitude 39°36", Longitude ↳ of basin center 106°04"

Month OCTOBER

Step	Duration (hrs)					
	6	12	18	24	48	72

A. Convergence PMP

1. Drainage average value from one of figures 2.5 to 2.16 13.7 in. (mm)
2. Reduction for barrier-elevation [fig. 2.18] 30 %
3. Barrier-elevation reduced PMP [step 1 X step 2] 4.1 in. (mm)
4. Durational variation [figs. 2.25 to 2.27 and table 2.7].

<u>66</u>	<u>84</u>	<u>93</u>	<u>100</u>	<u>116</u>	<u>124</u>
-----------	-----------	-----------	------------	------------	------------
5. Convergence PMP for indicated durations [steps 3 X 4]

<u>2.7</u>	<u>3.4</u>	<u>3.8</u>	<u>4.1</u>	<u>4.8</u>	<u>5.1</u>
------------	------------	------------	------------	------------	------------

in. (mm)
6. Incremental 10 mi² (26 km²) PMP [successive subtraction in step 5]

<u>2.7</u>	<u>0.7</u>	<u>0.4</u>	<u>0.3</u>	<u>0.7</u>	<u>0.3</u>
------------	------------	------------	------------	------------	------------

in. (mm)
7. Areal reduction [select from figs. 2.28 and 2.29]

<u>100</u>	<u>100</u>	<u>100</u>	<u>100</u>	<u>100</u>	<u>100</u>
------------	------------	------------	------------	------------	------------

%
8. Areally reduced PMP [step 6 X step 7]

<u>2.7</u>	<u>0.7</u>	<u>0.4</u>	<u>0.3</u>	<u>0.7</u>	<u>0.3</u>
------------	------------	------------	------------	------------	------------

in. (mm)
9. Drainage average PMP [accumulated values of step 8]

<u>2.7</u>	<u>3.4</u>	<u>3.8</u>	<u>4.1</u>	<u>4.8</u>	<u>5.1</u>
------------	------------	------------	------------	------------	------------

in. (mm)

B. Orographic PMP

1. Drainage average orographic index from figure 3.11a to d. 8.5 in. (mm)
2. Areal reduction [figure 3.20] 100 %
3. Adjustment for month [one of figs. 3.12 to 3.17] 98 %
4. Areally and seasonally adjusted PMP [steps 1 X 2 X 3] 8.3 in. (mm)
5. Durational variation [table 3.6] 3.9

<u>30</u>	<u>57</u>	<u>80</u>	<u>100</u>	<u>158</u>	<u>186</u>
-----------	-----------	-----------	------------	------------	------------
6. Orographic PMP for given durations [steps 4 X 5]

<u>2.5</u>	<u>4.7</u>	<u>6.6</u>	<u>8.3</u>	<u>13.1</u>	<u>15.4</u>
------------	------------	------------	------------	-------------	-------------

in. (mm)

C. Total PMP

1. Add steps A9 and B6

<u>5.2</u>	<u>8.1</u>	<u>10.4</u>	<u>12.4</u>	<u>17.9</u>	<u>20.5</u>
------------	------------	-------------	-------------	-------------	-------------

in. (mm)
2. PMP for other durations from smooth curve fitted to plot of computed data.
3. Comparison with local-storm PMP (see sec. 6.3).

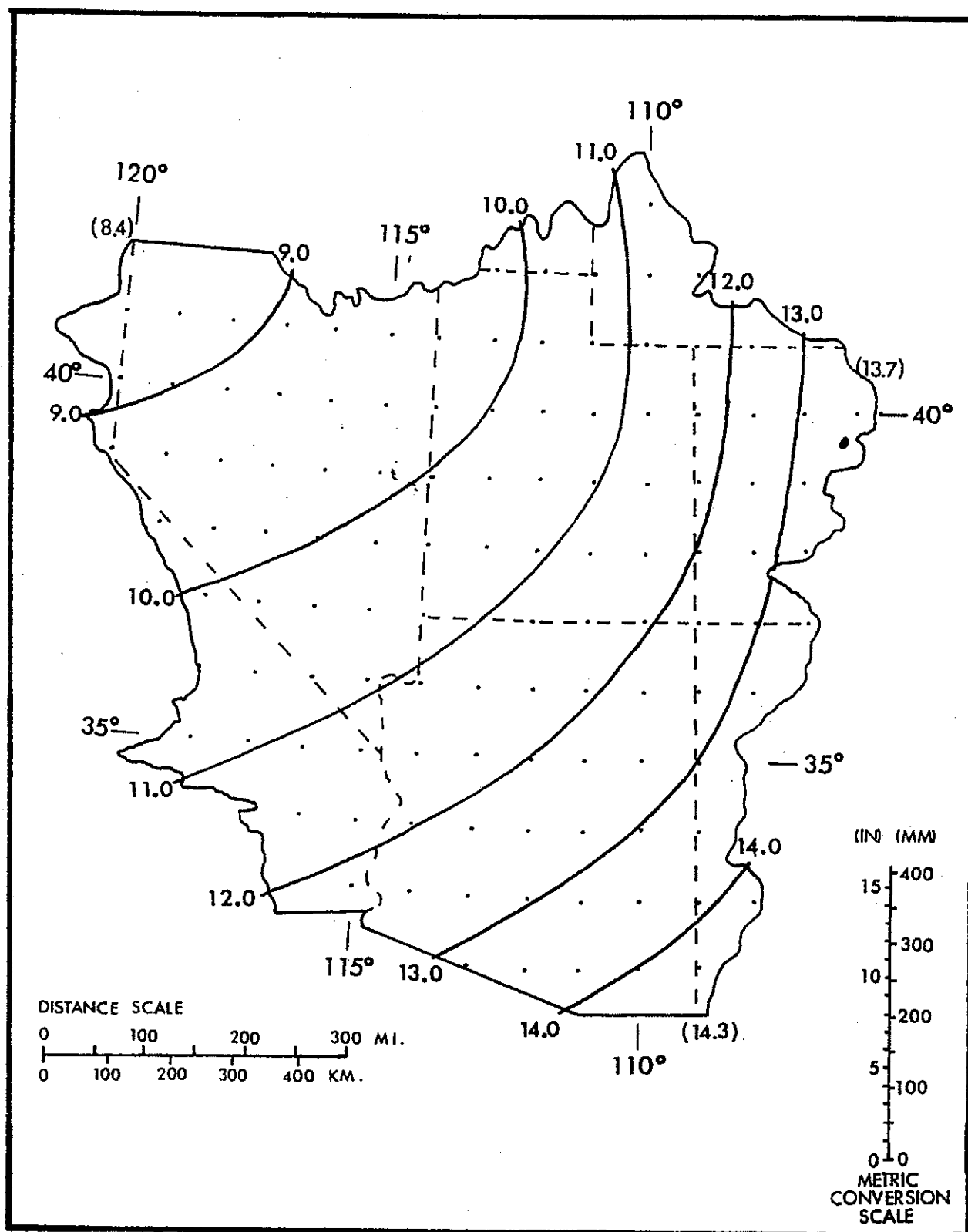


Figure 2.14.--1000-mb (100-kPa) 24-hr convergence PMP (inches) for 10 mi² (26 km²) for October. Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

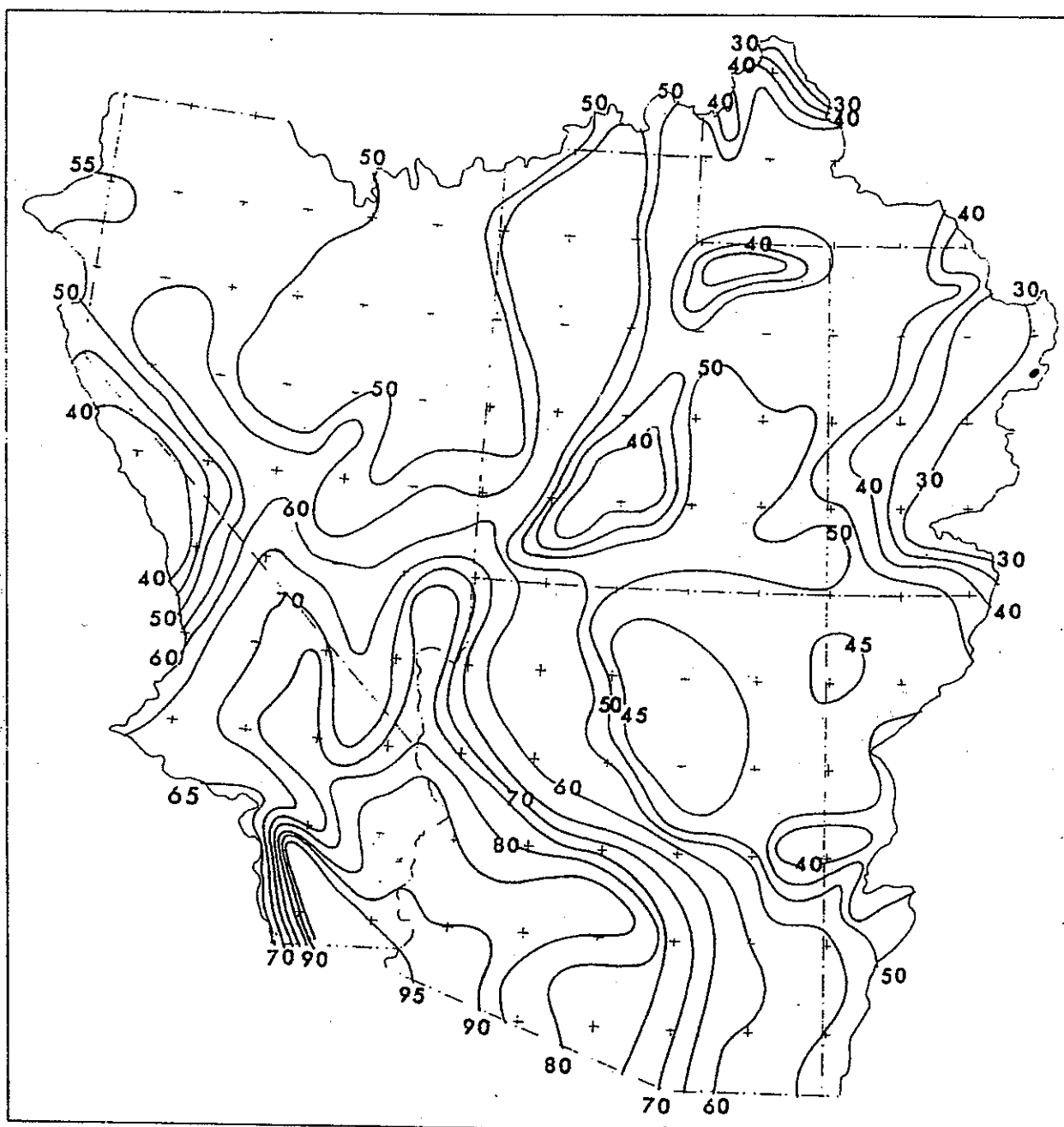


Figure 2.18.--Percent of 1000-mb (100-kPa) convergence PMP resulting from effective elevation and barrier considerations. Isolines drawn for every five percent.

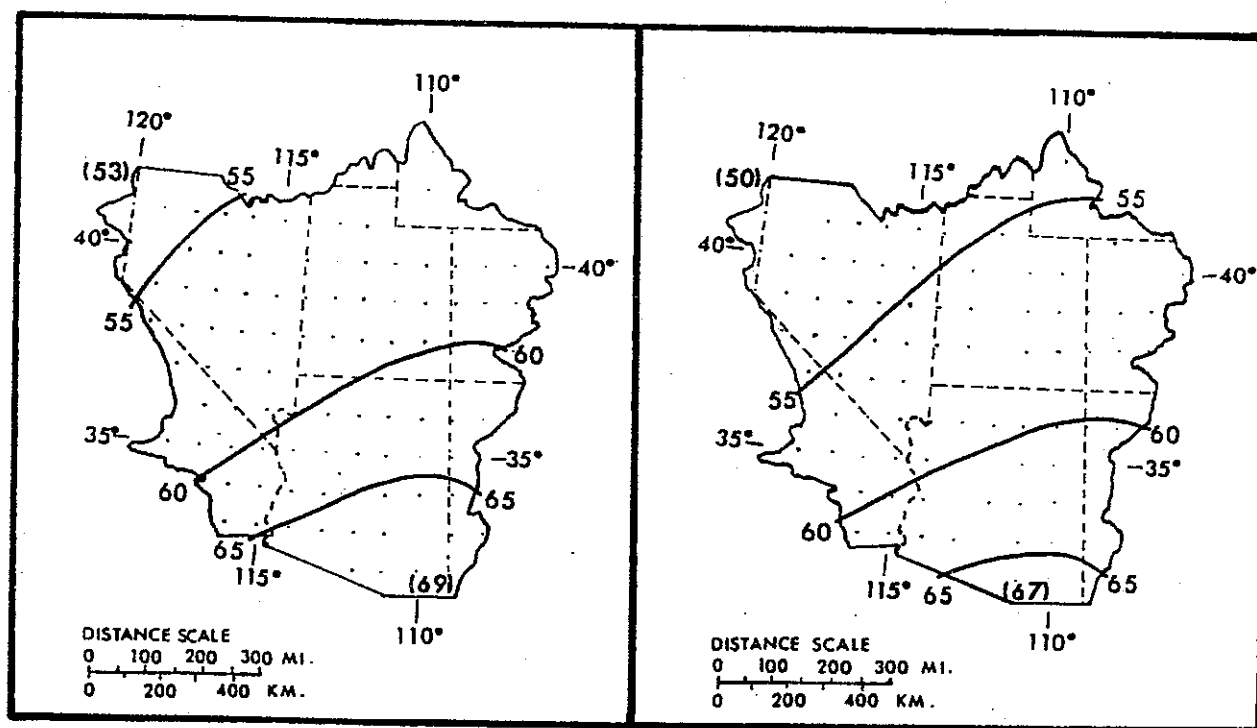
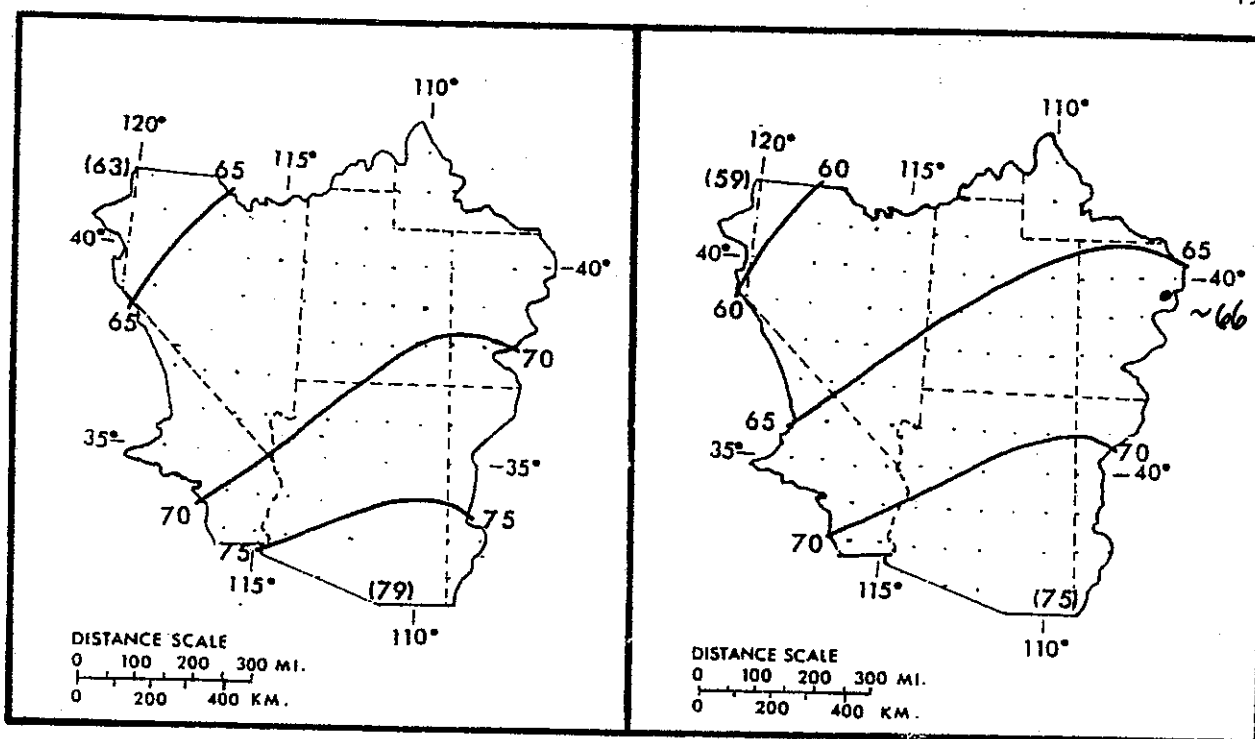


Figure 2.27.--Regional variation of 6/24-hr ratios by month (percent). Values in parentheses are limiting values and are to facilitate extrapolation beyond the indicated gradient.

For the range of 6/24-hr ratios included in figures 2.25 to 2.27, depth-duration values in percent of 24-hr amounts are found in table 2.7. The regional ratio maps, and the depth-duration curves presented in figure 2.20 were used in adjusting the major storm data to 24-hr amounts listed in table 2.1.

Table 2.7.--Durational variation of convergence PMP (in percent of 24-hr amount).

Duration (Hrs)						Duration (Hrs)					
6	12	18	24	48	72	6	12	18	24	48	72
50	76	90	100	129	150	<u>66</u>	<u>84</u>	<u>93</u>	<u>100</u>	<u>116</u>	<u>124</u>
51	77	90	100	128	148	67	85	94	100	116	123
52	77	90	100	127	146	68	85	94	100	115	122
53	77	91	100	127	144	69	86	94	100	115	121
54	78	91	100	126	142						
55	78	91	100	125	140	70	87	94	100	114	120
56	79	91	100	124	138	71	87	95	100	114	119
57	79	92	100	123	137	72	88	95	100	113	118
58	80	92	100	122	135	73	88	95	100	113	118
59	80	92	100	121	134	74	89	95	100	112	117
						75	89	96	100	112	116
60	81	92	100	120	132	76	90	96	100	111	115
61	81	92	100	120	131	77	90	96	100	110	114
62	82	93	100	119	129	78	91	96	100	110	114
63	82	93	100	118	128	79	92	97	100	109	113
64	83	93	100	117	126						
65	84	93	100	117	125	80	92	97	100	109	113

Note: For use, enter first column (6 hr) with 6/24-hr ratio from figures 2.25 to 2.27.

2.5 Areal Reduction for Basin Size

For operational use, basin average values of convergence PMP are needed rather than 10-mi² (26-km²) values. Preferably, the method for reducing 10-mi² (26-km²) values to basin average rainfalls should be derived from depth-area relations of storms in the region. However, all general storms in the region include large proportions of orographic precipitation.

Our solution was to use generalized depth-area relations developed for PMP estimates within bordering zones in the Central and Eastern United States (Riedel et al. 1956). The smoothed areal variations adopted for the Southwestern States are shown in figures 2.28 and 2.29 for each month or a combination of months where differences are insignificant.

Figures 2.28 and 2.29 give depth-area relations that reduce 10-mi² (26-km²) convergence PMP for basin sizes up to 5,000 mi² (12,950 km²) for each month. Areal variations are given for the 4 greatest (1st to 4th) 6-hr PMP increments. After the 4th increment no reduction for basin size is required. Application of these figures will become clear through consideration of an example of PMP computation in chapter 6.

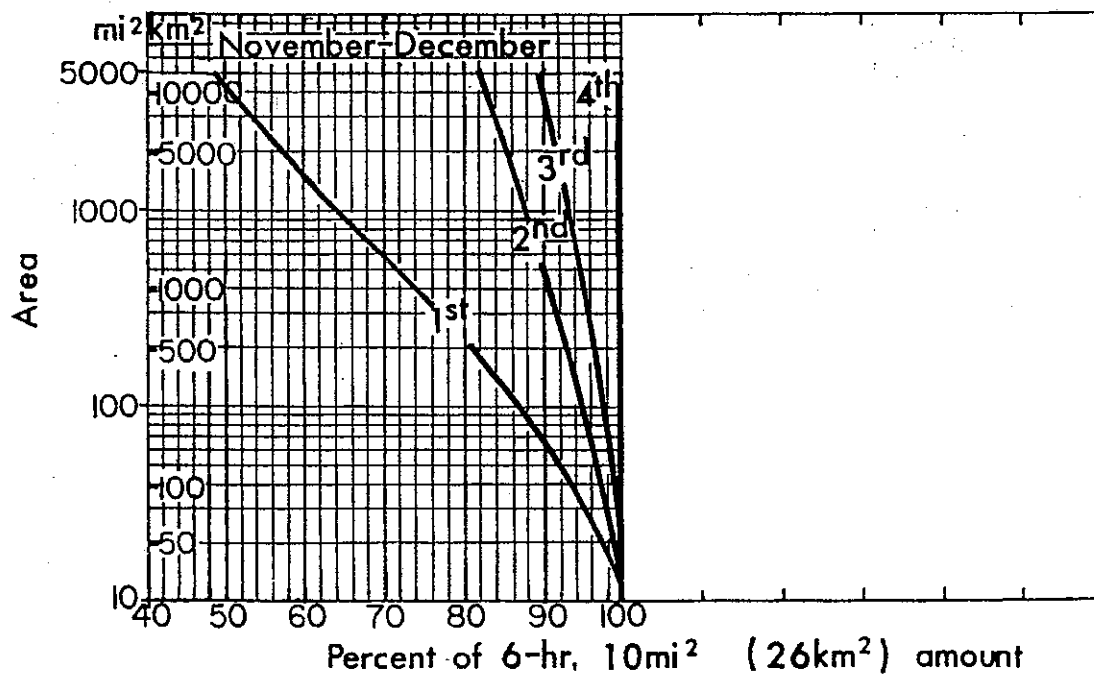
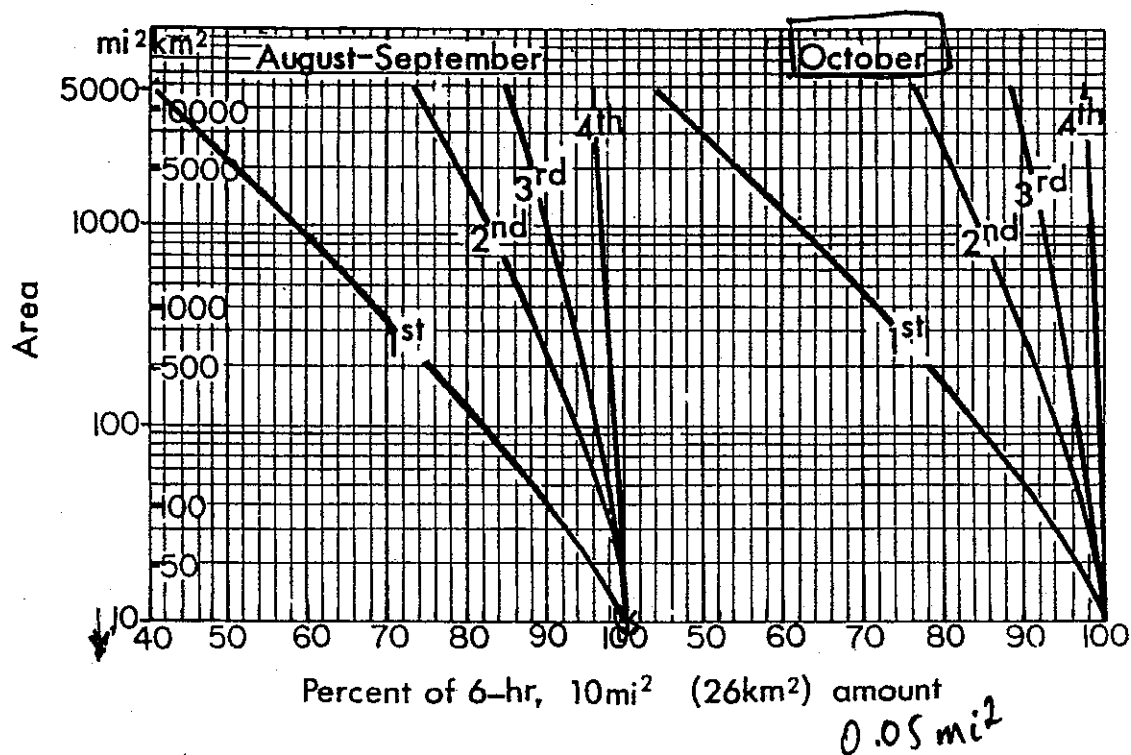


Figure 2.29.--Depth-area variation for convergence PMP for first to fourth 6-hr increments.

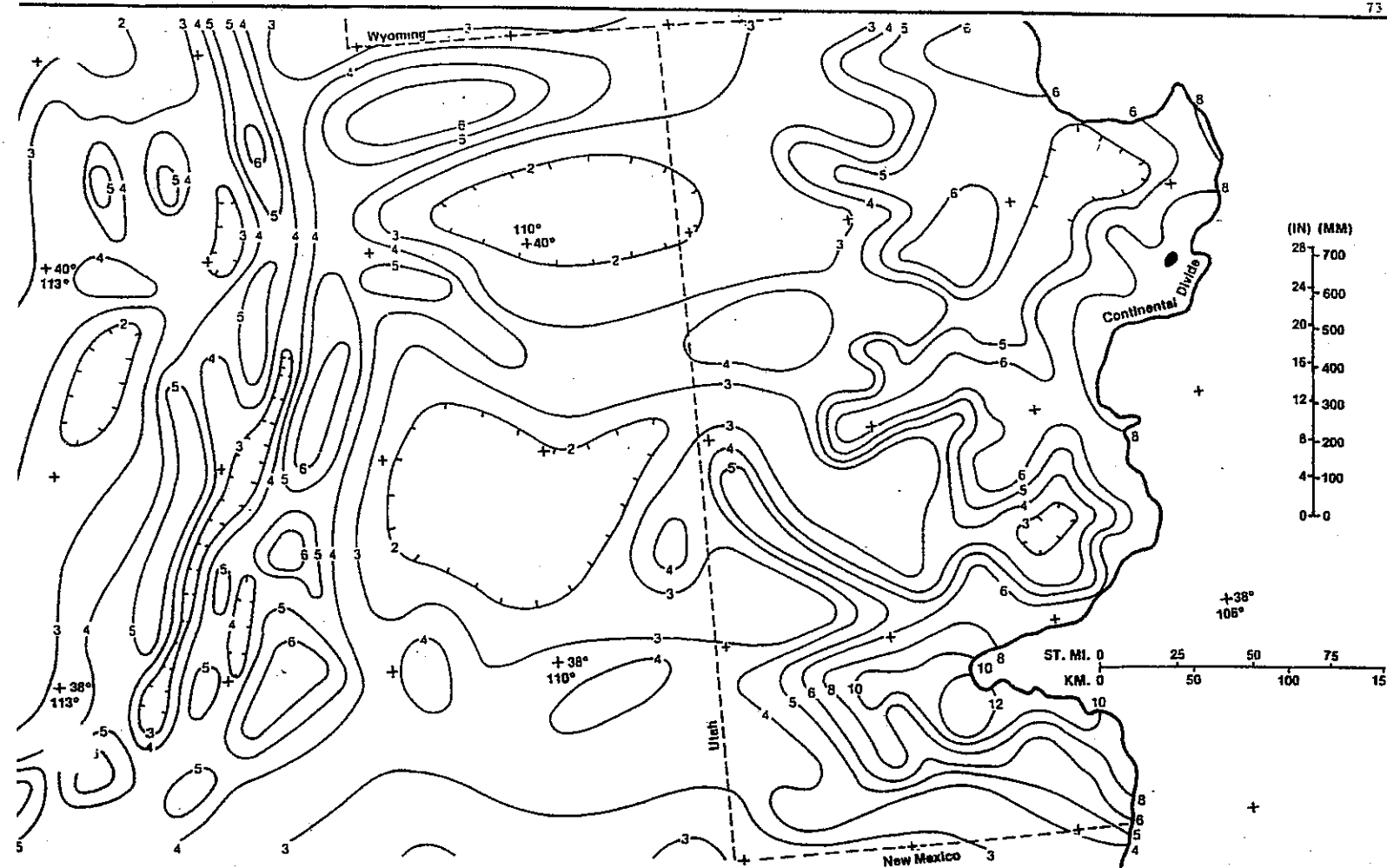


FIGURE 3.11b (Revised) — 10-mi² (26-km²) 24-hr orographic PMP index map (inches), north-central section.

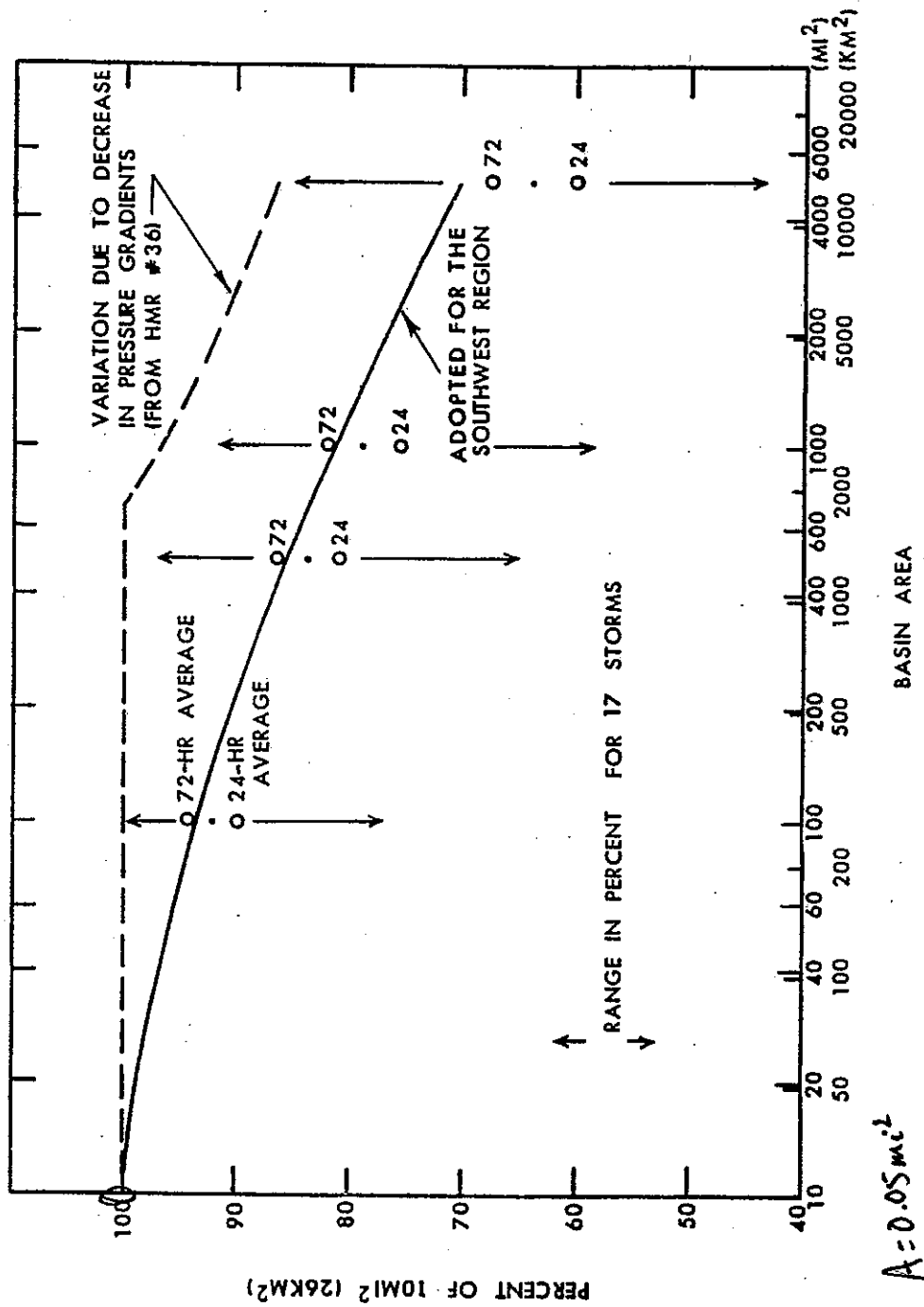
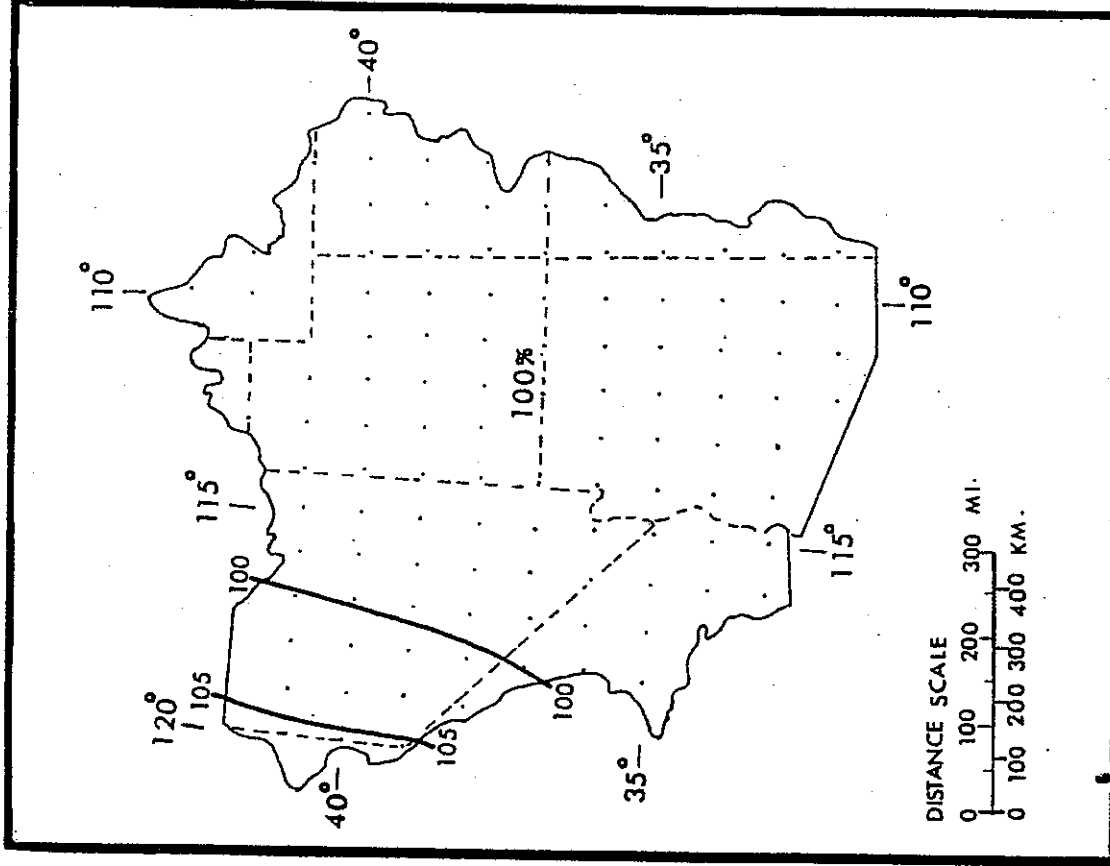
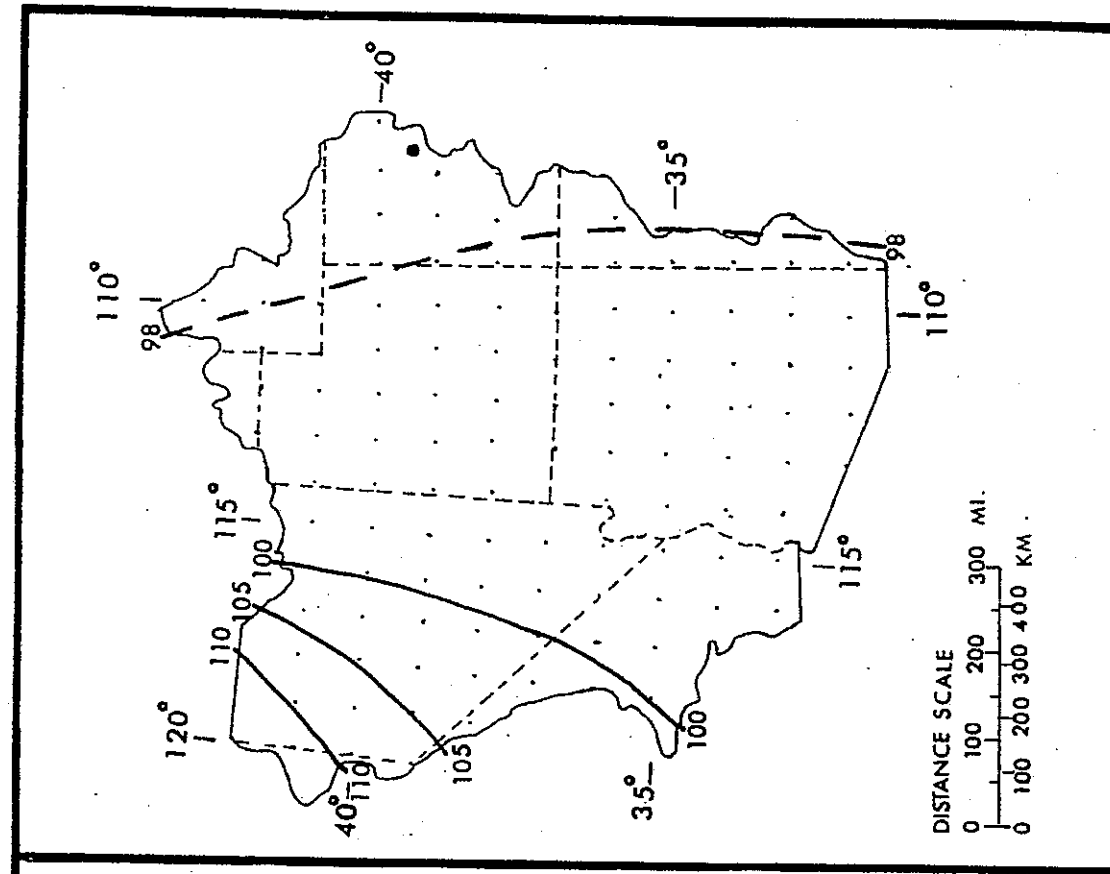


Figure 3.20. ---Variation of orographic PMP with basin size.



September



October

Figure 3.16.--Seasonal variation in 10-mi² (26-km²) 24-hr orographic PMP for the study region (in percent of values in figure 3.11).

Table 3.9.--Durational variation of orographic PMP

Latitude °N	Percent of 24-hr value					
	6 hr	12	18	24	48	72
42	28	55	79	100	161	190
41	29	56	79	100	160	189
39.6 40	30	57	80	100	159	187
39	30	57	80	100	157	185
38	31	58	81	100	155	182
37	32	59	81	100	152	177
36	33	60	82	100	149	172
35	34	61	82	100	146	167
34	35	62	83	100	143	162
33	36	63	84	100	139	157
32	37	64	84	100	135	152
31	39	66	85	100	132	146

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AREA CAPACITY CURVE



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: AREA CAPACITY CURVE FOR PROP. OPR

Total Number of Pages (including cover sheet): 3

Total Number of Computer Runs: -

Prepared by: PGS Date: 10/22/08

Checked by: _____ Date: _____

Description and Purpose:

DETERMINE THE AREA/CAPACITY RELATIONSHIP FOR THE PROPOSED
OLD DILLON RESERVOIR TO BE USED FOR ROUTING FLOWS & CALCULATING
DISCHARGES IN HEC-1

Design Basis/References/Assumptions:

- GET PROPOSED ELEVATION - AREA FROM DRAWINGS
- CALCULATE CAPACITY OF PROPOSED RESERVOIR FOR EACH ELEV. STEP
IN EXCEL & CREATE RATING CURVE

Remarks/Conclusions/Results:

ATTACHED

Calculation Approved by:  12/24/08
Project Manager Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____

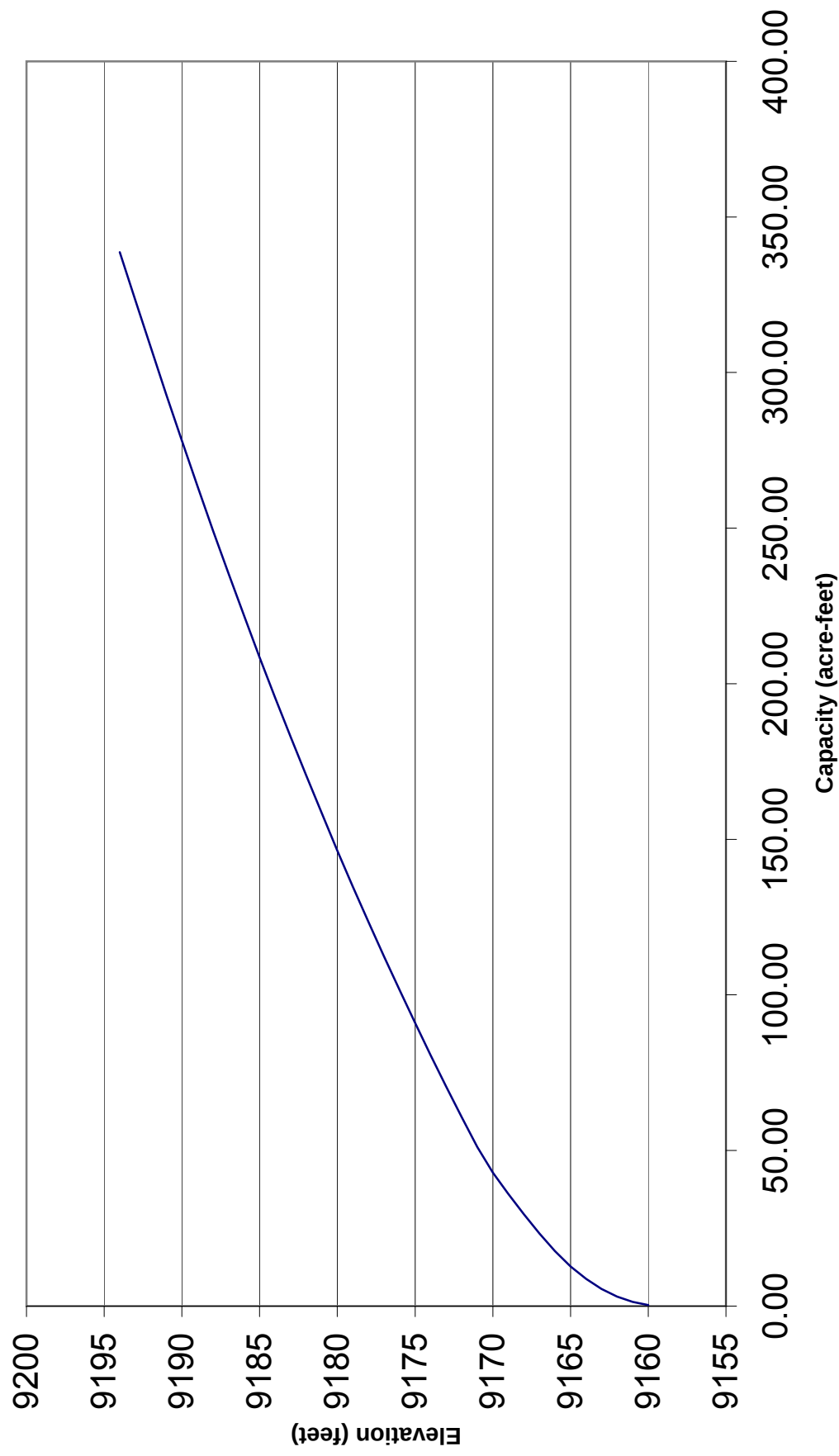
Project Manager/Date

Elevation	area ft^2	area acre	average area acre	Σ volume acre-ft
9159.99	0	0	0	
9160	29774	0.684	0.3418	0.34
9161	58310	1.339	1.0111	1.35
9162	91631	2.104	1.7211	3.07
9163	122320	2.808	2.4558	5.53
9164	156456	3.592	3.1999	8.73
9165	194829	4.473	4.0322	12.76
9166	235483	5.406	4.9393	17.70
9167	257978	5.922	5.6642	23.37
9168	278391	6.391	6.1567	29.52
9169	291106	6.683	6.5369	36.06
9170	303899	6.977	6.8297	42.89
9171	413151	9.485	8.2306	51.12
9172	423499	9.722	9.6034	60.72
9173	433938	9.962	9.8420	70.56
9174	444548	10.205	10.0836	80.65
9175	455294	10.452	10.3288	90.98
9176	466196	10.702	10.5772	101.55
9177	477228	10.956	10.8290	112.38
9178	488423	11.213	11.0841	123.47
9179	499772	11.473	11.3429	134.81
9180	511305	11.738	11.6056	146.42
9181	522923	12.005	11.8713	158.29
9182	534753	12.276	12.1404	170.43
9183	546715	12.551	12.4135	182.84
9184	558872	12.830	12.6904	195.53
9185	571145	13.112	12.9708	208.50
9186	583634	13.398	13.2550	221.76
9187	596318	13.690	13.5440	235.30
9188	614858	14.115	13.9024	249.20
9189	631594	14.499	14.3073	263.51
9190	640929	14.714	14.6066	278.12
9191	650306	14.929	14.8213	292.94
9192	659721	15.145	15.0370	307.98
9193	669174	15.362	15.2536	323.23
9194	678660	15.580	15.4710	338.70

CARDS FOR HEC-1 INPUT

SA	0.000	0.684	2.104	3.592	5.406	6.391	6.977	9.722	10.205	10.702
SA	11.213	11.738	12.276	12.830	13.398	14.115	14.714	14.929	15.145	15.580
SE	9159.9	9160	9162	9164	9166	9168	9170	9172	9174	9176
SE	9178	9180	9182	9184	9186	9188	9190	9191	9192	9194

**Enlargement of Old Dillon Reservoir
Capacity-Elevation Curve**



PROPOSED SPILLWAY RATING CURVE



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: SPILLWAY RATING CURVE FOR ODR

Total Number of Pages (including cover sheet): 4

Total Number of Computer Runs: —

Prepared by: PGS Date: 10/22/08

Checked by: _____ Date: _____

Description and Purpose:

CREATE A RATING CURVE FOR FLOW OVER THE PROPOSED
SPILLWAY AT OLD DILLON RESERVIOR

Design Basis/References/Assumptions:

USE THE SIMPLE WEIR EQUATION IN EXCEL TO DETERMINE
THE RELATIONSHIP BETWEEN ELEVATION & DISCHARGE FOR
ROUTING CALCULATIONS TO BE PERFORMED IN HEC-1

Remarks/Conclusions/Results:

ATTACHED

Calculation Approved by:  10/24/08
Project Manager Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____

Project Manager/Date

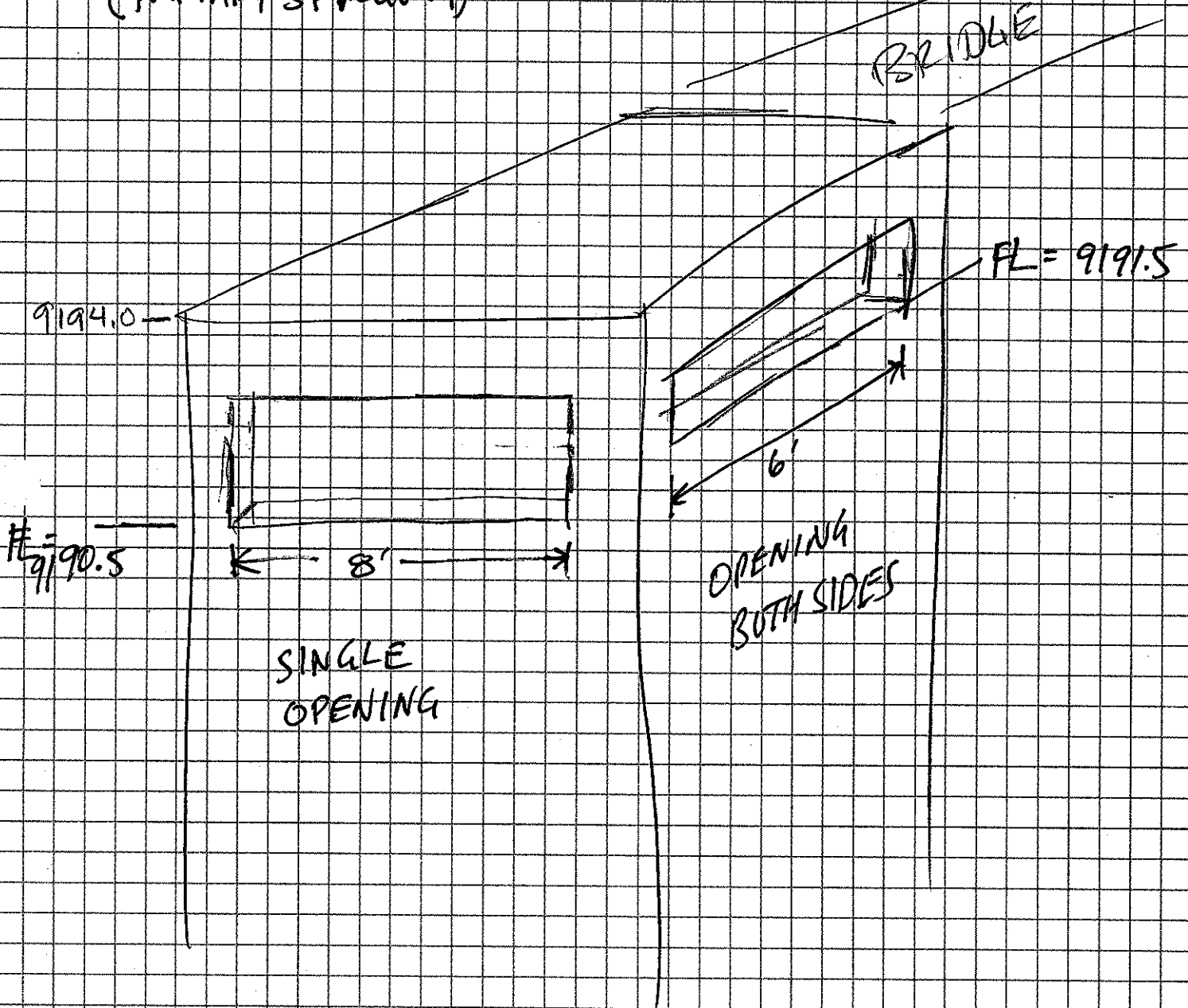


Client: _____ Job No.: 133-1187.004.03 Sheet _____ of _____

Description: _____ Designed By: _____ Date: _____

PROPOSED OLD DILLON DAM

Checked By: _____ Date: _____

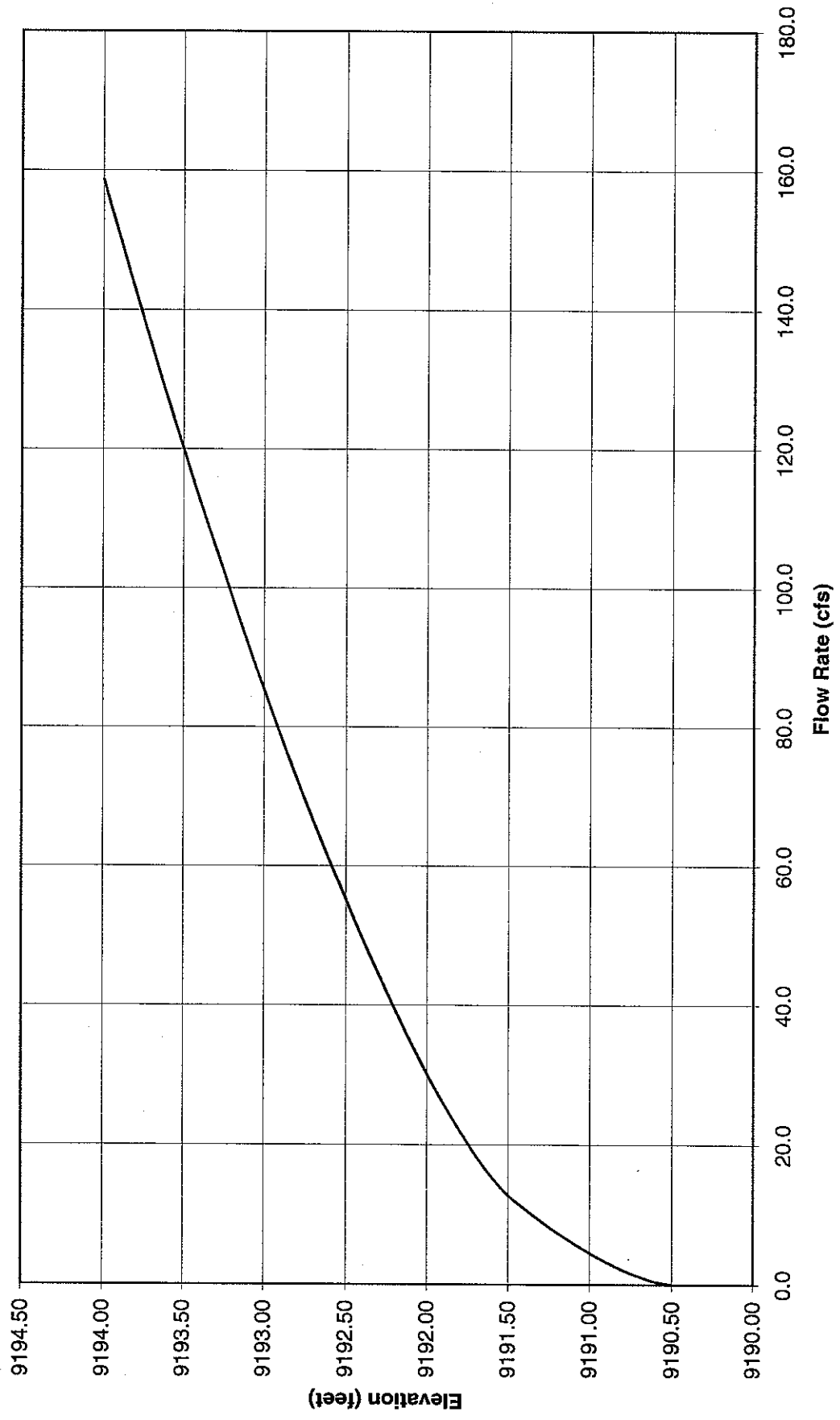
INTAKE STRUCTURE - OUTLET TO SALT LICK GULCH
(PRIMARY SPILLWAY)

$$Q = CLH^{3/2}$$

$$C = 2.65$$

Weir Coeff.	2.65											
Lower Opening L=8' - Reduce to 4.8 to account for 40% obstruction due to screening												
Upper Opening L=6' x2 - Reduce from 12' to 7.2' to account for 40% obstruction due to screening												
LOWER OPENING				UPPER OPENINGS				Total				
elev	h	L	q	elev	h	L	q	elev	h	q		
9190.5	0.0	4.8	0.0	9190.50	0.00	7.20	0.0	9190.5	0.0	0.0	Lower Opening Crest	
9190.6	0.1	4.8	0.4	9190.60	0.00	7.20	0.0	9190.6	0.0	0.4		
9190.7	0.2	4.8	1.1	9190.70	0.00	7.20	0.0	9190.7	0.0	1.1		
9190.8	0.3	4.8	2.1	9190.80	0.00	7.20	0.0	9190.8	0.0	2.1		
9190.9	0.4	4.8	3.2	9190.90	0.00	7.20	0.0	9190.9	0.0	3.2		
9191.0	0.5	4.8	4.5	9191.00	0.00	7.20	0.0	9191.0	0.0	4.5		
9191.1	0.6	4.8	5.9	9191.10	0.00	7.20	0.0	9191.1	0.0	5.9		
9191.2	0.7	4.8	7.4	9191.20	0.00	7.20	0.0	9191.2	0.0	7.4		
9191.3	0.8	4.8	9.1	9191.30	0.00	7.20	0.0	9191.3	0.0	9.1		
9191.4	0.9	4.8	10.9	9191.40	0.00	7.20	0.0	9191.4	0.0	10.9		
9191.5	1.0	4.8	12.7	9191.50	0.00	7.20	0.0	9191.5	0.0	12.7	Upper Opening Crest	
9191.6	1.1	4.8	14.7	9191.60	0.10	7.20	0.6	9191.6	0.1	15.3		
9191.7	1.2	4.8	16.7	9191.70	0.20	7.20	1.7	9191.7	0.2	18.4		
9191.8	1.3	4.8	18.9	9191.80	0.30	7.20	3.1	9191.8	0.3	22.0		
9191.9	1.4	4.8	21.1	9191.90	0.40	7.20	4.8	9191.9	0.4	25.9		
9192.0	1.5	4.8	23.4	9192.00	0.50	7.20	6.7	9192.0	0.5	30.1		
9192.1	1.6	4.8	25.7	9192.10	0.60	7.20	8.9	9192.1	0.6	34.6		
9192.2	1.7	4.8	28.2	9192.20	0.70	7.20	11.2	9192.2	0.7	39.4		
9192.3	1.8	4.8	30.7	9192.30	0.80	7.20	13.7	9192.3	0.8	44.4		
9192.4	1.9	4.8	33.3	9192.40	0.90	7.20	16.3	9192.4	0.9	49.6		
9192.5	2.0	4.8	36.0	9192.50	1.00	7.20	19.1	9192.5	1.0	55.1		
9192.6	2.1	4.8	38.7	9192.60	1.10	7.20	22.0	9192.6	1.1	60.7		
9192.7	2.2	4.8	41.5	9192.70	1.20	7.20	25.1	9192.7	1.2	66.6		
9192.8	2.3	4.8	44.4	9192.80	1.30	7.20	28.3	9192.8	1.3	72.6		
9192.9	2.4	4.8	47.3	9192.90	1.40	7.20	31.6	9192.9	1.4	78.9		
9193.0	2.5	4.8	50.3	9193.00	1.50	7.20	35.1	9193.0	1.5	85.3		
9193.1	2.6	4.8	53.3	9193.10	1.60	7.20	38.6	9193.1	1.6	91.9		
9193.2	2.7	4.8	56.4	9193.20	1.70	7.20	42.3	9193.2	1.7	98.7		
9193.3	2.8	4.8	59.6	9193.30	1.80	7.20	46.1	9193.3	1.8	105.7		
9193.4	2.9	4.8	62.8	9193.40	1.90	7.20	50.0	9193.4	1.9	112.8		
9193.5	3.0	4.8	66.1	9193.50	2.00	7.20	54.0	9193.5	2.0	120.1		
9193.6	3.1	4.8	69.4	9193.60	2.10	7.20	58.1	9193.6	2.1	127.5		
9193.7	3.2	4.8	72.8	9193.70	2.20	7.20	62.3	9193.7	2.2	135.1		
9193.8	3.3	4.8	76.3	9193.80	2.30	7.20	66.6	9193.8	2.3	142.8		
9193.9	3.4	4.8	79.7	9193.90	2.40	7.20	70.9	9193.9	2.4	150.7		
9194.0	3.5	4.8	83.3	9194.00	2.50	7.20	75.4	9194.0	2.5	158.7	Dam Crest	

**Spillway Rating Curve
Enlargement of Old Dillon Reservoir**



RESERVOIR ELEVATION – CAPACITY CURVE



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: RESERVOIR ELEVATION CAPACITY CURVE

Total Number of Pages (including cover sheet): 3

Total Number of Computer Runs: —

Prepared by: AJT Date: OCT 24, 2008

Checked by: — Date: —

Description and Purpose:

EXHIBIT RELATING PROPOSED
RESERVOIR - AREA - CAPACITY

Design Basis/References/Assumptions:

SUMMARY OF PREVIOUS CALCS + RESERVOIR
- NHWL
- PMP ELEVATION
- DAM CREST

Remarks/Conclusions/Results:

Calculation Approved by: _____
Project Manager Date

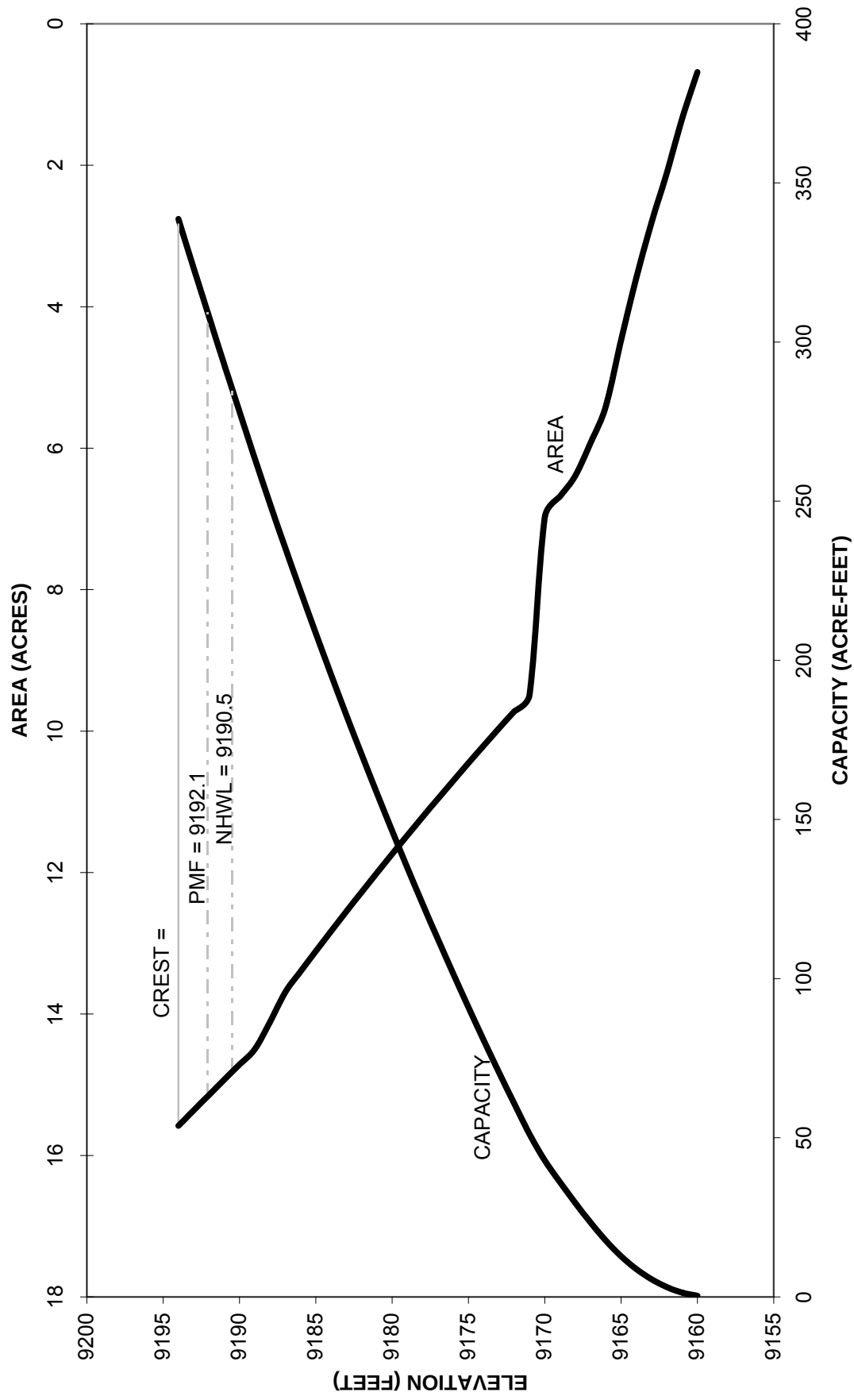
Revision No.: _____ Description of Revision: _____ Approved by: _____

Project Manager/Date

AREA - CAPACITY TABLE

Elevation	Area	Average area	Cum Volume	
	(Acres)		(Acre-Ft)	
9194	15.58	15.5	338.70	Dam Crest
9193	15.36	15.3	323.23	
9192.4	15.23	15.2	314.08	PMF
9192	15.15	15.0	307.98	
9191	14.93	14.8	292.94	Spillway Crest
9190.5	14.82	14.7	285.53	
9190	14.71	14.6	278.12	
9189	14.50	14.3	263.51	
9188	14.12	13.9	249.20	
9187	13.69	13.5	235.30	
9186	13.40	13.3	221.76	
9185	13.11	13.0	208.50	
9184	12.83	12.7	195.53	
9183	12.55	12.4	182.84	
9182	12.28	12.1	170.43	
9181	12.00	11.9	158.29	
9180	11.74	11.6	146.42	
9179	11.47	11.3	134.81	
9178	11.21	11.1	123.47	
9177	10.96	10.8	112.38	
9176	10.70	10.6	101.55	
9175	10.45	10.3	90.98	
9174	10.21	10.1	80.65	
9173	9.96	9.8	70.56	
9172	9.72	9.6	60.72	
9171	9.48	8.2	51.12	
9170	6.98	6.8	42.89	
9169	6.68	6.5	36.06	
9168	6.39	6.2	29.52	
9167	5.92	5.7	23.37	
9166	5.41	4.9	17.70	
9165	4.47	4.0	12.76	
9164	3.59	3.2	8.73	
9163	2.81	2.5	5.53	
9162	2.10	1.7	3.07	
9161	1.34	1.0	1.35	
9160	0.68	0.3	0.34	Outlet Works Invert

AREA CAPACITY CURVE



APPENDIX B

HEC-1 MODELS

USBR

LOCAL



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: HEC-1 Calculations for ODR - Local PMP - USBR hydrographs

Total Number of Pages (including cover sheet): 13

Total Number of Computer Runs: _____

Prepared by: AGS Date: 10/22/08

Checked by: _____ Date: _____

Description and Purpose:

Calculate/Route flows tributary to ODR through reservoir
1 out the spillway to determine max. discharge & elevation

Design Basis/References/Assumptions:

- Input data from USBR hydrographs & rating curves for stage-storage-discharge into HEC-1 & calculate
- Rule 5.9.1.4 - 'Small Dam, High Hazard' - 0.9 IDF reduction

Remarks/Conclusions/Results:

$$Q = 51 \text{ cfs}$$

$$\text{Max. Elev.} = 9192.43$$

Calculation Approved by:  Date: 10/24/08

Project Manager

Date

Revision No.: _____ Description of Revision: _____ Approved by: _____

Project Manager/Date

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 24OCT08 TIME 14:44:59 *
*****

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```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          *DIAGRAM
2          ID Old Dillon Reservoir
3          ID Proposed Reservoir - LOCAL PMP
4          ID USBR hydrographs
5          ID Maximum water surface and discharge determination for proposed spillway struct
6          ID 10/22/2008
7          ID file name: PMP_USBR_LOCAL.ih1
8          *
9          IT      1 01JUL09      1200      361
10         IO      3      0
11         * Rule 5.9.1.4 - From Table 5.2 - Small Dam, High Hazard
12         JR      PREC      0.9
13         *
14
15         KK      H[NE]
16         KM      Rainfall runoff for Basin NE
17         BA      0.012
18         IN      60
19         PI      0.25      0.58      8.4      1.18      0.34      0.17
20         KO      22
21         UI      0      1      3      11      19      27      37      46      52      45
22         UI      38      31      24      18      14      11      9      8      7      6
23         UI      5      5      4      4      3      3      3      3      2      2
24         UI      2      2      2      2      1      1      1      1      1      1
25         UI      1      1      1      1      1      1      1      1      0      0
26         *
27
28         KK      H[SW]
29         KM      Rainfall runoff for Basin SW
30         BA      0.014
31         IN      60
32         PI      0.25      0.58      8.4      1.18      0.34      0.17
33         KO      22
34         UI      0      1      1      4      10      16      22      29      36      43
35         UI      49      45      39      34      29      23      19      15      13      11
36         UI      9      8      7      6      6      5      5      4      4      4
37         UI      3      3      3      3      2      2      2      2      2      2
38         UI      2      2      1      1      1      1      1      1      1      1
39         UI      1      1      1      1      1      1      1      1      0      0
40         *
41
42         KK      water
43         KM      Rainfall falling on ODR
44         KO      22
45         BA      0.025
46         * Base flow = 10 cfs from dillon ditch
47         BF      10
48         UI      0      968
49         *

```

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
39	KK combn
40	KM
41	KO
42	HC 3 22
	*
43	KK ODR
44	KM Proposed ODR - enlarged reservoir and proposed spillway; NHWL = 9190.5
45	KO 22
46	RS 1 ELEV 9190.5
47	SA 0 0.684 2.104 3.592 5.406 6.391 6.977 9.722 10.205 10.702
48	SA 11.213 11.738 12.276 12.83 13.398 14.115 14.714 14.929 15.145 15.58
49	SE 9159.9 9160 9162 9164 9166 9168 9170 9172 9174 9176
50	SE 9178 9180 9182 9184 9186 9188 9190 9191 9192 9194
	*
	* Outflow structure - lower opening - FL = 90.5; L = 8'; 40% obstruction
	* due to screening
51	SS 9190.5 4.8 2.65 1.5
	* Outflow structure - upper openings - FL = 91.5; L = 12'; 40% obstruction
	* due to screening
52	ST 9191.5 7.2 2.65 1.5
	*
53	ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	H[NE]	
2		H[SW]
33		water
39	combn.....	
	V	
43	ODR	

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
* RUN DATE 24OCT08 TIME 14:44:59
*****

*****
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*****
```

Old Dillon Reservoir
Proposed Reservoir - LOCAL PMP
USBR hydrographs
Maximum water surface and discharge determination for proposed spillway struct
10/22/2008
file name: PMP_USBR_LOCAL.iht

8 IO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 1 MINUTES IN COMPUTATION INTERVAL
 IDATE 1JUL 9 STARTING DATE
 ITIME 1200 STARTING TIME
 NQ 361 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 1JUL 9 ENDING DATE
 NDTIME 1800 ENDING TIME
 ICENT 19 CENTURY MARK

 COMPUTATION INTERVAL .02 HOURS
 TOTAL TIME BASE 6.00 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .90

*** **

10 KK *****
 * *
 * H[NE] *
 * *

 Rainfall runoff for Basin NE

13 IN TIME DATA FOR INPUT TIME SERIES
 JXMIN 60 TIME INTERVAL IN MINUTES
 JXDATE 1JUL 9 STARTING DATE
 JXTIME 1200 STARTING TIME

15 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH
 IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 361 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .017 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

12 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

14 PB STORM 10.92 BASIN TOTAL PRECIPITATION

14 PI INCREMENTAL PRECIPITATION PATTERN
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00
 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01
 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01
 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01
 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01

.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
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.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

16 UI INPUT UNITGRAPH, 47 ORDINATES, VOLUME = .99

.0	1.0	3.0	11.0	19.0	27.0	37.0	46.0	52.0	45.0
38.0	31.0	24.0	18.0	14.0	11.0	9.0	8.0	7.0	6.0
5.0	5.0	4.0	4.0	3.0	3.0	3.0	3.0	2.0	2.0
2.0	2.0	2.0	2.0	1.0	1.0	1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0

*** *** *** *** ***

HYDROGRAPH AT STATION H[NE]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 10.92, TOTAL LOSS = .00, TOTAL EXCESS = 10.92

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	6.00-HR (CFS)
65.	2.78	14.	10.824	7.	14.
			10.824	10.824	10.824
			7.	7.	7.

CUMULATIVE AREA = .01 SQ MI

*** *** *** ***

HYDROGRAPH AT STATION H[NE]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 9.83, TOTAL LOSS = .00, TOTAL EXCESS = 9.83

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	6.00-HR (CFS)
58.	2.78	13.	9.742	6.	13.
			9.742	9.742	9.742
			6.	6.	6.

CUMULATIVE AREA = .01 SQ MI

*** **

21 KK

* H[SW] *
* *

Rainfall runoff for Basin SW

24 IN

TIME DATA FOR INPUT TIME SERIES
JXMIN 60 TIME INTERVAL IN MINUTES
JXDATE 1JUL 9 STARTING DATE
JXTIME 1200 STARTING TIME

26 KO

OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 361 LAST ORDINATE PUNCHED OR SAVED
TIMINT .017 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

23 BA

SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

25 PB STORM 10.92 BASIN TOTAL PRECIPITATION

25 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

27 UI INPUT UNITGRAPH, 58 ORDINATES, VOLUME = 1.00

.0	1.0	1.0	4.0	10.0	16.0	22.0	29.0	36.0	43.0
49.0	45.0	39.0	34.0	29.0	23.0	19.0	15.0	13.0	11.0
9.0	8.0	7.0	6.0	6.0	5.0	5.0	4.0	4.0	4.0
3.0	3.0	3.0	3.0	2.0	2.0	2.0	2.0	2.0	2.0
2.0	2.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0

HYDROGRAPH AT STATION H[SW]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 10.92, TOTAL LOSS = .00, TOTAL EXCESS = 10.92

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (INCHES)	6.00-HR (INCHES)
76.	2.97	16.	16.	16.	16.
		10.855	10.855	10.855	10.855
		8.	8.	8.	8.

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION H[SW]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 9.83, TOTAL LOSS = .00, TOTAL EXCESS = 9.83

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (INCHES)	6.00-HR (INCHES)
68.	2.97	15.	15.	15.	15.
		9.770	9.770	9.770	9.770
		7.	7.	7.	7.

CUMULATIVE AREA = .01 SQ MI

*

33 KK water *

*

Rainfall falling on ODR

35 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED

SUBBASIN RUNOFF DATA

36 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

37 RF BASE FLOW CHARACTERISTICS
STRTO 10.00 INITIAL FLOW
QRCSN .00 BEGIN BASE FLOW RECESSION
RTIOR 1.00000 RECESSION CONSTANT

PRECIPITATION DATA

25 PB STORM 10.92 BASIN TOTAL PRECIPITATION

25 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

36 UI INPUT UNITGRAPH, 2 ORDINATES, VOLUME = 1.00
.0 968.0

*** *** *** *** ***

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 10.92, TOTAL LOSS = .00, TOTAL EXCESS = 10.92

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	6.00-HR (CFS)
146.	2.03	39.	39.	39.	39.
		14.635	14.635	14.635	14.635
		20.	20.	20.	20.

CUMULATIVE AREA = .03 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 9.83, TOTAL LOSS = .00, TOTAL EXCESS = 9.83

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	6.00-HR (CFS)
132.	2.03	36.	36.	36.	36.
		13.543	13.543	13.543	13.543
		18.	18.	18.	18.

CUMULATIVE AREA = .03 SQ MI

*** **

39 KK *****
*
* combn *
*

```

41 KO          OUTPUT CONTROL VARIABLES
                IPRNT      3  PRINT CONTROL
                IPLOT      0  PLOT CONTROL
                QSCAL      0.  HYDROGRAPH PLOT SCALE
                IPNCH      0  PUNCH COMPUTED HYDROGRAPH
                IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
                ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
                ISAV2     361  LAST ORDINATE PUNCHED OR SAVED
                TIMINT     .017 TIME INTERVAL IN HOURS

```

PEAK FLOW (CFS)	TIME (HR)	6-HR	24-HR	72-HR	6.00-HR
258.	2.97	(CFS) 64.	64.	64.	64.
		(INCHES) 11.613	11.613	11.613	11.613
		(AC-FT) 32.	32.	32.	32.

Proposed ODR ~ enlarged reservoir and proposed spillway; NHWL = 9190.5

```

45 KO          OUTPUT CONTROL VARIABLES
                IPRNT      3  PRINT CONTROL
                IPLOT      0  PLOT CONTROL
                QSCAL      0.  HYDROGRAPH PLOT SCALE
                IPNCH      0  PUNCH COMPUTED HYDROGRAPH
                IOUT       22  SAVE HYDROGRAPH ON THIS UNIT
                ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
                ISAV2     361  LAST ORDINATE PUNCHED OR SAVED
                TIMINT     .017 TIME INTERVAL IN HOURS

```

```

46 RS      STORAGE ROUTING
           NSTPS      1  NUMBER OF SUBREACHES
           ITYP      ELEV  TYPE OF INITIAL CONDITION
           RSVRIC    9190.50  INITIAL CONDITION
           X          .00  WORKING R AND D COEFFICIENT

```

49 SE	ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
		9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00

51 SS	SPILLWAY		
	CREL	9190.50	SPILLWAY CREST ELEVATION
	SPWID	4.80	SPILLWAY WIDTH
	COQW	2.65	WEIR COEFFICIENT
	EXPW	1.50	EXPONENT OF HEAD

52 ST	TOP OF DAM		
	TOPEL	9191.50	ELEVATION AT TOP OF DAM
	DAMWID	7.20	DAM WIDTH
	COQD	2.65	WEIR COEFFICIENT
	EXPD	1.50	EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	291.21	306.25	336.97
ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00

COMPUTED OUTFLOW-ELEVATION DATA

(EXCLUDING FLOW OVER DAM)

OUTFLOW	.00	.00	.01	.11	.39	.91	1.79	3.08	4.90	7.31
ELEVATION	9159.90	9190.50	9190.51	9190.54	9190.60	9190.67	9190.77	9190.89	9191.03	9191.19
OUTFLOW	10.41	14.28	19.00	24.68	31.37	39.19	48.20	58.50	70.17	83.29
ELEVATION	9191.38	9191.58	9191.81	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

(INCLUDING FLOW OVER DAM)

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	283.77	283.93	284.41
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.01	.11
ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9190.50	9190.51	9190.54
STORAGE	285.22	286.34	287.79	289.55	291.21	291.65	294.07	296.82	299.91	303.32
OUTFLOW	.39	.91	1.79	3.08	4.50	4.90	7.31	10.41	14.71	22.24
ELEVATION	9190.60	9190.67	9190.77	9190.89	9191.00	9191.03	9191.19	9191.38	9191.58	9191.81
STORAGE	306.25	307.09	311.18	315.64	320.44	325.59	331.10	336.97		
OUTFLOW	30.11	32.58	45.67	61.72	80.85	103.27	129.15	158.71		
ELEVATION	9192.00	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00		

HYDROGRAPH AT STATION ODR
FOR PLAN 1, RATIO = .90

PEAK OUTFLOW IS 37. AT TIME 4.02 HOURS

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
37.	4.02	6-HR	24-HR	72-HR	6.00-HR
		19.	19.	19.	19.
		(INCHES)	3.427	3.427	3.427
		(AC-FT)	9.	9.	9.
PEAK STORAGE (AC-FT)	TIME (HR)	MAXIMUM AVERAGE STORAGE			
308.	4.02	6-HR	24-HR	72-HR	6.00-HR
		298.	298.	298.	298.
PEAK STAGE (FEET)	TIME (HR)	MAXIMUM AVERAGE STAGE			
9192.14	4.02	6-HR	24-HR	72-HR	6.00-HR
		9191.45	9191.45	9191.45	9191.45

CUMULATIVE AREA = .05 SQ MI

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
				.90	
HYD. PH AT	H[NE]	.01	1	FLOW	58.
				TIME	2.78
HYDROGRAPH AT	H[SW]	.01	1	FLOW	68.
				TIME	2.97
HYDROGRAPH AT	water	.03	1	FLOW	132.
				TIME	2.03
3 COMBINED AT	combn	.05	1	FLOW	258.
				TIME	2.97
ROUTED TO	ODR	.05	1	FLOW	37.
				TIME	4.02
** PEAK STAGES IN FEET **					
1	STAGE				9192.14
	TIME				4.02

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION ODR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

ELEVATION	9190.50	9190.50	9191.50
STORAGE	284.	284.	299.
OUTFLOW	0.	0.	13.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.90	9192.14	.64	308.	37.	3.33	4.02	.00

*** NORMAL END OF HEC-1 ***

USBR
GENERAL



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03

Project Name: Enlargement of Old Dillon Reservoir

Title: HEC-1 Calculations for ODR - General PMP - USBR hydrographs

Total Number of Pages (including cover sheet): 12

Total Number of Computer Runs: _____

Prepared by: PGS Date: 10/22/08

Checked by: _____ Date: _____

Description and Purpose:

Calculate / route flows tributary to ODR through reservoir
& out the spillway to determine max. discharge & elevation

Design Basis/References/Assumptions:

- Input data from USBR hydrographs & rating curves for stage-storage-discharge into HEC-1 & calculate
- Rule 5.9.1.4 - 'Small Dam, High Hazard' - 0.9 IDF reduction

Remarks/Conclusions/Results:

$Q = 20 \text{ cfs}$

Max. Elev. = 9191.73

Calculation Approved by:  Date: 10/24/08

Project Manager

Date

Revision No.: _____ Description of Revision: _____ Approved by: _____

Project Manager/Date

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 24OCT08 TIME 14:46:16 *
* *****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
* *****

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X X XXXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXX XXXX X XXXX X
X X X X X
X X X X X
X X XXXXXXX XXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          *DIAGRAM
2          ID   Old Dillon Reservior
3          ID   Proposed Reservoir - GENERAL PMP
4          ID   USBR hydrographs
5          ID   Maximum water surface and discharge determination for proposed spillway struct
6          ID   10/22/2008
7          ID   file name: PMP_USBR_GENERAL.ih1
8          *
9          IT      3 01JUL09      1200      1441
10         IO      3      0
11         * Rule 5.9.1.4 - From Table 5.2 - Small Dam, High Hazard
12         JR      PREC      0.9
13         *
14
15         KK      H[NE]
16         KM      Rainfall runoff for Basin NE
17         BA      0.012
18         PH      0.002      0.049      0.62      1.61      2.33      3.37      4.18      5.8      8.8      13.1
19         PH      18.7      21.4
20         KO
21         UI      4      11      30      22      16      13      10      8      6      5
22         UI      4      4      3      3      2      2      2      1      1      1
23         UI      1      1      1      1      0      0      0      0      0      0
24         *
25         *
26
27         KK      H[SW]
28         KM      Rainfall runoff for Basin SW
29         BA      0.014
30         *      60
31         * 0.25 0.58 8.4 1.18 0.34 0.17
32         KO
33         UI      2      7      18      27      21      16      13      11      9      8
34         UI      6      5      5      4      3      3      3      2      2      2
35         UI      2      1      1      1      1      1      1      1      1      1
36         *
37         *
38
39         KK      water
40         KM      Rainfall falling on ODR
41         KO
42         BA      0.025
43         * Base flow = 10 cfs from dillon ditch
44         BF      10
45         UI      0      323
46         *
47
48         KK      combn
49         KM
50         KO
51         HC      3
52         *

```

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
36	KK ODR
37	KO 22
38	RS 1 ELEV 9190.5
39	SA 0 0.684 2.104 3.592 5.406 6.391 6.977 9.722 10.205 10.702
40	SA 11.213 11.738 12.276 12.83 13.398 14.115 14.714 14.929 15.145 15.58
41	SE 9159.9 9160 9162 9164 9166 9168 9170 9172 9174 9176
42	SE 9178 9180 9182 9184 9186 9188 9190 9191 9192 9194
	*
	* Outflow structure - lower opening - FL = 90.5; L = 8'; 40% obstruction
	* due to screening
43	SS 9190.5 4.8 2.65 1.5
	* Outflow structure - upper openings - FL = 91.5; L = 12'; 40% obstruction
	* due to screening
44	ST 9191.5 7.2 2.65 1.5
	*
45	ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	H[NE]	
	.	
	.	H[SW]
	.	.
26	.	water
	.	.
32	combn.....	.
	v	
	v	
36	ODR	

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 24OCT08 TIME 14:46:16 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

Old Dillon Reservoir
Proposed Reservoir - GENERAL PMP
USBR hydrographs
Maximum water surface and discharge determination for proposed spillway struct
10/22/2008
file name: PMP_USBR_GENERAL.ih1

8 IO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 3 MINUTES IN COMPUTATION INTERVAL
IDATE 1JUL 9 STARTING DATE
ITIME 1200 STARTING TIME
NQ 1441 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 4JUL 9 ENDING DATE
NDTIME 1200 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
TOTAL TIME BASE 72.00 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.90

*** **

* H[NE] *
* *

Rainfall runoff for Basin NE

15 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 1441 LAST ORDINATE PUNCHED OR SAVED
TIMINT .050 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

12 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

13 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.62 1.61 2.33 3.37 4.18 5.80 8.80 13.10 18.70 21.40 .00 .00
STORM AREA = .05

16 UI INPUT UNITGRAPH, 24 ORDINATES, VOLUME = .98
4.0 11.0 30.0 22.0 16.0 13.0 10.0 8.0 6.0 5.0
4.0 4.0 3.0 3.0 2.0 2.0 2.0 1.0 1.0 1.0
1.0 1.0 1.0 1.0

*** **

HYDROGRAPH AT STATION H[NE]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 20.23, TOTAL LOSS = .00, TOTAL EXCESS = 20.23

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	72.00-HR
34.	36.20	(CFS)	7.	4.	2.	2.
		(INCHES)	5.735	12.849	19.841	19.841
		(AC-FT)	4.	8.	13.	13.

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION H[NE]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 18.21, TOTAL LOSS = .00, TOTAL EXCESS = 18.21

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	72.00-HR
31.	36.20	(CFS)	7.	4.	2.	2.
		(INCHES)	5.162	11.564	17.857	17.857
		(AC-FT)	3.	7.	11.	11.

CUMULATIVE AREA = .01 SQ MI

19 KK

* H[SW] *

Rainfall runoff for Basin SW

22 KO

OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	1441	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.050	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

21 SA

SUBBASIN CHARACTERISTICS

TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

13 PH

DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.62	1.61	2.33	3.37	4.18	5.80	8.80	13.10	18.70	21.40	.00	.00

STORM AREA = .05

23 UI

INPUT UNITGRAPH, 30 ORDINATES, VOLUME = .99

2.0	7.0	18.0	27.0	21.0	16.0	13.0	11.0	9.0	8.0
6.0	5.0	5.0	4.0	3.0	3.0	3.0	2.0	2.0	2.0
2.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0

HYDROGRAPH AT STATION H[SW]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 20.23, TOTAL LOSS = .00, TOTAL EXCESS = 20.23

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	72.00-HR
36.	36.25	(CFS)	9.	5.	2.	2.
		(INCHES)	5.756	12.896	19.911	19.911
		(AC-FT)	4.	10.	15.	15.

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION H[SW]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 18.21, TOTAL LOSS = .00, TOTAL EXCESS = 18.21

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	72.00-HR
32.	36.25	(CFS)	8.	4.	2.	2.
		(INCHES)	5.180	11.606	17.920	17.920
		(AC-FT)	4.	9.	13.	13.

CUMULATIVE AREA = .01 SQ MI

*** **

*
26 W water
*

Rainfall falling on ODR

28 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 1441 LAST ORDINATE PUNCHED OR SAVED
TIMINT .050 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

29 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

30 BF BASE FLOW CHARACTERISTICS
STRTO 10.00 INITIAL FLOW
QRCSN .00 BEGIN BASE FLOW RECESSION
RTIOR 1.00000 RECESSION CONSTANT

PRECIPITATION DATA

13 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.62 1.61 2.33 3.37 4.18 5.80 8.80 13.10 18.70 21.40 .00 .00

STORM AREA = .05

29 UI INPUT UNITGRAPH, 2 ORDINATES, VOLUME = 1.00
.0 323.0

*** **

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 20.23, TOTAL LOSS = .00, TOTAL EXCESS = 20.23

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	72.00-HR (INCHES)
130.	36.10	26.	19.	15.	15.
		9.574	27.988	64.879	64.879
		13.	37.	87.	87.

CUMULATIVE AREA = .03 SQ MI

*** **

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 18.21, TOTAL LOSS = .00, TOTAL EXCESS = 18.21

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	72.00-HR (INCHES)
118.	36.10	24.	18.	14.	14.
		8.988	26.677	62.854	62.854
		12.	36.	84.	84.

CUMULATIVE AREA = .03 SQ MI

*** **

*
32 KK combn
*

3 OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 1441 LAST ORDINATE PUNCHED OR SAVED
TIMINT .050 TIME INTERVAL IN HOURS

35 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION combin
FOR PLAN 1, RATIO = .90

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	72.00-HR
169.	36.15	(CFS)	39.	26.	18.	18.
		(INCHES)	7.042	18.982	39.932	39.932
		(AC-FT)	19.	52.	109.	109.

CUMULATIVE AREA = .05 SQ MI

*** **

36 KK
*
* ODR *
*

37 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22.	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	1441	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.050	TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

38 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRIC	9190.50	INITIAL CONDITION
X	.00	WORKING R AND D COEFFICIENT

3	AREA	.0	.7	2.1	3.6	5.4	6.4	7.0	9.7	10.2	10.7
		11.2	11.7	12.3	12.8	13.4	14.1	14.7	14.9	15.1	15.6

41 SE	ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
		9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00

43 SS SPILLWAY

CREL	9190.50	SPILLWAY CREST ELEVATION
SPWID	4.80	SPILLWAY WIDTH
COQW	2.65	WEIR COEFFICIENT
EXPW	1.50	EXPONENT OF HEAD

44 ST TOP OF DAM

TOPEL	9191.50	ELEVATION AT TOP OF DAM
DAMWID	7.20	DAM WIDTH
COQD	2.65	WEIR COEFFICIENT
EXPD	1.50	EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	291.21	306.25	336.97
ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00

COMPUTED OUTFLOW-ELEVATION DATA

(EXCLUDING FLOW OVER DAM)

OUTFLOW	.00	.00	.01	.11	.39	.91	1.79	3.08	4.90	7.31
ELEVATION	9159.90	9190.50	9190.51	9190.54	9190.60	9190.67	9190.77	9190.89	9191.03	9191.19
OUTFLOW	10.41	14.28	19.00	24.68	31.37	39.19	48.20	58.50	70.17	83.29
ELEVATION	9191.38	9191.58	9191.81	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

(INCLUDING FLOW OVER DAM)

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	283.77	283.93	284.41
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.01	.11
ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9190.50	9190.51	9190.54

STORAGE	285.22	286.34	287.79	289.55	291.21	291.65	294.07	296.82	299.91	303.32
OUTFLOW	.39	.91	1.79	3.08	4.50	4.90	7.31	10.41	14.71	22.24
ELEVATION	9190.60	9190.67	9190.77	9190.89	9191.00	9191.03	9191.19	9191.38	9191.58	9191.81

STORAGE	306.25	307.09	311.18	315.64	320.44	325.59	331.10	336.97
OUTFLOW	30.11	32.58	45.67	61.72	80.85	103.27	129.15	158.71
ELEVATION	9192.00	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00

*** *** *** ***

HYDROGRAPH AT STATION ODR
FOR PLAN 1, RATIO = .90

PEAK OUTFLOW IS 37. AT TIME 37.20 HOURS

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
37.	37.20	(CFS)	6-HR	24-HR	72-HR	72.00-HR
		(INCHES)	33.	25.	16.	16.
		(AC-FT)	6.052	18.366	34.395	34.395
			16.	50.	94.	94.

PEAK STORAGE (AC-FT)	TIME (HR)		MAXIMUM AVERAGE STORAGE			
309.	37.20		6-HR	24-HR	72-HR	72.00-HR
			307.	304.	299.	299.

PEAK STAGE (FEET)	TIME (HR)		MAXIMUM AVERAGE STAGE			
9192.15	37.20		6-HR	24-HR	72-HR	72.00-HR
			9192.07	9191.91	9191.64	9191.64

CUMULATIVE AREA = .05 SQ MI

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
				.90	
HYD PH AT	H{NE]	.01	1	FLOW	31.
				TIME	36.20
HYDROGRAPH AT	H{SW]	.01	1	FLOW	32.
				TIME	36.25
HYDROGRAPH AT	water	.03	1	FLOW	118.
				TIME	36.10
3 COMBINED AT	combn	.05	1	FLOW	169.
				TIME	36.15
ROUTED TO	ODR	.05	1	FLOW	37.
				TIME	37.20
** PEAK STAGES IN FEET **					
1	STAGE				9192.15
	TIME				37.20

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION ODR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
STORAGE	9190.50	9190.50	9191.50
OUTFLOW	284.	284.	299.
	0.	0.	13.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.90	9192.15	.65	309.	37.	49.25	37.20	.00

*** NORMAL END OF HEC-1 ***

NRCS

LOCAL



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03
Project Name: Enlargement of Old Dillon Reservoir NRCS
Title: HEC-1 Calculations for ODR - Local PMP - SCS hydrographs
Total Number of Pages (including cover sheet): 13
Total Number of Computer Runs: _____
Prepared by: PGS Date: 10/22/08
Checked by: _____ Date: _____
Description and Purpose:

Calculate / route flows tributary to ODR through reservoir
& out the spillway to determine max. discharge & elevation

Design Basis/References/Assumptions:

- Input data from SCS hydrographs & rating curves for stage - storage - discharge into HEC-1 & calculate
- Rule 5.9.1.4 - 'Small Dam, High Hazard' - 0.9 IDF reduction

Remarks/Conclusions/Results:

$$Q = 47 \text{ cfs}$$

$$\text{Max. Elev.} = 9192.35$$

Calculation Approved by: _____

Project Manager

10/24/08

Date

Revision No.: _____

Description of Revision: _____

Approved by: _____

Project Manager/Date

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 24OCT08 TIME 14:46:51 *
* *****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
* *****

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X X X X X
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          *DIAGRAM
2          ID   Old Dillon Reservoir
3          ID   Proposed Reservoir - LOCAL PMP
4          ID   NRCS SCS hydrographs
5          ID   Maximum water surface and discharge determination for proposed spillway struct
6          ID   10/22/2008
7          ID   file name: PMP_NRCS_LOCAL.ih1
8          *
9          IT      1 01JUL09      1200      361
10         IO      3          0
11         *
12         *
13         * Rule 5.9.1.4 - From Table 5.2 - Small Dam, High Hazard
14         JR      PREC      0.9
15
16         KK      H[NE]
17         KM      Rainfall runoff for Basin NE
18         BA      0.012
19         LS      0          86
20         UD      0.104
21         IN      60
22         PI      0.25      0.58      8.4      1.18      0.34      0.17
23         *
24         * 0.002 0.049 0.62 1.61 2.33 3.37 4.18 5.8 8.8 13.1
25         * 18.7 21.4
26         KO
27         *
28
29         KK      H[SW]
30         KM      Rainfall runoff for Basin SW
31         BA      0.014
32         LS      0          86
33         UD      0.117
34         KO
35         *
36
37         KK      water
38         KM      Rainfall falling on ODR
39         BA      0.025
40         * Base flow = 10 cfs from dillon ditch
41         BF      10
42         LS      0          98
43         UD      0.083
44         KO
45         *
46
47         KK      combn
48         KM
49         KO
50         HC      3
51         *

```

[illegible]

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	H[NE]	
	.	
	.	H[SW]
	.	.
24	.	water
	.	.
31	combn.....	
	v	
	v	
35	ODR	

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 24OCT08 TIME 14:46:51 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

Old Dillon Reservoir
Proposed Reservoir - LOCAL PMP
NRCS SCS hydrographs
Maximum water surface and discharge determination for proposed spillway struct
10/22/2008
file name: PMP_NRCS_LOCAL.ihl

8 IO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1JUL 9 STARTING DATE
ITIME 1200 STARTING TIME
NQ 361 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1JUL 9 ENDING DATE
NDTIME 1800 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 6.00 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.90

*** **

* H[NE] *

Rainfall runoff for Basin NE

15 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 60 TIME INTERVAL IN MINUTES
JXDATE 1JUL 9 STARTING DATE
JXTIME 1200 STARTING TIME

17 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 361 LAST ORDINATE PUNCHED OR SAVED
TIMINT .017 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

12 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

16 PB STORM 10.92 BASIN TOTAL PRECIPITATION

16 PI INCREMENTAL PRECIPITATION PATTERN
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.01 .01 .01 .01 .01 .01 .01 .01 .01 .01
.01 .01 .01 .01 .01 .01 .01 .01 .01 .01
.01 .01 .01 .01 .01 .01 .01 .01 .01 .01
.01 .01 .01 .01 .01 .01 .01 .01 .01 .01

.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

13 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

14 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .10 LAG

UNIT HYDROGRAPH
 33 END-OF-PERIOD ORDINATES

3.	10.	20.	33.	45.	51.	51.	48.	43.	36.
27.	21.	16.	13.	10.	8.	6.	5.	4.	3.
2.	2.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.	0.							

HYDROGRAPH AT STATION H[NE]
 FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 10.92, TOTAL LOSS = 1.74, TOTAL EXCESS = 9.18

PEP	OW	TIME (HR)	(CFS)	6-HR	24-HR	72-HR	6.00-HR
3.00			12.	12.	12.	12.	
			(INCHES)	9.160	9.160	9.160	9.160
			(AC-FT)	6.	6.	6.	6.

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION H[NE]
 FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 9.83, TOTAL LOSS = 1.72, TOTAL EXCESS = 8.11

PEAK FLOW (CFS)	TIME (HR)	(CFS)	6-HR	24-HR	72-HR	6.00-HR
56.	3.00	10.	10.	10.	10.	10.
		(INCHES)	8.092	8.092	8.092	8.092
		(AC-FT)	5.	5.	5.	5.

CUMULATIVE AREA = .01 SQ MI

18 KK

 *
 * H{SW}
 *

Rainfall runoff for Basin SW

23 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	.361	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.017	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

20 BA SUBBASIN CHARACTERISTICS

PRECIPITATION DATA

16 PB STORM 10.92 BASIN TOTAL PRECIPITATION

16 PI INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
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.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

21 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

22 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .12 LAG

UNIT HYDROGRAPH
37 END-OF-PERIOD ORDINATES

3.	9.	17.	29.	41.	50.	54.	54.	50.	45.
39.	31.	24.	19.	15.	13.	10.	8.	7.	5.
4.	3.	3.	2.	2.	1.	1.	1.	1.	1.
1.	0.	0.	0.	0.	0.	0.	0.	0.	0.

HYDROGRAPH AT STATION H[SW]
 FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 10.92, TOTAL LOSS = 1.74, TOTAL EXCESS = 9.18

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	6.00-HR (CFS)
73.	3.00	14.	14.	14.	14.
		(INCHES) 9.158	(INCHES) 9.158	(INCHES) 9.158	(INCHES) 9.158
		(AC-FT) 7.	(AC-FT) 7.	(AC-FT) 7.	(AC-FT) 7.

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION H[SW]
 FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 9.83, TOTAL LOSS = 1.72, TOTAL EXCESS = 8.11

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	6.00-HR (CFS)
66.	3.00	12.	12.	12.	12.
		(INCHES) 8.090	(INCHES) 8.090	(INCHES) 8.090	(INCHES) 8.090
		(AC-FT) 6.	(AC-FT) 6.	(AC-FT) 6.	(AC-FT) 6.

CUMULATIVE AREA = .01 SQ MI

*** **

24 KK water

Rainfall falling on ODR

30 KO

OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 361 LAST ORDINATE PUNCHED OR SAVED
TIMINT .017 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

26 BA

SUBBASIN CHARACTERISTICS

TAREA .03 SUBBASIN AREA

27 BF

BASE FLOW CHARACTERISTICS

STRTO 10.00 INITIAL FLOW
QRCSN .00 BEGIN BASE FLOW RECESSION
RTIOR 1.00000 RECESSION CONSTANT

PRECIPITATION DATA

16 PB

STORM 10.92 BASIN TOTAL PRECIPITATION

16 PI

INCREMENTAL PRECIPITATION PATTERN

.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.14	.14	.14	.14	.14	.14	.14	.14	.14	.14
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.02	.02	.02	.02	.02	.02	.02	.02	.02	.02
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01	.01
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

28 LS

SCS LOSS RATE

STRTL .04 INITIAL ABSTRACTION
CRVNR 98.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

29 UD

SCS DIMENSIONLESS UNITGRAPH

TLAG .08 LAG

UNIT HYDROGRAPH
27 END-OF-PERIOD ORDINATES

12.	35.	74.	113.	131.	131.	116.	95.	68.	50.
37.	28.	21.	15.	11.	8.	6.	5.	3.	3.
2.	1.	1.	1.	1.	0.	0.			

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 10.92, TOTAL LOSS = .24, TOTAL EXCESS = 10.68

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	6.00-HR (CFS)
145.	3.00	39.	39.	39.	39.
		(INCHES) 14.379	14.379	14.379	14.379
		(AC-FT) 19.	19.	19.	19.

CUMULATIVE AREA = .03 SQ MI

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 9.83, TOTAL LOSS = .24, TOTAL EXCESS = 9.59

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	6.00-HR
132.	3.00	(CFS) 36.	36.	36.	36.
		(INCHES) 13.290	13.290	13.290	13.290
		(AC-FT) 18.	18.	18.	18.

CUMULATIVE AREA = .03 SQ MI

*** **

*
31 KK *
* combn *
*

33 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	361	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.017	TIME INTERVAL IN HOURS

34 HC HYDROGRAPH COMBINATION

ICOMB	3	NUMBER OF HYDROGRAPHS TO COMBINE
-------	---	----------------------------------

*** **

HYDROGRAPH AT STATION combn
FOR PLAN 1, RATIO = .90

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	6.00-HR
254.	3.00	(CFS) 58.	58.	58.	58.
		(INCHES) 10.639	10.639	10.639	10.639
		(AC-FT) 29.	29.	29.	29.

CUMULATIVE AREA = .05 SQ MI

*** **

*
35 KK *
* ODR *
*

36 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	361	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.017	TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

37 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRIC	9190.50	INITIAL CONDITION
X	.00	WORKING R AND D COEFFICIENT

38 SA	AREA	.0	.7	2.1	3.6	5.4	6.4	7.0	9.7	10.2	10.7
		11.2	11.7	12.3	12.8	13.4	14.1	14.7	14.9	15.1	15.6

40 SE	ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
		9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00

42 SS SPILLWAY

CREL	9190.50	SPILLWAY CREST ELEVATION
SPWID	4.80	SPILLWAY WIDTH
COQW	2.65	WEIR COEFFICIENT
EXPW	1.50	EXPONENT OF HEAD

43 ST TOP OF DAM

TOPEL	9191.50	ELEVATION AT TOP OF DAM
DAMWID	7.20	DAM WIDTH
COQD	2.65	WEIR COEFFICIENT
EXPD	1.50	EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	291.21	306.25	336.97
ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00

COMPUTED OUTFLOW-ELEVATION DATA

(EXCLUDING FLOW OVER DAM)

OUTFLOW	.00	.00	.01	.11	.39	.91	1.79	3.08	4.90	7.31
ELEVATION	9159.90	9190.50	9190.51	9190.54	9190.60	9190.67	9190.77	9190.89	9191.03	9191.19
OUTFLOW	10.41	14.28	19.00	24.68	31.37	39.19	48.20	58.50	70.17	83.29
ELEVATION	9191.38	9191.58	9191.81	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

(INCLUDING FLOW OVER DAM)

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	283.77	283.93	284.41
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.01	.11
ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9190.50	9190.51	9190.54
STORAGE	285.22	286.34	287.79	289.55	291.21	291.65	294.07	296.82	299.91	303.32
OUTFLOW	.39	.91	1.79	3.08	4.50	4.90	7.31	10.41	14.71	22.24
ELEVATION	9190.60	9190.67	9190.77	9190.89	9191.00	9191.03	9191.19	9191.38	9191.58	9191.81
STORAGE	306.25	307.09	311.18	315.64	320.44	325.59	331.10	336.97		
OUTFLOW	30.11	32.58	45.67	61.72	80.85	103.27	129.15	158.71		
ELEVATION	9192.00	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00		

HYDROGRAPH AT STATION ODR
FOR PLAN 1, RATIO = .90

PEAK OUTFLOW IS 31. AT TIME 4.10 HOURS

PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW	
(HR)	(HR)			24-HR	72-HR
4.10	4.10	(CFS)	16.	16.	16.
		(INCHES)	2.838	2.838	2.838
		(AC-FT)	8.	8.	8.
PEAK STORAGE	TIME			MAXIMUM AVERAGE STORAGE	
(AC-FT)	(HR)			24-HR	72-HR
306.	4.10		297.	297.	297.
PEAK STAGE	TIME			MAXIMUM AVERAGE STAGE	
(FEET)	(HR)			24-HR	72-HR
9192.01	4.10		9191.38	9191.38	9191.38

CUMULATIVE AREA = .05 SQ MI

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION		
				RATIO 1		
				.90		
HYD.	PH AT	H[NE]	.01	1	FLOW TIME	56. 3.00
HYDROGRAPH AT	H[SW]	.01	1	FLOW TIME	66. 3.00	
HYDROGRAPH AT	water	.03	1	FLOW TIME	132. 3.00	
3 COMBINED AT	combn	.05	1	FLOW TIME	254. 3.00	
ROUTED TO	ODR	.05	1	FLOW TIME	31. 4.10	
** PEAK STAGES IN FEET **						
			1	STAGE	9192.01	
				TIME	4.10	

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION ODR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1

ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
STORAGE	9190.50	9190.50	9191.50
OUTFLOW	284.	284.	299.
	0.	0.	13.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.90	9192.01	.51	306.	31.	3.22	4.10	.00

*** NORMAL END OF HEC-1 ***

NRCS
GENERAL



CALCULATION COVER SHEET

Client: Colorado River Water Conservation District Project No.: 133-1187.004.03
Project Name: Enlargement of Old Dillon Reservoir NRCS
Title: HEC-1 Calculations for ODR - General PMP - SCS hydrographs
Total Number of Pages (including cover sheet): 12
Total Number of Computer Runs: _____
Prepared by: PGS Date: 10/22/08
Checked by: _____ Date: _____
Description and Purpose:

Calculate/Route flows tributary to ODR through reservoir
1 out the spillway to determine max. discharge & elevation

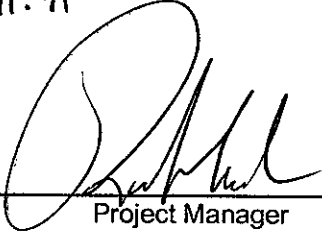
Design Basis/References/Assumptions:

- Input data from SCS hydrographs & rating curves for stage-storage-discharge into HEC-1 & calculate
- Rule 5.9.1.4 - 'Small Dam, High Hazard' - 0.9 IDF reduction

Remarks/Conclusions/Results:

$Q = 19 \text{ cfs}$

Max. Elev. = 9191.71

Calculation Approved by:  10/24/08
Project Manager Date

Revision No.:	Description of Revision:	Approved by:
_____	_____	_____
_____	_____	_____

Project Manager/Date

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 24OCT08 TIME 14:47:33 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          *DIAGRAM
2          ID   Old Dillon Reservoir
3          ID   Proposed Reservoir - GENERAL PMP
4          ID   NRCS SCS hydrographs
5          ID   Maximum water surface and discharge determination for proposed spillway struct
6          ID   10/22/2008
7          ID   file name: PMP_NRCS_GENERAL.ih1
8          *
9          IT      3 01JUL09    1200    1441
10         IO      3          0
11         * Rule 5.9.1.4 - From Table 5.2 - Small Dam, High Hazard
12         JR      PREC      0.9
13         *
14
15         KK      H[NE]
16         KM      Rainfall runoff for Basin NE
17         BA      0.012
18         LS      0          86
19         UD      0.104
20         PH      0.002    0.049    0.62    1.61    2.33    3.37    4.18    5.8    8.8    13.1
21         PH      18.7    21.4
22         *
23         *
24         *
25         KO
26         *
27
28         KK      H[SW]
29         KM      Rainfall runoff for Basin SW
30         BA      0.014
31         LS      0          86
32         UD      0.117
33         KO
34         *
35
36         KK      water
37         KM      Rainfall falling on ODR
38         BA      0.025
39         LS      0          98
40         * Base flow = 10 cfs from dillon ditch
41         BF      10
42         UD      0.083
43         KO
44         *
45
46         KK      combn
47         KM
48         KO
49         HC      3
50         *

```

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
35	KK ODR
36	KO 22
37	RS 1 ELEV 9190.5
38	SA 0 0.684 2.104 3.592 5.406 6.391 6.977 9.722 10.205 10.702
39	SA 11.213 11.738 12.276 12.83 13.398 14.115 14.714 14.929 15.145 15.58
40	SE 9159.9 9160 9162 9164 9166 9168 9170 9172 9174 9176
41	SE 9178 9180 9182 9184 9186 9188 9190 9191 9192 9194
	* Outflow structure - lower opening - FL = 90.5; L = 8'; 40% obstruction
	* due to screening
42	SS 9190.5 4.8 2.65 1.5
	* Outflow structure - upper openings - FL = 91.5; L = 12'; 40% obstruction
	* due to screening
43	ST 9191.5 7.2 2.65 1.5
	*
44	ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
LINE		
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
10	H[NE]	
	.	
	.	H[SW]
	.	.
24	.	water
	.	.
31	combn.....	.
	v	.
	v	.
35	ODR	.

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 24OCT08 TIME 14:47:33 *

* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *

Old Dillon Reservoir
Proposed Reservoir - GENERAL PMP
NRCS SCS hydrographs
Maximum water surface and discharge determination for proposed spillway struct
10/22/2008
file name: PMP_NRCS_GENERAL.ih1

8 IO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 3 MINUTES IN COMPUTATION INTERVAL
IDATE 1JUL 9 STARTING DATE
ITIME 1200 STARTING TIME
NQ 1441 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 4JUL 9 ENDING DATE
NDTIME 1200 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
TOTAL TIME BASE 72.00 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
.90

*** **

10 KK *****
* H[NE] *

Rainfall runoff for Basin NE

17 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 1441 LAST ORDINATE PUNCHED OR SAVED
TIMINT .050 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

12 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

15 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.62 1.61 2.33 3.37 4.18 5.80 8.80 13.10 18.70 21.40 .00 .00

STORM AREA = .05

13 LS SCS LOSS RATE
STRTL .33 INITIAL ABSTRACTION
CRVNR 86.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

14 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .10 LAG

UNIT HYDROGRAPH

13. 41. 43. 28. 12 END-OF-PERIOD ORDINATES 14. 8. 4. 2. 1. 1.
0. 0.

*** *** *** *** ***

HYDROGRAPH AT STATION H[NE]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 20.23, TOTAL LOSS = 1.83, TOTAL EXCESS = 18.40

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW
48.	36.15	
(CFS)		6-HR 24-HR 72-HR 72.00-HR
(INCHES)		7. 4. 2. 2.
(AC-FT)		5.730 12.702 18.396 18.396
		4. 8. 12. 12.

CUMULATIVE AREA = .01 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION H[NE]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 18.21, TOTAL LOSS = 1.82, TOTAL EXCESS = 16.39

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW
43.	36.15	
(CFS)		6-HR 24-HR 72-HR 72.00-HR
(INCHES)		7. 4. 2. 2.
(AC-FT)		5.136 11.365 16.386 16.386
		3. 7. 10. 10.

CUMULATIVE AREA = .01 SQ MI

*** **

18 KK H[SW]

Rainfall runoff for Basin SW

23 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	1441	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.050	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

20 BA SUBBASIN CHARACTERISTICS

TAREA	.01	SUBBASIN AREA
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PRECIPITATION DATA

15 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.62	1.61	2.33	3.37	4.18	5.80	8.80	13.10	18.70	21.40	.00	.00

STORM AREA = .05

21 LS SCS LOSS RATE

STRTL	.33	INITIAL ABSTRACTION
CRVNR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

22 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	.12	LAG
------	-----	-----

UNIT HYDROGRAPH
14 END-OF-PERIOD ORDINATES

12.	39.	47.	37.	20.	11.	6.	4.	2.	1.
1.	0.	0.	0.						

*** *** *** *** ***

HYDROGRAPH AT STATION H[SW]
FOR PLAN 1, RATIO = .90

RAINFALL = 20.23, TOTAL LOSS = 1.83, TOTAL EXCESS = 18.40

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW
54.	36.15	
(CFS)		6-HR 24-HR 72-HR 72.00-HR
(INCHES)		9. 5. 2. 2.
(AC-FT)		5.730 12.701 18.395 18.395
		4. 9. 14. 14.

CUMULATIVE AREA = .01 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION H[SW]
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 18.21, TOTAL LOSS = 1.82, TOTAL EXCESS = 16.39

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	72.00-HR
36.15		8.	4.	2.	2.
(INCHES)		5.136	11.365	16.385	16.385
(AC-FT)		4.	8.	12.	12.

CUMULATIVE AREA = .01 SQ MI

*** **

*
24 KK * water *
*

Rainfall falling on ODR

30 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	22	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	1441	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.050	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

26 BA SUBBASIN CHARACTERISTICS

TAREA	.03	SUBBASIN AREA
-------	-----	---------------

28 BF BASE FLOW CHARACTERISTICS

STRTO	10.00	INITIAL FLOW
QRCSN	.00	BEGIN BASE FLOW RECESSION
RTIOR	1.00000	RECESSION CONSTANT

PRECIPITATION DATA

1. DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40						TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY	
.62	1.61	2.33	3.37	4.18	5.80	8.80	13.10	18.70	21.40	.00	.00	

STORM AREA = .05

27 LS SCS LOSS RATE

STRTL	.04	INITIAL ABSTRACTION
CRVNBR	98.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

29 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	.08	LAG
------	-----	-----

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

46.	112.	89.	40.	19.	9.	4.	2.	1.	0.
-----	------	-----	-----	-----	----	----	----	----	----

*** **

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 20.23, TOTAL LOSS = .24, TOTAL EXCESS = 19.99

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	72.00-HR
114.	36.15	26.	19.	14.	14.
(INCHES)		9.565	27.965	64.613	64.613
(AC-FT)		13.	37.	86.	86.

CUMULATIVE AREA = .03 SQ MI

*** **

HYDROGRAPH AT STATION water
FOR PLAN 1, RATIO = .90

TOTAL RAINFALL = 18.21, TOTAL LOSS = .24, TOTAL EXCESS = 17.97

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	72.00-HR
104.	36.15	24.	18.	14.	14.
(INCHES)		8.980	26.654	62.591	62.591
(AC-FT)		12.	36.	83.	83.

CUMULATIVE AREA = .03 SQ MI

*** **

3.

*
* combn *
*

33 KO

OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 1441 LAST ORDINATE PUNCHED OR SAVED
TIMINT .050 TIME INTERVAL IN HOURS

34 HC

HYDROGRAPH COMBINATION

ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION combn
FOR PLAN 1, RATIO = .90

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	72.00-HR
195.	36.15	(CFS)	39.	26.	18.	18.
		(INCHES)	7.020	18.858	39.035	39.035
		(AC-FT)	19.	51.	106.	106.

CUMULATIVE AREA = .05 SQ MI

*** **

35

*
* ODR *
*

36 KO

OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 0 PUNCH COMPUTED HYDROGRAPH
IOUT 22 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 1441 LAST ORDINATE PUNCHED OR SAVED
TIMINT .050 TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

37 RS

STORAGE ROUTING

NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 9190.50 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

38 SA

AREA	.0	.7	2.1	3.6	5.4	6.4	7.0	9.7	10.2	10.7
	11.2	11.7	12.3	12.8	13.4	14.1	14.7	14.9	15.1	15.6

40 SE

ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00

42 SS

SPILLWAY

CREL 9190.50 SPILLWAY CREST ELEVATION
SPWID 4.80 SPILLWAY WIDTH
COQW 2.65 WEIR COEFFICIENT
EXPW 1.50 EXPONENT OF HEAD

43 ST

TOP OF DAM

TOPEL 9191.50 ELEVATION AT TOP OF DAM
DAMWID 7.20 DAM WIDTH
COQD 2.65 WEIR COEFFICIENT
EXPD 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	291.21	306.25	336.97

ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9191.00	9192.00	9194.00
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COMPUTED OUTFLOW-ELEVATION DATA

(EXCLUDING FLOW OVER DAM)

OUTFLOW	.00	.00	.01	.11	.39	.91	1.79	3.08	4.90	7.31
ELEVATION	9159.90	9190.50	9190.51	9190.54	9190.60	9190.67	9190.77	9190.89	9191.03	9191.19
OUTFLOW	10.41	14.28	19.00	24.68	31.37	39.19	48.20	58.50	70.17	83.29
ELEVATION	9191.38	9191.58	9191.81	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

(INCLUDING FLOW OVER DAM)

STORAGE	.00	.02	2.68	8.31	17.25	29.03	42.39	59.02	78.94	99.85
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
ELEVATION	9159.90	9160.00	9162.00	9164.00	9166.00	9168.00	9170.00	9172.00	9174.00	9176.00
STORAGE	121.76	144.71	168.72	193.83	220.05	247.56	276.39	283.77	283.93	284.41
OUTFLOW	.00	.00	.00	.00	.00	.00	.00	.00	.01	.11
ELEVATION	9178.00	9180.00	9182.00	9184.00	9186.00	9188.00	9190.00	9190.50	9190.51	9190.54
STORAGE	285.22	286.34	287.79	289.55	291.21	291.65	294.07	296.82	299.91	303.32
OUTFLOW	.39	.91	1.79	3.08	4.50	4.90	7.31	10.41	14.71	22.24
ELEVATION	9190.60	9190.67	9190.77	9190.89	9191.00	9191.03	9191.19	9191.38	9191.58	9191.81
STORAGE	306.25	307.09	311.18	315.64	320.44	325.59	331.10	336.97		
OUTFLOW	30.11	32.58	45.67	61.72	80.85	103.27	129.15	158.71		
ELEVATION	9192.00	9192.06	9192.33	9192.62	9192.93	9193.27	9193.62	9194.00		

*** *** *** *** ***

HYDROGRAPH AT STATION ODR
FOR PLAN 1, RATIO = .90

PEAK OUTFLOW IS 37. AT TIME 37.00 HOURS

PEAK FLOW	TIME				
(CFS)	(HR)		6-HR	24-HR	72-HR
37.	37.00		33.	25.	15.
		(CFS)	5.995	18.229	33.694
		(INCHES)			
		(AC-FT)	16.	50.	92.
PEAK STORAGE	TIME				
(AC-FT)	(HR)		6-HR	24-HR	72-HR
308.	37.00		307.	304.	299.
PEAK STAGE	TIME				
(FT)	(HR)		6-HR	24-HR	72-HR
9192.14	37.00		9192.07	9191.89	9191.62

CUMULATIVE AREA = .05 SQ MI

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION	
				RATIO 1	
					.90
HYD.	PH AT	H[NE]	.01	1	FLOW
					43.
					TIME
					36.15
HYDROGRAPH AT	H[SW]	.01	1	FLOW	48.
					TIME
					36.15
HYDROGRAPH AT	water	.03	1	FLOW	104.
					TIME
					36.15
3 COMBINED AT	combn	.05	1	FLOW	195.
					TIME
					36.15
ROUTED TO	ODR	.05	1	FLOW	37.
					TIME
					37.00
** PEAK STAGES IN FEET **					
1	STAGE				9192.14
	TIME				37.00

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION ODR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1							
	ELEVATION	INITIAL VALUE		SPILLWAY CREST	TOP OF DAM		
	STORAGE	9190.50		9190.50	9191.50		
	OUTFLOW	284.		284.	299.		
		0.		0.	13.		
	RATIO	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
	OF	RESERVOIR	DEPTH	STORAGE	OVER TOP	MAX OUTFLOW	FAILURE
	PMF	W.S.ELEV	OVER DAM	AC-FT	HOURS	HOURS	HOURS
	.90	9192.14	.64	308.	37.	47.55	37.00
							.00

*** NORMAL END OF HEC-1 ***